



water & sanitation

Department:
Water and Sanitation
REPUBLIC OF SOUTH AFRICA

P WMA 12/T30/00/5212/10

DIRECTORATE: OPTIONS ANALYSIS

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS:

NTABELANGA, SOMABADI AND THABENG DAM SITES

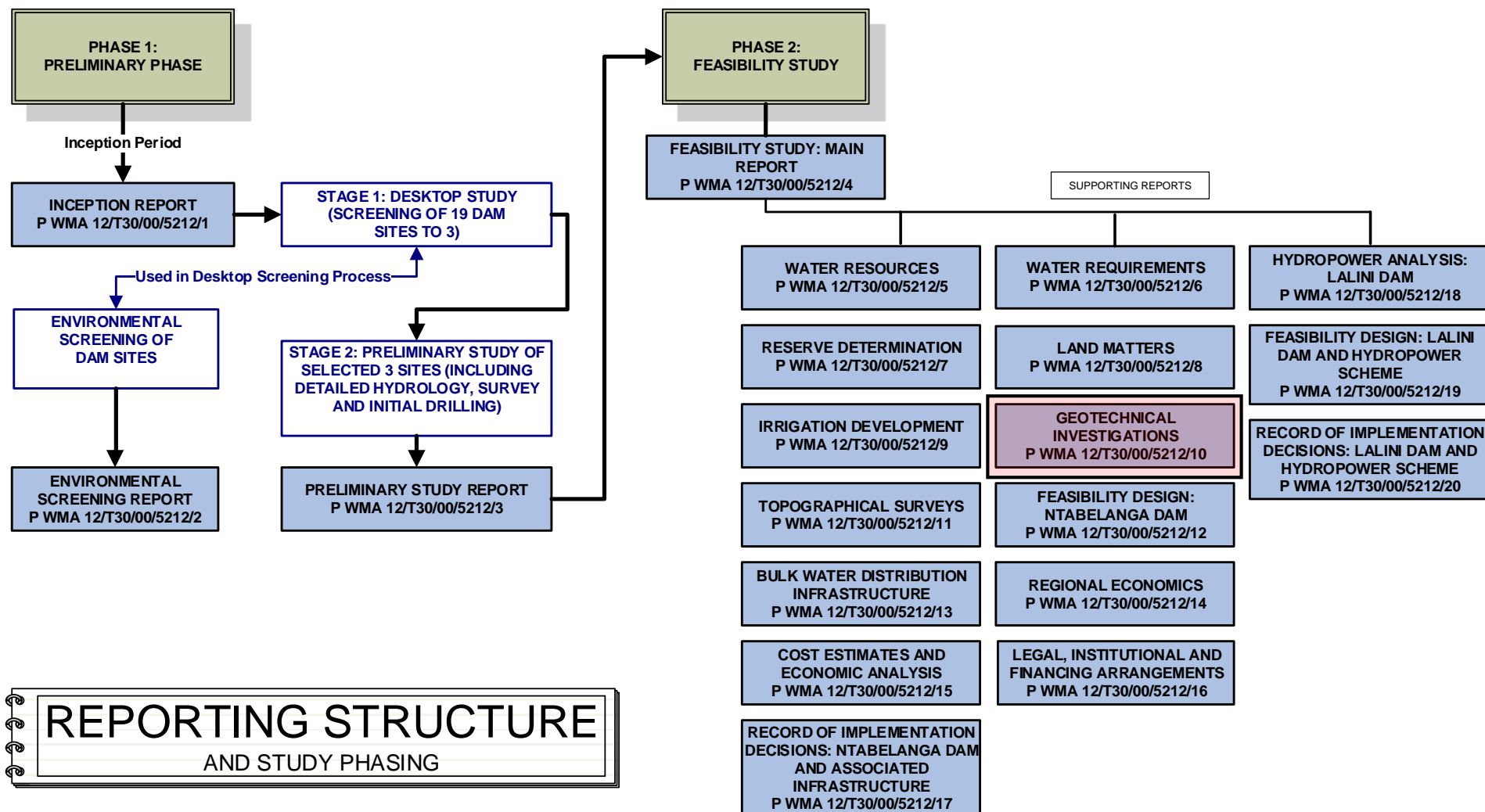
APPENDICES



OCTOBER 2014

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Record of Implementation Decisions: Lalini Dam and Hydropower Scheme	P WMA 12/T30/00/5212/20



REFERENCE

This report is to be referred to in bibliographies as:

*Department of Water and Sanitation (2014). **Feasibility Study for the Mzimvubu Water Project: Geotechnical Investigations: Ntabelanga, Somabadi and Thabeng Dam Sites: Appendices***

DWS Report No: P WMA 12/T30/00/5212/10

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Note on Departmental Name Change:

In 2014, the Department of Water Affairs changed its name to the Department of Water and Sanitation, which happened during the course of this study. In some cases this was after some of the study reports had been finalized. The reader should therefore kindly note that references to the Department of Water Affairs and the Department of Water and Sanitation herein should be considered to be one and the same.

Note on Spelling of Laleni:

The settlement named Laleni on maps issued by the Surveyor General is locally known as Lalini and both names therefore refer to the same settlement.

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APPENDIX A

PHASE 1 SITE PLANS

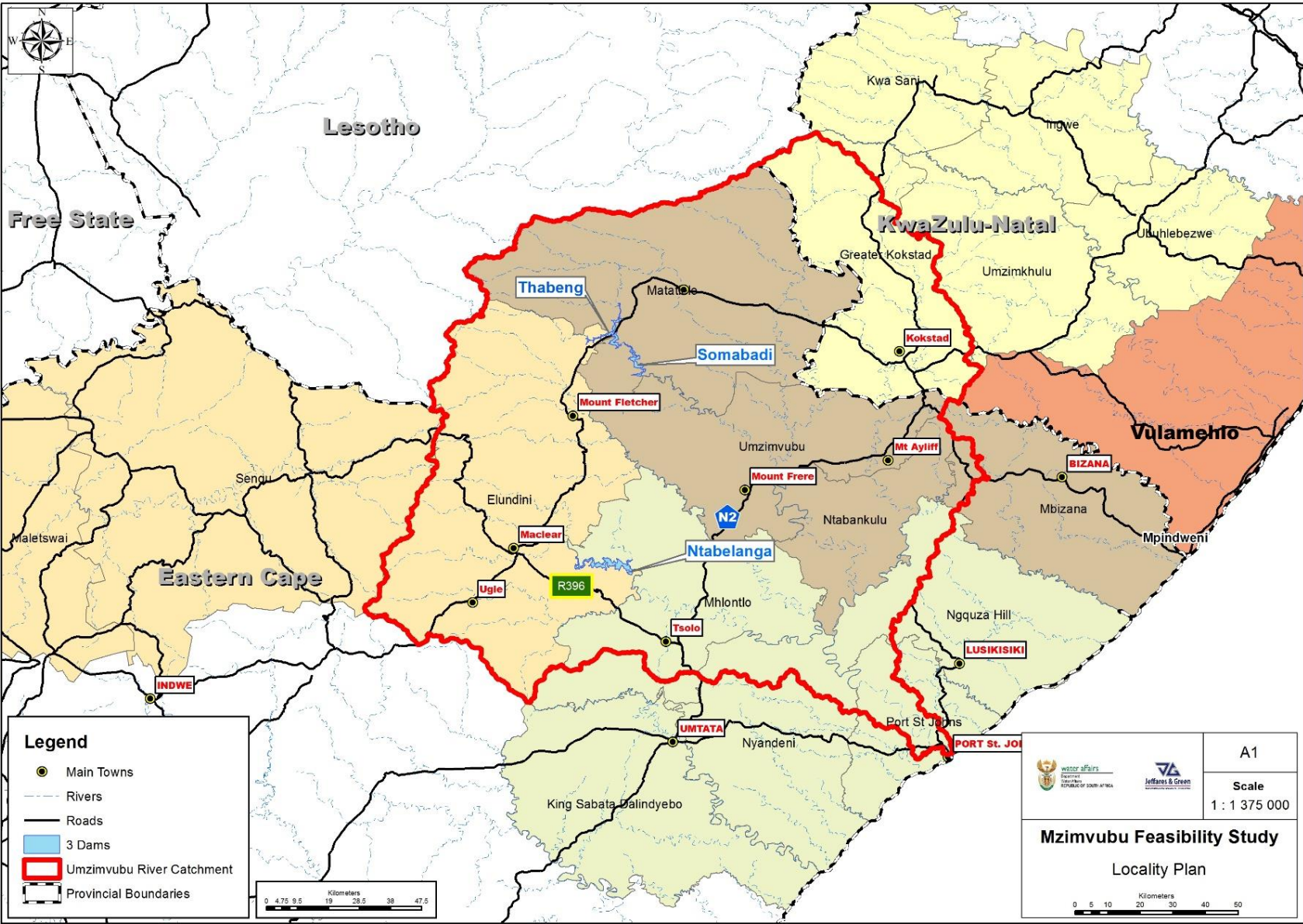


Fig A-1: Locality Plan

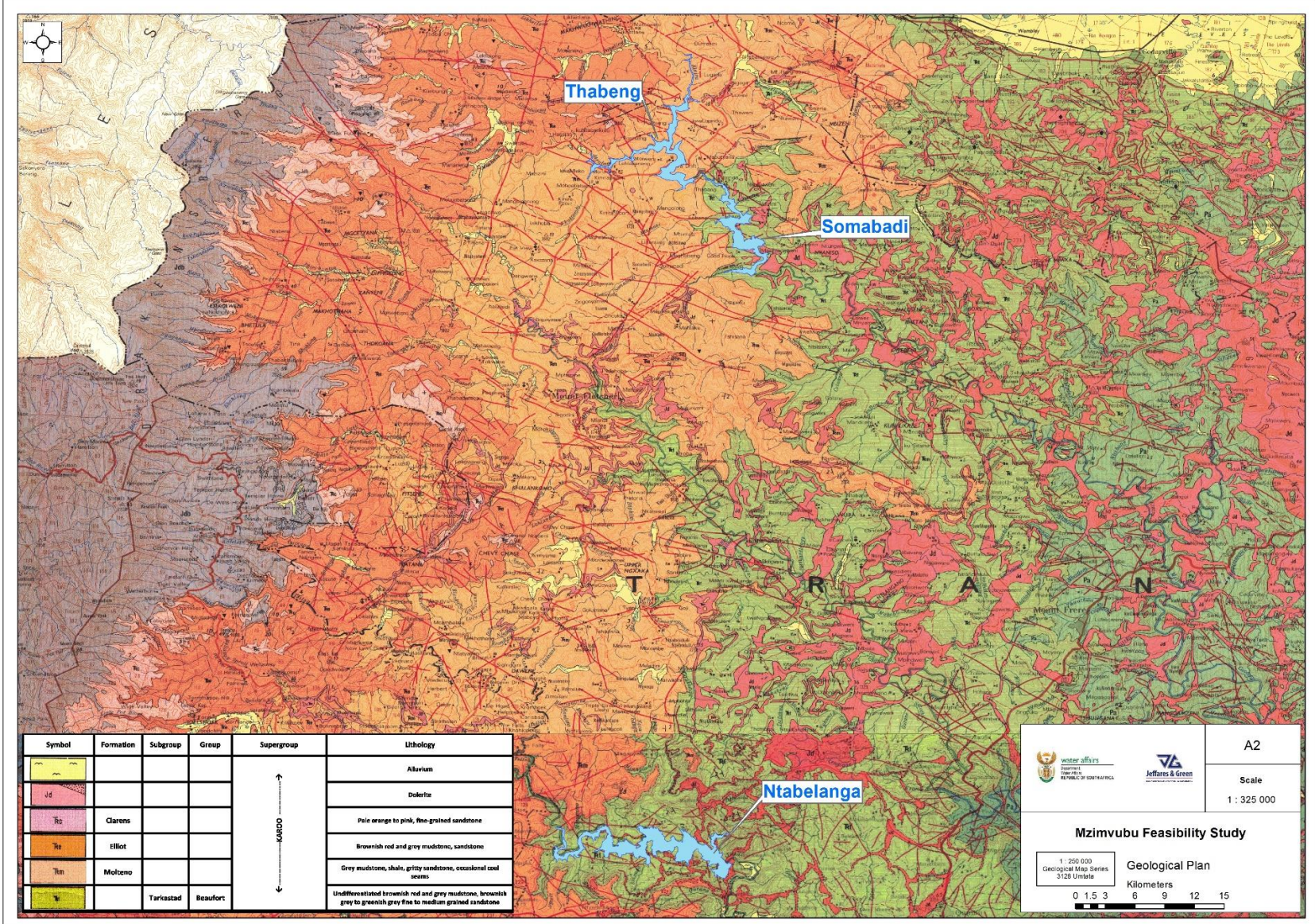


Fig A-2: Geological Plan



Fig A-3: Thabeng Dam Site Plan



Fig A-4: Somabadi Dam Site Plan

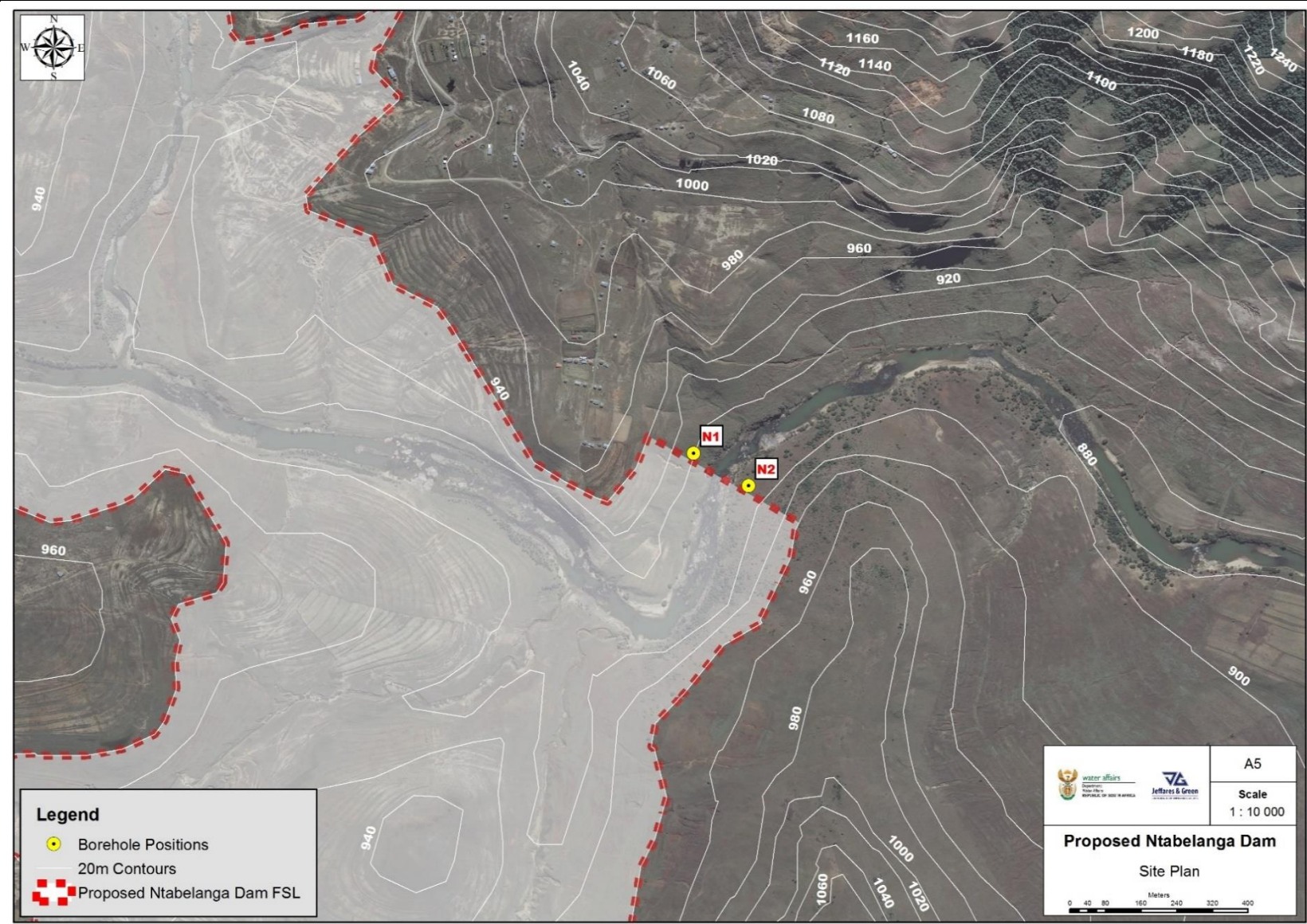


Fig A-5: Ntabelanga Dam Site Plan

APPENDIX B

PHASE 1 DAM SITE VISUAL APPRAISALS

B1:

THABENG DAM SITE

STAGE 1 GEOTECHNICAL ASSESSMENT

DAM SITE NAME: Thabeng

RIVER: Kinira

DAM LENGTH: Approx. 280m

DAM HEIGHT: Approx. 53m

GPS CO-ORD ON RIVER: S 30°29'45.51"; E 28°38'22.49"; ELEV. 1347m

APPROX C/L ORIENTATION: NW – SE

TOPOGRAPHY (valley shape, steepness)

LEFT FLANK:

Very steep to precipitous in places

RIVER SECTION:

Steep U-shaped profile. Both flanks rise steeply from the river.

RIGHT FLANK:

Steep, consistent to slightly convex slope.

GEOLOGICAL INFLUENCE:

Dolerite sill through river section and up the right flank. Dolerite on left flank is thinner and not as prevalent so that founding is likely to be in both dolerite and sandstone.

BASIN MORPHOLOGY:

Just upstream of the dam the river flows in a steep sided valley. Further upstream in the mid to upper backwater reaches the topography moderates. The geology comprises predominantly sandstone, as well as mudrock of the Molteno Formation.

GEOLOGY

OUTCROP:

Dolerite outcrop in the river section.

JOINTS (no, condition, spacing, orientation):

Orthogonal joints sets, two sub-vertical and one sub-horizontal. Comprise moderate and high angle subvertical joints that dip upstream and downstream respectively. Major strike direction is NW – SE.

STRUCTURAL FEATURES (dykes, faults, lineaments)

AERIAL PHOTOS, MAPS:

No apparent linear features suggesting faults or other structural lineaments. Stereoscopic aerial photographic interpretation was not undertaken, as the other information was deemed adequate.

OBSERVED:

Dolerite strike is NW – SE.

SOIL COVER:

Thin soil cover with sub-outcrop on the flanks.

FOUNDING, STABILITY, PROBLEM AREAS, OTHER:

Good founding on dolerite through the river section and right flank. The left flank is underlain by dolerite as well as by sandstone and intercalated mudrock. Pronounced bedding in the sedimentary rocks, whilst appearing tight, could lead to higher grout takes on the left flank.

BASIN GEOL:

Mainly sandstone with intercalated mudrock. Occasional dolerite dykes in the basin. Dolerite sills were only evident in the upper reaches of the basin.

CONSTRUCTION MATERIALS

CLAY:

No source of core material identified in the impoundment basin during this initial assessment, but the presence of mudrock of the Molteno Formation in the basin suggests that suitable core material is likely to be available. Mudrock of the Tarkastad Formation is plentiful downstream of the dam site. In addition, reddish brown, clayey colluvial soils associated with dolerite occur downstream of the dam.

SOIL / ROCK FILL:

Core trench excavation and dolerite rock quarry

SAND (concrete, filter):

River sand. Extensive deposits of sand occur upstream of the dam near to Kinira Drift.

ROCK (concrete, rip-rap):

Dolerite quarry. Initial indications suggest a paucity of suitable dolerite quarry sites in the basin, but there is an extensive body of dolerite downstream of the dam.

PROBLEM AREAS:

At this stage indications are that the most suitable sources of core and rock aggregate occur downstream of the dam, consequently with higher environmental impacts effecting their exploitation, as they would ultimately not be inundated following impoundment and would require rehabilitation.

INFRASTRUCTURE

ROADS:

A number of roads will be inundated including the R56, the Kinira Drift road and the road to Pontseng / Lekhalaneng.

HOUSES:

A water treatment works being constructed near Kinira Drift, as well as associated pipelines would be inundated. There is also a weir and gauging station at Kinira Drift.

CULTIVATION:

Due to the relatively narrow impoundment basin and limited cultivation, inundation of cultivated areas in the lower reaches would be limited. Inundation of cultivation would occur around Kinira Drift and possibly upstream of the main road.

FURTHER INVESTIGATIONS

BOREHOLES (where, access):

Rotary core drilling will be required along the dam centre-line, spillway, appurtenant structures and to prove a rock quarry. Access along the dam axis is difficult due to the steep topography.

TRIAL PITS (where, access):

Access for mechanical excavating equipment will be restricted along the dam centre-line due to the steep topography, especially along the left flank. This will be a limiting factor to the undertaking of centre-line trial pitting. Trial pits would be required to prove construction material volumes and quality.

GEOPHYSICS:

A seismic refraction survey is recommended along the dam axis, with transverse traverses at the positions of structures and to pick up stratigraphic dip.

OTHER:

Joint orientation surveys, stability analyses, aerial photographic interpretation if deemed necessary, rock strength testing, materials testing, water pressure testing and analysis of grouting requirements, dam and basin mapping.

Quarry and borrow pit investigations.

ADVANTAGES OF SITE:

Good valley profile, which lends itself to either earth-fill, rockfill or concrete dam construction.

Good founding on dolerite in the river section and right flank. The cut-off on the left flank is likely to be in a combination of dolerite and sedimentary rocks.

Joints in the dolerite appear to be tight, resulting in low seepage losses and low grout takes.

The basin topography contributes to a high storage to area ratio thereby minimising evaporation losses.

DISADVANTAGES OF SITE:

Difficult access due to steep valley sides, particularly along the left flank.

Based upon this initial assessment potential sources of core and rock aggregate do not appear to be readily available in the basin, although they occur a short distance downstream.

Inundation of infrastructure in the basin would occur, including a water treatment works currently under construction.

GENERAL

No fatal flaws were identified in respect of the dam site and founding conditions.

The valley profile is suitable for an earth embankment, rockfill or concrete dam.

This suitability assessment is based solely on geotechnical parameters and does not consider the other interrelated criteria such as hydrology, engineering or socio-economic factors. It also does not consider the site location relative to end user requirements.

B2:

SOMABADI DAM SITE

STAGE 1 GEOTECHNICAL ASSESSMENT

DAM SITE NAME: Somabadi

RIVER: Kinira

DAM LENGTH: Approx. 630m

DAM HEIGHT: Approx. 59m

GPS CO-ORD ON RIVER: S 30°34'59.79"; E 28°41'35.5"; ELEV. 1276m

APPROX C/L ORIENTATION: NE – SW

TOPOGRAPHY (valley shape, steepness)

LEFT FLANK:

Initially steep and then a wide terrace and again becoming steep

RIVER SECTION:

U-shaped. Steep banks.

RIGHT FLANK:

Very steep, consistent slope

GEOLOGICAL INFLUENCE:

Sandstone outcrop in the riverbed and in the river banks. Sub-outcrop of sandstone on the right flank and a major proportion of the left flank. Dolerite occurs on the upper left flank.

BASIN MORPHOLOGY:

Variable, ranging from steep valley sides to moderately flat.

GEOLOGY

OUTCROP:

Sandstone outcrop in the river section.

JOINTS (no, condition, spacing, orientation):

Pronounced bedding in the sandstone dipping at a low angle in a downstream direction.

STRUCTURAL FEATURES (dykes, faults, lineaments)

AERIAL PHOTOS, MAPS: No observed linear features to suggest faults or structural lineaments.

OBSERVED: None.

SOIL COVER: Generally thin

FOUNDING, STABILITY, PROBLEM AREAS, OTHER:

Good founding on sandstone. Pronounced bedding partings are potentially conducive to seepage losses and may result in relatively high grout takes.

BASIN GEOL:

Tarkastad Formation sandstone and mudrock, with intrusive dolerite.

CONSTRUCTION MATERIALS

CLAY:

Mudrock occurs in abundance in the basin. Red-brown colluvial soils of doleritic origin occur in abundance on the high lying area to the north-east of the dam.

SOIL / ROCK FILL:

Sandstone and dolerite from foundation excavations and a rock quarry. An elevated saddle on the left flank could be excavated to create an off-channel spillway and to generate dolerite material.

SAND (concrete, filter):

River sand from upstream, of which there are a number of deposits

ROCK (concrete, rip-rap):

Dolerite quarry.

PROBLEM AREAS:

No apparent problems in respect of materials.

INFRASTRUCTURE

ROADS:

A number of roads would be inundated.

HOUSES:

This was not ascertained in this assessment.

CULTIVATION:

Extensive areas of cultivation in the basin would be inundated.

BOREHOLES (where, access):

Rotary core drilling would be required along the dam axis, spillway, appurtenant structures and to prove potential rock quarry sites. Drilling could possibly also be undertaken in the saddle area adjacent to the upper left flank to prove the feasibility of creating an off-channel spillway, which could duplicate as a rock quarry.

TRIAL PITS (where, access):

Difficult access along most of the dam axis, especially the right flank may curtail the successful undertaking of trial pits along the entire dam axis. Trial pits would be required to investigate appurtenant works and to prove borrow pits.

GEOPHYSICS:

Seismic refraction traverses along and transverse to the dam axis.

OTHER:

Joint orientation surveys, stability analyses, rock strength testing, materials testing, water pressure testing, dam and basin mapping, aerial photographic interpretation if deemed necessary, quarry and borrow pit investigations.

ADVANTAGES OF THE SITE:

Good valley profile.

Good founding on sandstone.

A saddle adjacent to the upper left flank has the potential to be excavated as a rock quarry and to serve as an off-channel spillway. Further investigation would be required to verify the feasibility of this.

Construction materials appear to be readily available within relatively close proximity to the dam.

DISADVANTAGES OF THE SITE:

There is difficult access along the dam axis due to steep valley sides.

Pronounced bedding planes imply possible high grout takes.

Inundation of roads and cultivation would occur.

GENERAL

No fatal flaws identified.

The valley profile and founding conditions are suitable for a number of dam alternatives including earth embankment, rockfill and concrete.

This assessment entailed a suitability assessment based solely on geotechnical parameters. It does not consider the other inter-related criteria, such as hydrology, engineering and socio-economic aspects that will ultimately influence the feasibility of this site. It also does not consider the site location relative to end-user requirements.

B3:

NTABELANGA DAM SITE

STAGE 1 GEOTECHNICAL ASSESSMENT

DAM SITE NAME: Ntabelanga

RIVER: Tsitsa

DAM LENGTH: Approx. 350m

DAM HEIGHT: Approx. 53m

GPS CO-ORD ON RIVER: S31°07'01.18"; E 28°40'20.7"; ELEV. 898m

APPROX C/L ORIENTATION: NW – SE

TOPOGRAPHY (valley shape, steepness)

LEFT FLANK:

Steep consistent to slightly convex slope rising from the river

RIVER SECTION:

U-shaped profile with the channel skewed towards the left flank. Dolerite outcrop across the river and in the left bank. Steep incline up the left flank. Gentle to moderately sloping terrace extends from the right bank, thereafter steepening up the right flank.

RIGHT FLANK:

There is a narrow terrace extending from the river bank, steepening into a concavo-convex slope at the bottom becoming convex, at a generally steep gradient.

GEOLOGICAL INFLUENCE:

Dolerite sill outcropping in the river section. Dolerite outcrop and sub-outcrop up the right flank. Dolerite on the left flank occurs beneath a cover of soil. The top of the left flank is underlain by sandstone.

BASIN MORPHOLOGY:

Variable topography comprising mainly sedimentary rocks of the Tarkastad Formation, with dolerite intrusions generally forming positive relief features.

GEOLOGY

OUTCROP:

Dolerite outcrops in the river section and on the mid to upper right flank

JOINTS (no, condition, spacing, orientation):

Three main orthogonal joints sets, two sub-vertical and one sub-horizontal. Sub-vertical joints comprise an obliquely striking joint dipping steeply upstream and a diagonal, near-vertical joint. The sub-horizontal joint dips moderately from right to left.

STRUCTURAL FEATURES (dykes, faults, lineaments)

AERIAL PHOTOS, MAPS:

No observed linear features to suggest faults or structural lineaments. Stereoscopic aerial photo interpretation on stereo-pairs was not undertaken, as the existing information was deemed adequate.

OBSERVED:

There is a cross-cutting dolerite sill and valley constriction at the dam site. No linear features observed in the vicinity of the dam.

SOIL COVER:

Thin to moderate soil cover on the left flank. The river terrace on the right flank is covered by alluvium, comprising soil and boulders of unknown thickness. The mid to upper right flank is characterised by dolerite outcrop and sub-outcrop.

FOUNDING, STABILITY, PROBLEM AREAS, OTHER:

Founding conditions appear to be good. Based upon the surface indications it is presumed that the cut-off will be in dolerite bedrock at relatively shallow depth. Foundations on the upper left flank will be in sandstone. Inundation and resultant saturation could induce small-scale slope instability in the left hand side river bank a few hundred metres upstream of the dam.

BASIN GEOLOGY:

Mainly sedimentary rocks, comprising mudrock and sandstone.

CONSTRUCTION MATERIALS

CLAY:

Purple mudrock occurs in abundance in the basin just upstream of the dam. Reddish brown colluvial soil of doleritic origin are also evident in the basin just upstream of the dam.

SOIL / ROCK FILL:

Dolerite rock / weathered dolerite from the dam foundations, as well as from potential dolerite quarry sites in the basin upstream of the dam. Sandstone and possibly mudrock could be considered for use as embankment fill.

SAND (concrete, filters):

River sand from upstream. Whilst high river flow at the time of the assessment prevented a detailed assessment, there appears to be a potential source of alluvial sand upstream of the dam in the vicinity of the low level bridge crossing. A further reconnaissance is required during periods of low flow to optimise location.

ROCK (concrete, rip-rap, filters):

Dolerite occurs in relative abundance in the basin and it is recommended that further reconnaissance be undertaken to identify a potential dolerite quarry within the basin. There also appears to be potential for forming the top of the right flank into an off-channel spillway with the excavation duplicating as a rock quarry.

PROBLEM AREAS:

No apparent problems in respect of materials.

INFRASTRUCTURE

ROADS:

Roads, including an upstream river crossing would be inundated.

HOUSES:

The effect on houses was not ascertained as the FSL had not been delineated.

CULTIVATION:

Extensive areas of cultivation would be inundated.

BOREHOLES (where, access):

Rotary core drilling would be required along the dam axis, at the spillway, structures and to prove a rock quarry. Both flanks are steep, necessitating difficult skid set-ups.

TRIAL PITS (where, access):

Trial pits by means of an excavator / TLB along the dam centre-line and in potential borrow pits. Machine access to both flanks, particularly the left flank, will be extremely difficult and may preclude trial pits along sections of the dam axis.

GEOPHYSICS:

A seismic refraction survey with traverses orientated parallel and transverse to the dam centre-line and to include the positions of the spillway, intake and outlet works.

OTHER:

Joint orientation surveys, stability analyses, possibly aerial photographic interpretation if subsequently deemed necessary, dam and basin mapping to identify potential problems and influence factors, rock strength testing, materials testing, water pressure testing and analysis of grouting requirements.

Quarry and borrow pit investigations.

ADVANTAGES OF THE SITE:

Good valley profile.

Good founding on dolerite, with indications of a relatively shallow cut-off.

Whilst joints are high angle, they appear tight, so that seepage losses and grout takes are not expected to be excessive.

Whilst requiring further assessment, excavating an off-channel spillway into the right flank could double as a rock quarry.

Construction materials appear to be readily available in the basin.

DISADVANTAGES OF THE SITE:

Access along the dam axis for mechanical plant will generally be difficult due to steep valley sides. There will be inundation of cultivation and roads in the basin.

GENERAL

No fatal flaws identified.

The observed conditions in respect of the site cross-sectional profile and the apparent founding conditions appear to lend themselves to a number of dam options, namely earthfill, rockfill or concrete.

This assessment entailed a suitability assessment based solely on geotechnical parameters. It does not consider the other inter-related criteria, such as hydrology, engineering and socio-economic aspects that will ultimately influence the feasibility of this site. It also does not consider the site location relative to end-user requirements.

APPENDIX C

PHASE 1 ROTARY CORE DRILLING INVESTIGATION

C1:

THABENG DAM SITE

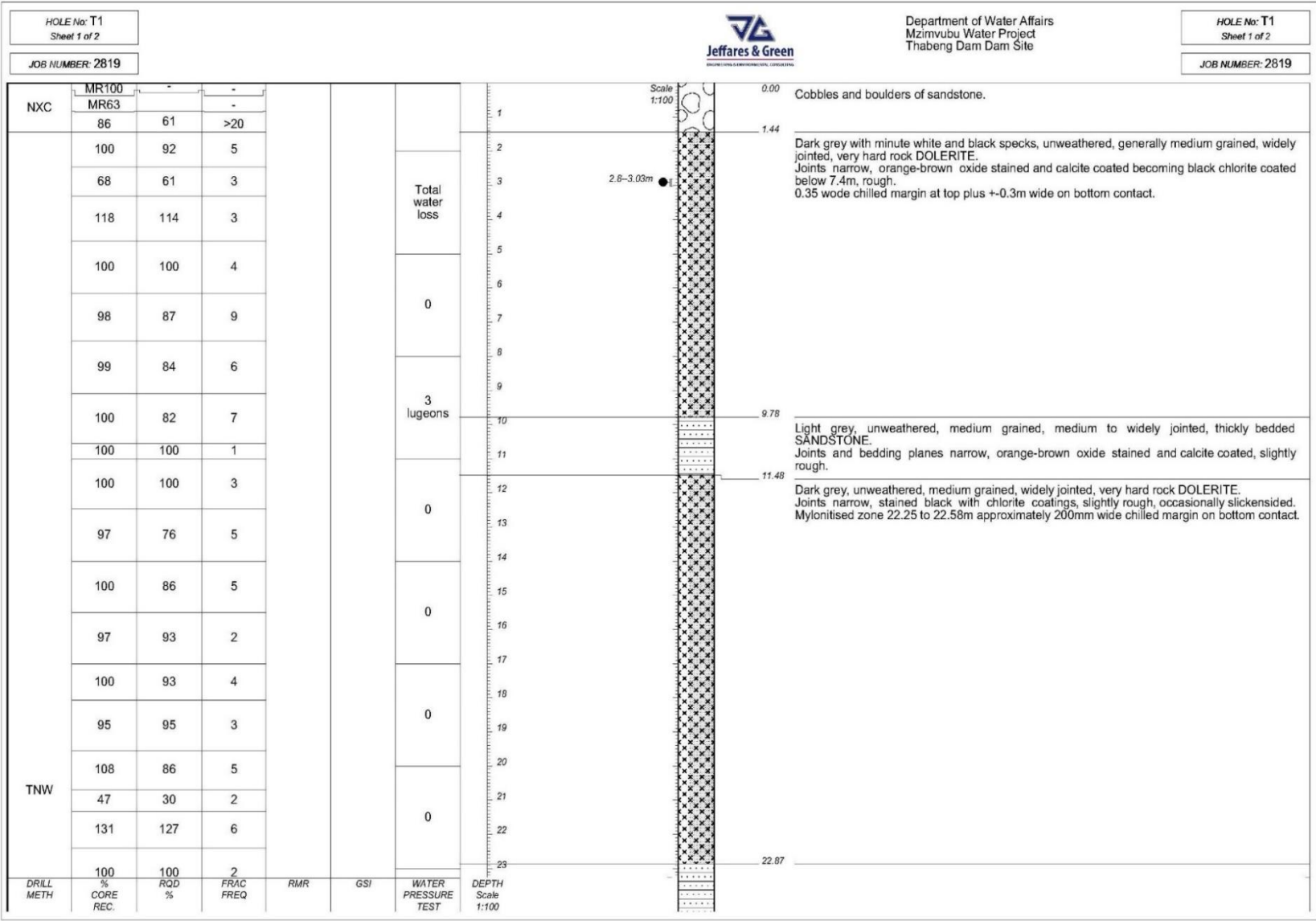


Fig C-1.1: Borehole Logs (T1)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

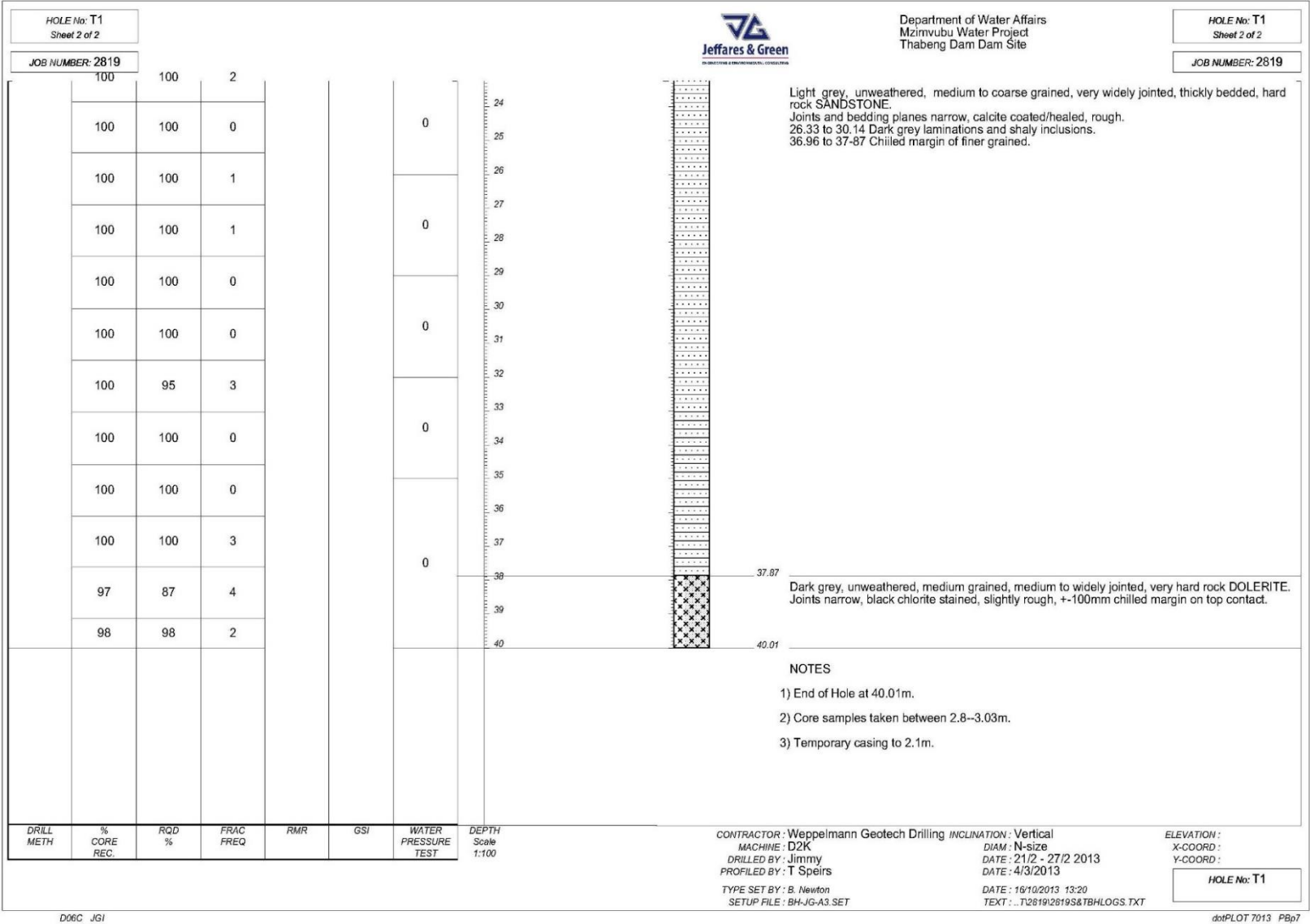


Fig C-1.2: Borehole Logs (T1)



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Report on Waterpressure Testing

SCHEME: Mzimvubu Water Project

BOREHOLE NR: T 1

DRILLER: Jimmy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESSURES	PRESURES	WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
Double	FROM: 5.00m	10min	45	45	54676.2-54749.7= 73.5lt
		10min	80	80	54753.8-54842.6= 88.8lt
	TO: 8.00m	10min	115	115	54847.8-54931.8= 84lt
		10min	80	80	54933.9- 54941.3= 7.4lt
		10min	45	45	54942.3-54959.3= 1.7lt
Double	FROM: 8.00m	10min	70	70	10lt
		10min	130	130	76.7lt
	TO: 11.00m	10min	180	180	79.5lt
		10min	130	130	13.1lt
		10min	70	70	4.7lt
Double	FROM: 11.00m	10min	100	100	4.3lt
		10min	170	170	6.9lt
	TO: 14.00m	10min	250	250	2.6lt
		10min	170	170	2.7lt
		10min	100	100	1.7lt
Double	FROM: 14.00m	10min	125	125	4.1lt
		10min	220	220	1.6lt
	TO: 17.00m	10min	320	320	3.2lt
		10min	220	220	1.9lt
		10min	125	125	0lt
Double	FROM: 17.00m	10min	155	155	0lt
		10min	270	270	0lt
	TO: 20.00m	10min	385	385	0lt
		10min	270	270	0lt
		10min	155	155	0lt
Double	FROM: 20.00m	10min	180	180	0lt
		10min	320	320	0lt
	TO: 23.00m	10min	450	450	0lt
		10min	320	320	0lt
		10min	180	180	0lt
Double	FROM: 23.00m	10min	210	210	0lt
		10min	365	365	0lt
	TO: 26.00m	10min	520	520	0lt
		10min	365	365	0lt
		10min	210	210	0lt
Double	FROM: 26.00m	10min	235	235	0lt
		10min	410	410	0lt
	TO: 29.00m	10min	590	590	0lt
		10min	410	410	0lt
		10min	235	235	0lt
Double	FROM: 29.00m	10min	265	265	0lt
		10min	460	460	2.5lt
	TO: 32.00m	10min	655	655	52.3lt
		10min	460	460	5.6lt
		10min	265	265	0lt
Double	FROM: 32.00m	10min	290	290	55404.2-55404.2= 0lt
		10min	510	510	55407.5-55408.9= 1.4lt
	TO: 35.00m	10min	725	725	55416.3-55470.2= 59.9lt
		10min	510	510	55481.0-55523.2= 42.2lt
		10min	725	725	55525.4-55526.1= 0.7lt
Single	FROM: 35.00m	10min	315	315	55544.0-55544.0= 0lt
		10min	555	555	55548.5-55556.1= 7.6lt
	TO: END OF BOREHOLE	10min	790	790	55561.6-55581.6= 20.0lt
		10min	555	555	55585.8-55588.3= 4.5lt
		10min	315	315	55589.2-55590.9= 1.7lt

REMARKS: Total water loss 2.00m to 5.00m. (Water seepage pass packer due to weathered and fractures in rock)

Fig C-2: Water Pressure Testing Report (T1)



Fig C-3: Borehole T1 Core Box 1 of 6



Fig C-4: Borehole T1 Core Box 2 of 6



Fig C-5: Borehole T1 Core Box 3 of 6



Fig C-6: Borehole T1 Core Box 4 of 6



Fig C-7: Borehole T1 Core Box 5 of 6



Fig C-8: Borehole T1 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

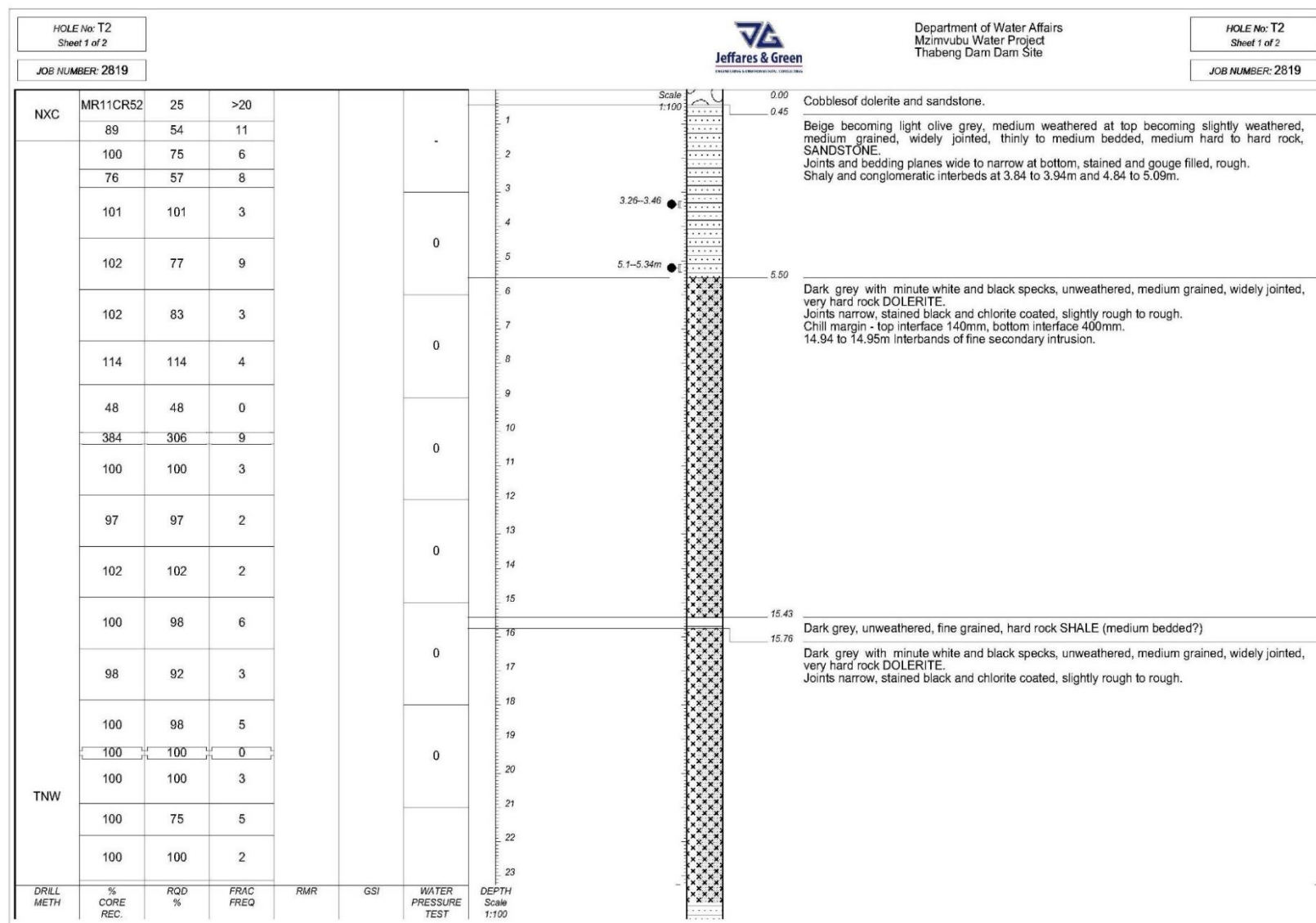


Fig C-9.1: Borehole Logs (T2)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

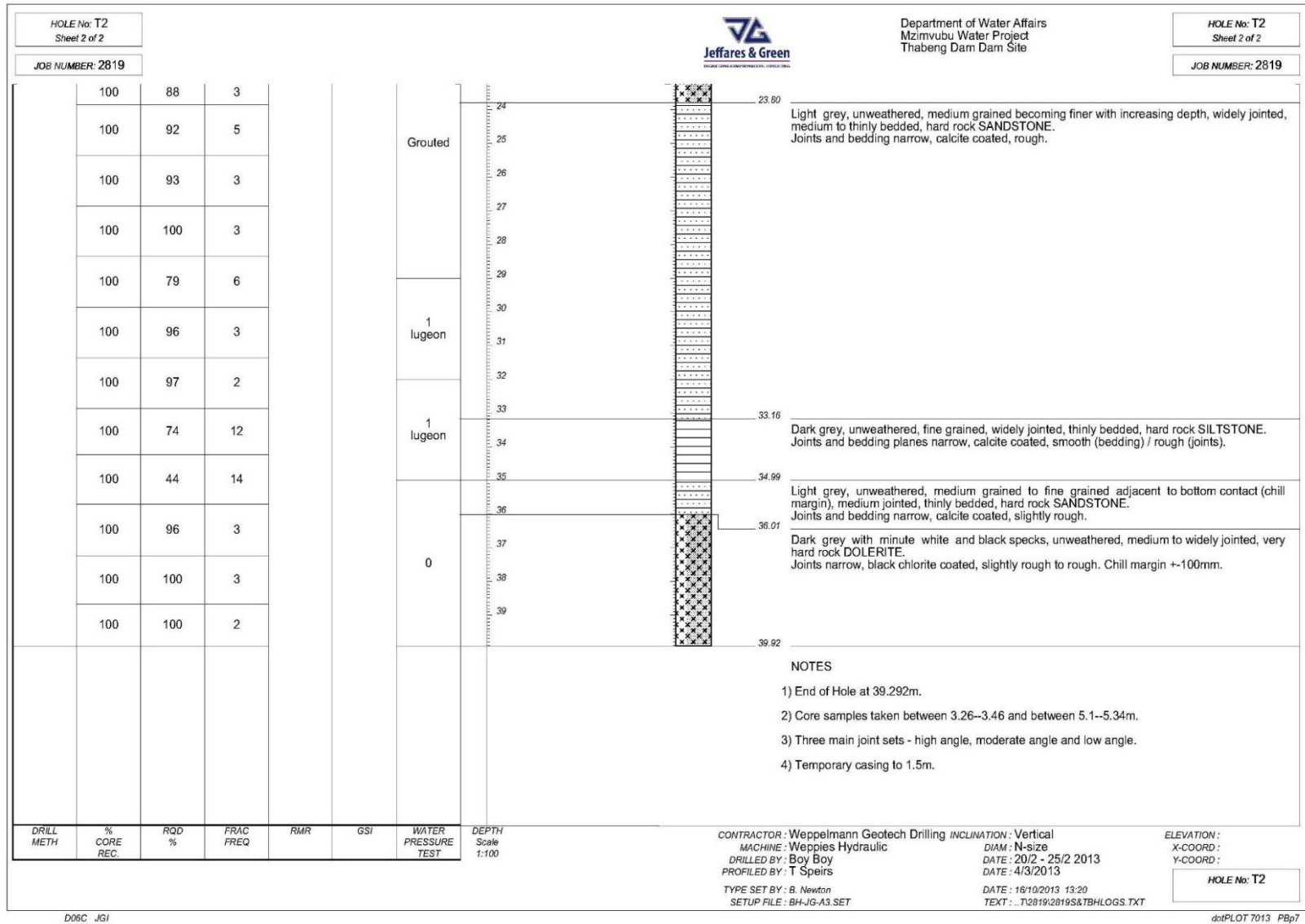


Fig C-9.2: Borehole Logs (T2)



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Report on Waterpressure Testing

SCHEME: Mzimvubu Water Project

BOREHOLE NR: T 2

DRILLER: Boy Boy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESSURES	PRESURES	WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
Double	FROM: 3.00m	10min	25	25	53659.9-53659.9= 0lt
		10min	50	50	53660.9-53660.9= 0lt
	TO: 6.00m	10min	70	70	53663.6-53663.6= 0lt
		10min	50	50	53667.1-53667.1= 0lt
		10min	25	25	53670.3-53670.3= 0lt
Double	FROM: 6.00m	10min	55	55	53683.5-53683.5= 0lt
		10min	95	95	53685.3-53685.3= 0lt
	TO: 9.00m	10min	135	135	53690.7-53690.7= 0lt
		10min	95	95	53692.3-53692.3= 0lt
		10min	55	55	53693.7-53693.7= 0lt
Double	FROM: 9.00m	10min	80	80	53705.7-53705.7= 0lt
		10min	140	140	53707.3-53707.3= 0lt
	TO: 12.00m	10min	200	200	53708.1-53708.1= 0lt
		10min	140	140	53710.5-53710.5= 0lt
		10min	80	80	53712.3-53712.3= 0lt
Double	FROM: 12.00m	10min	110	110	53723.4-53723.4= 0lt
		10min	190	190	53725.5-53725.5= 0lt
	TO: 15.00m	10min	270	270	53727.1-53727.1= 0lt
		10min	190	190	53729.6-53729.6= 0lt
		10min	110	110	53730.1-53730.1= 0lt
Double	FROM: 15.00m	10min	135	135	53743.8-53743.8= 0lt
		10min	240	240	53748.5-53748.5= 0lt
	TO: 18.00m	10min	340	340	53767.1-53767.1= 0lt
		10min	240	240	53760.6-53760.6= 0lt
		10min	135	135	53770.3-53770.3= 0lt
Double	FROM: 18.00m	10min	165	165	53784.7-53784.7= 0lt
		10min	285	285	53785.7-53785.7= 0lt
	TO: 21.00m	10min	405	405	53803.8-53826.4= 22.6lt
		10min	285	285	53832.6-53832.6= 0lt
		10min	165	165	53838.0-53838.1= 0.1lt
Double	FROM: 21.00m	10min	265	265	53848.4-53848.4= 0lt
		10min	460	460	53858.6-53906.1= 47.5lt
	TO: 24.00m	10min	655	450	53910.5-53964.0= 47.5lt
		10min	460	400	53970.9-54025.5= 54.6lt
		10min	265	265	54030.4-54034.1= 3.7lt
Double	FROM: 24.00m	10min	290	290	54047.8-54051.8= 4lt
		10min	510	500	54101.6-54161.0= 59.4lt
	TO: 27.00m	10min	725	500	54165.8-54232.4= 66.6lt
		10min	510	500	54240.8-54273.4= 32.6lt
		10min	290	290	54276.5-54284.7= 8.2lt
Single	FROM: 27.00m	10min	315	315	54296.5-54302.4= 5.9lt
		10min	555	450	54313.4-54401.7= 88.3lt
	TO: END OF BOREHOLE	10min	790	450	54411.9-54499.6= 87.7lt
		10min	555	450	54508.1-54592.5= 84.4lt
		10min	315	315	54595.9-54607.1= 11.2lt

REMARKS: Water seepage pass packer out the borehole; 29.00m to 32.00m= 30lt; 32.00m to 35.00m= 30lt
 35.00m to end of borehole = 40lt

Grout from 21.00m to 29.00m see drilling journal did not pressure test at this depth

Fig C-10 Water Pressure Testing Report (T2)



Fig C-11: Borehole T2 Core Box 1 of 6



Fig C-12: Borehole T2 Core Box 2 of 6



Fig C-13: Borehole T2 Core Box 3 of 6



Fig C-14: Borehole T2 Core Box 4 of 6



Fig C-15: Borehole T2 Core Box 5 of 6



Fig C-16: Borehole T2 Core Box 6 of 6

C2:

SOMABADI DAM SITE

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

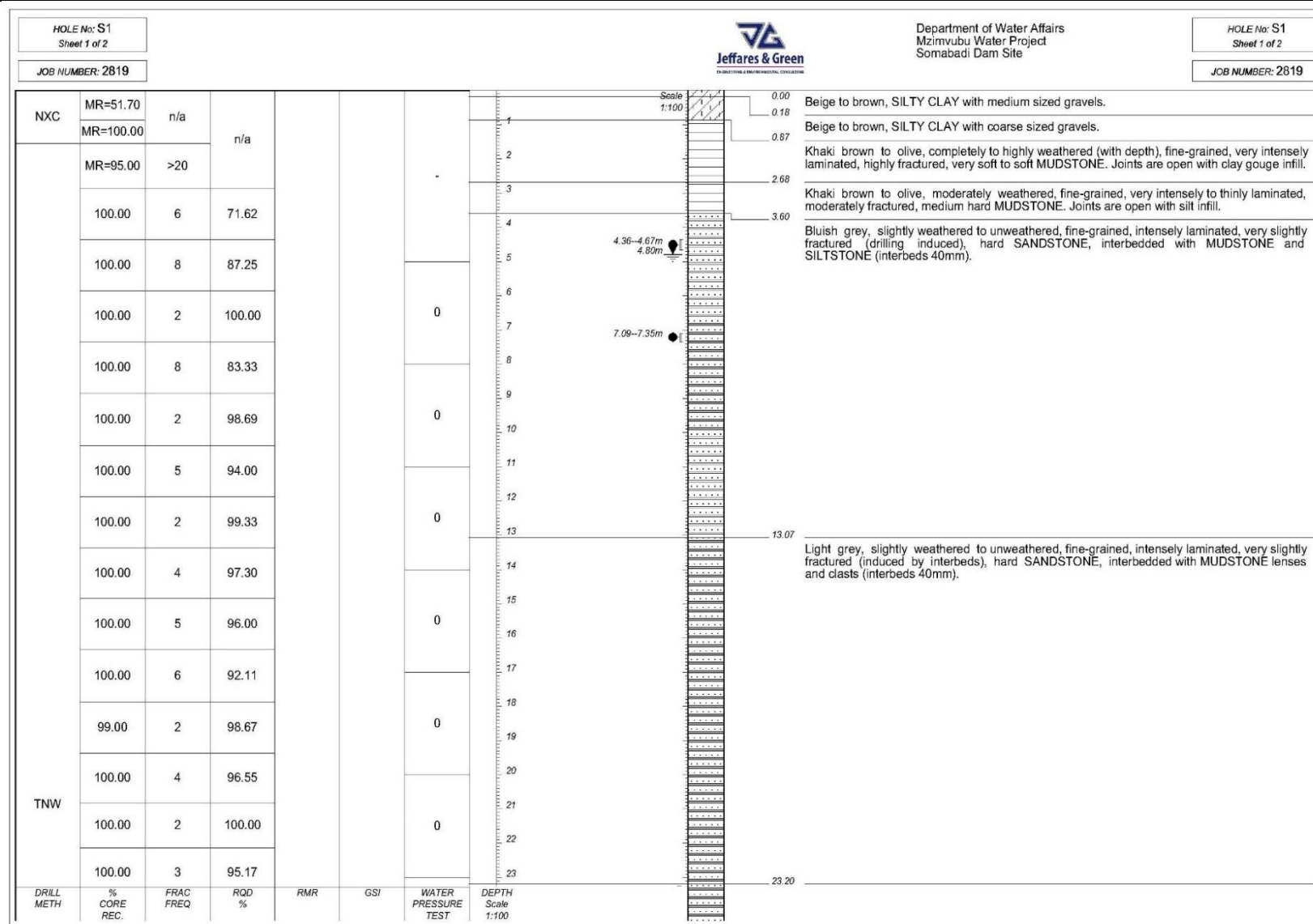


Fig C-17.1: Borehole Logs (S1)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

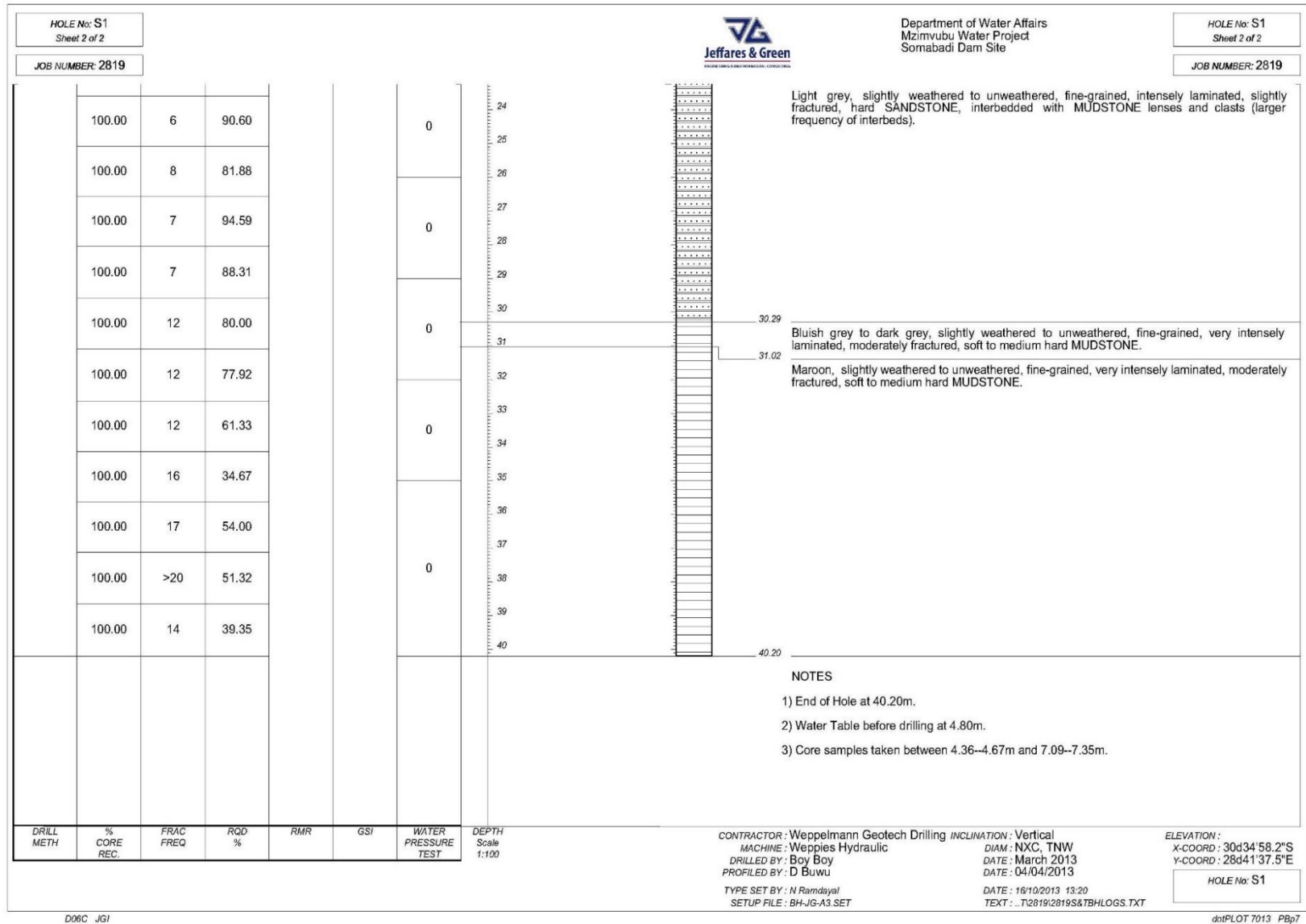


Fig C-17.2: Borehole Logs (S2)



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Report on Waterpressure Testing

SCHEME: Mzimvubu Water Project

BOREHOLE NR: S 1

DRILLER: Boy Boy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESURES		WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
22/03/2013 Double	FROM: 5.00m	10 min	45 kpa		0
		10 min	80		0
	TO: 8.00m	10 min	115		0
		10 min	80		0
		10 min	45		0
Double	FROM: 8.00m	10 min	70 kpa		0
		10 min	130		0
	TO: 11.00m	10 min	180		0
		10 min	130		0
		10 min	70		0
Double	FROM: 11.00m	10 min	100 kpa		0
		10 min	170		0
	TO: 14.00m	10 min	250		0
		10 min	170		0
		10 min	100		0
Double	FROM: 14.00m	10 min	125 kpa		0
		10 min	220		0
	TO: 17.00m	10 min	320		0
		10 min	220		0
		10 min	123		0
Double	FROM: 17.00m	10 min	155 kpa		0
		10 min	270		0
	TO: 20.00m	10 min	385		0
		10 min	270		0
		10 min	155		0
Double	FROM: 20.00m	10 min	180 kpa		0
		10 min	320		0
	TO: 23.00m	10 min	450		0
		10 min	320		0
		10 min	180		0
Double	FROM: 23.00m	10 min	210 kpa		0
		10 min	365		0
	TO: 26.00m	10 min	520		0
		10 min	365		0
		10 min	210		0
Double	FROM: 26.00m	10 min	235 kpa		0
		10 min	410		0
	TO: 29.00m	10 min	590		0
		10 min	410		0
		10 min	235		0
Double	FROM: 29.00m	10 min	265 kpa		0
		10 min	460		0
	TO: 32.00m	10 min	655		0
		10 min	460		0
		10 min	265		0
23/03/2013 Double	FROM: 32.00m	10 min	290 kpa		0
		10 min	510		0
	TO: 35.00m	10 min	725		0
		10 min	510		0
		10 min	290		0
Single	FROM: 35.00m	10 min	315 kpa		0
		10 min	555		0
	TO: 40.20m	10 min	790		0
	END OF HOLE	10 min	555		0
		10 min	315		0
REMARKS:					

Fig C-18: Water Pressure Testing Report (S1)



Fig C-19: Borehole S1 Core Box 1 of 6



Fig C-20: Borehole S1 Core Box 2 of 6



Fig C-21: Borehole S1 Core Box 3 of 6



Fig C-22: Borehole S1 Core Box 4 of 6



Fig C-23: Borehole S1 Core Box 5 of 6



Fig C-24: Borehole S1 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
 GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

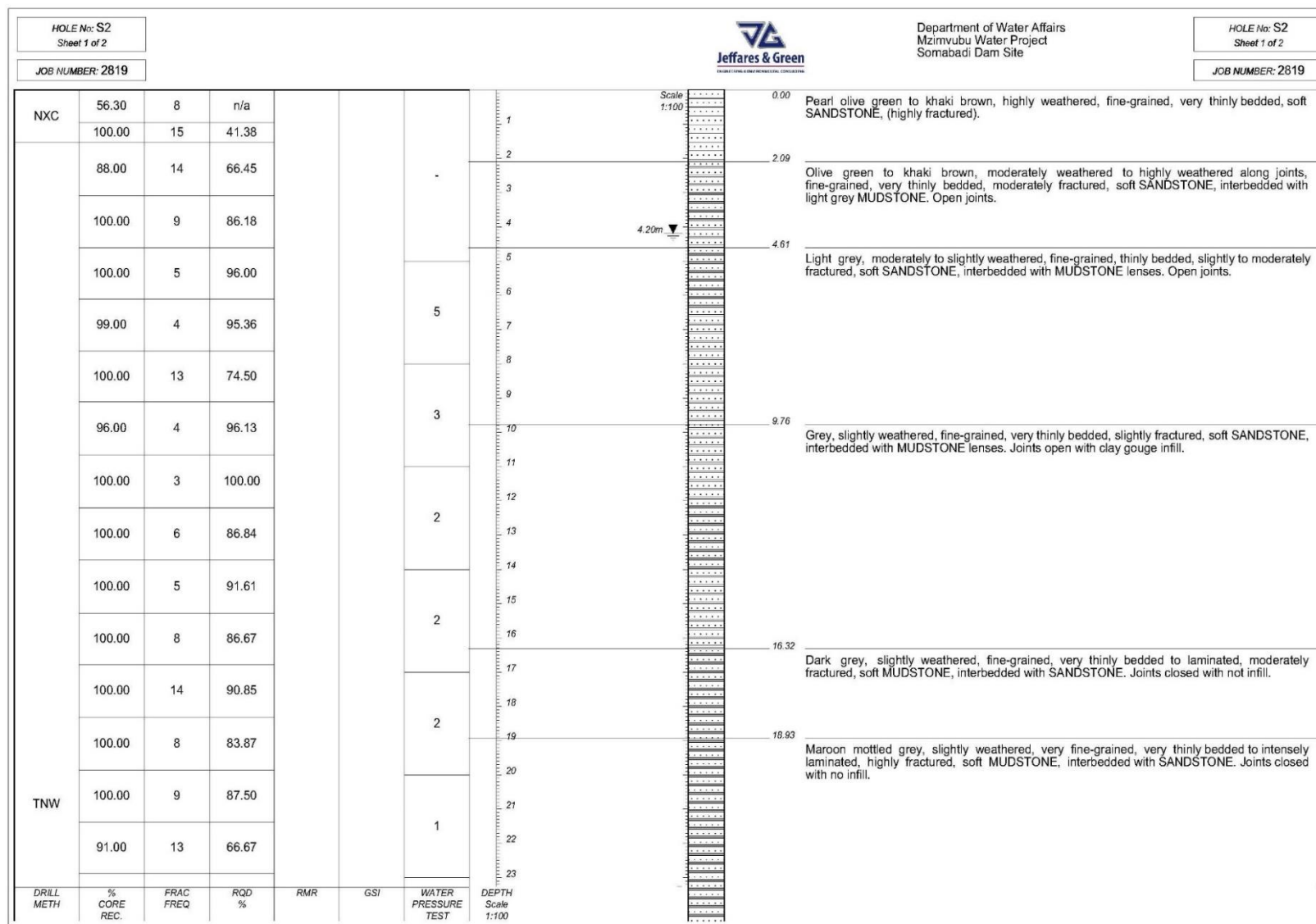


Fig C-25.1: Borehole Logs (S2)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

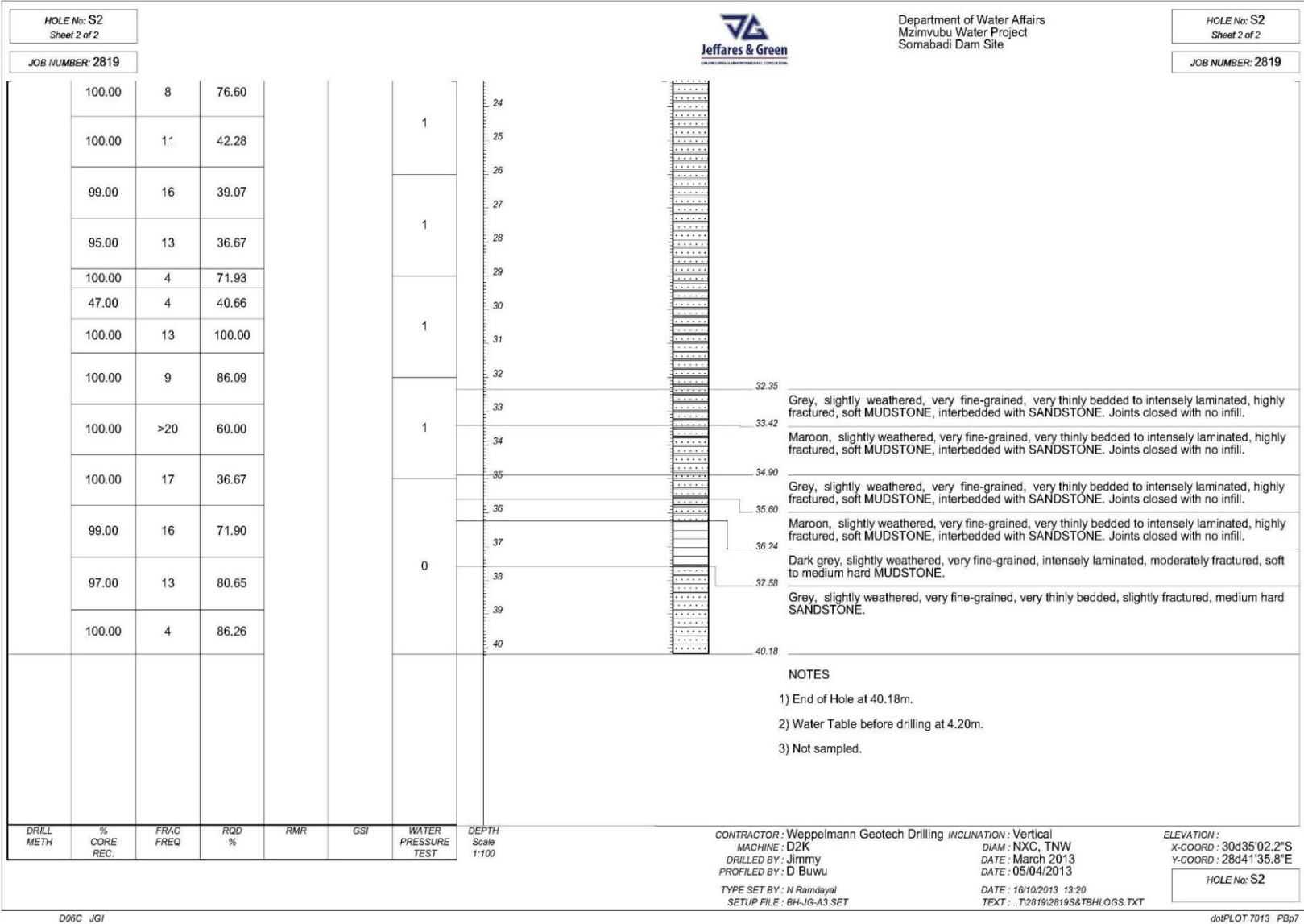


Fig C-25.2: Borehole Logs (S2)



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Report on Waterpressure Testing

SCHEME: Mzimvubu Water Project

BOREHOLE NR: S 2

DRILLER: Jimmy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESSURES	PRESURES	WATER INTAKE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
25/03/2013 Double	FROM: 5.00m	10 min	45 kpa		0
		10 min	80		0
	TO: 8.00m	10 min	115		0
		10 min	80		0
		10 min	45		0
Double	FROM: 8.00m	10 min	70 kpa		0
		10 min	130		0
	TO: 11.00m	10 min	180		0
		10 min	130		0
		10 min	70		0
Double	FROM: 11.00m	10 min	100 kpa		0
		10 min	170		0
	TO: 14.00m	10 min	250		0
		10 min	170		0
		10 min	100		0
Double	FROM: 14.00m	10 min	125 kpa		0
		10 min	220		0
	TO: 17.00m	10 min	320		0
		10 min	220		0
		10 min	125		0
Double	FROM: 17.00m	10 min	155 kpa		0
		10 min	270		0
	TO: 20.00m	10 min	385		0
		10 min	270		0
		10 min	155		0
Double	FROM: 20.00m	10 min	180 kpa		0
		10 min	320		0
	TO: 23.00m	10 min	450		0
		10 min	320		0
		10 min	180		0
Double	FROM: 23.00m	10 min	210 kpa		0
		10 min	365		0
	TO: 26.00m	10 min	520		0
		10 min	365		0
		10 min	210		0
Double	FROM: 26.00m	10 min	235 kpa		0
		10 min	410		0
	TO: 29.00m	10 min	590		0
		10 min	410		0
		10 min	235		0
Double	FROM: 29.00m	10 min	265 kpa		0
		10 min	460		0
	TO: 32.00m	10 min	655		0
		10 min	460		0
		10 min	265		0
26/03/2013 Double	FROM: 32.00m	10 min	290 kpa	290 kpa	88
		10 min	510	290	84.2
	TO: 35.00m	10 min	775	290	107.3
		10 min	510	290	80.5
		10 min	290	290	70.1
Single	FROM: 35.00m	10 min	315 kpa	200 kpa	104.8
		10 min	555	200	123.8
	TO: 40.18m	10 min	790	200	158.5
	END OF HOLE	10 min	555	200	115
		10 min	315	200	112
REMARKS:					

Fig C-26: Water Pressure Testing Report (S2)



Fig C-27: Borehole S2 Core Box 1 of 6



Fig C-28: Borehole S2 Core Box 2 of 6



Fig C-29: Borehole S2 Core Box 3 of 6



Fig C-30: Borehole S2 Core Box 4 of 6



Fig C-31: Borehole S2 Core Box 5 of 6



Fig C-32: Borehole S2 Core Box 6 of 6

C3:

NTABELANGA DAM SITE

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

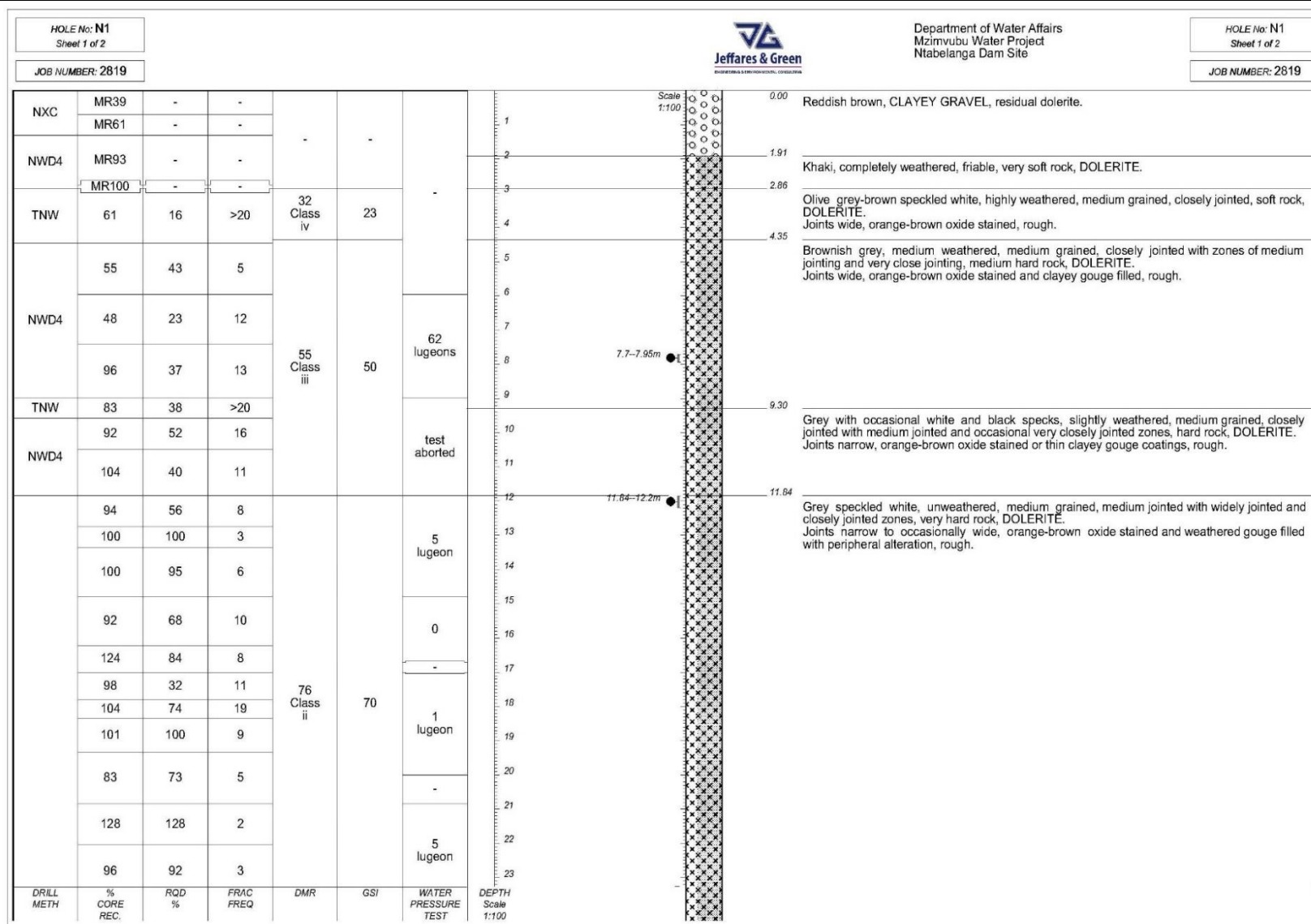


Fig C-33.1: Borehole Logs (N1)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

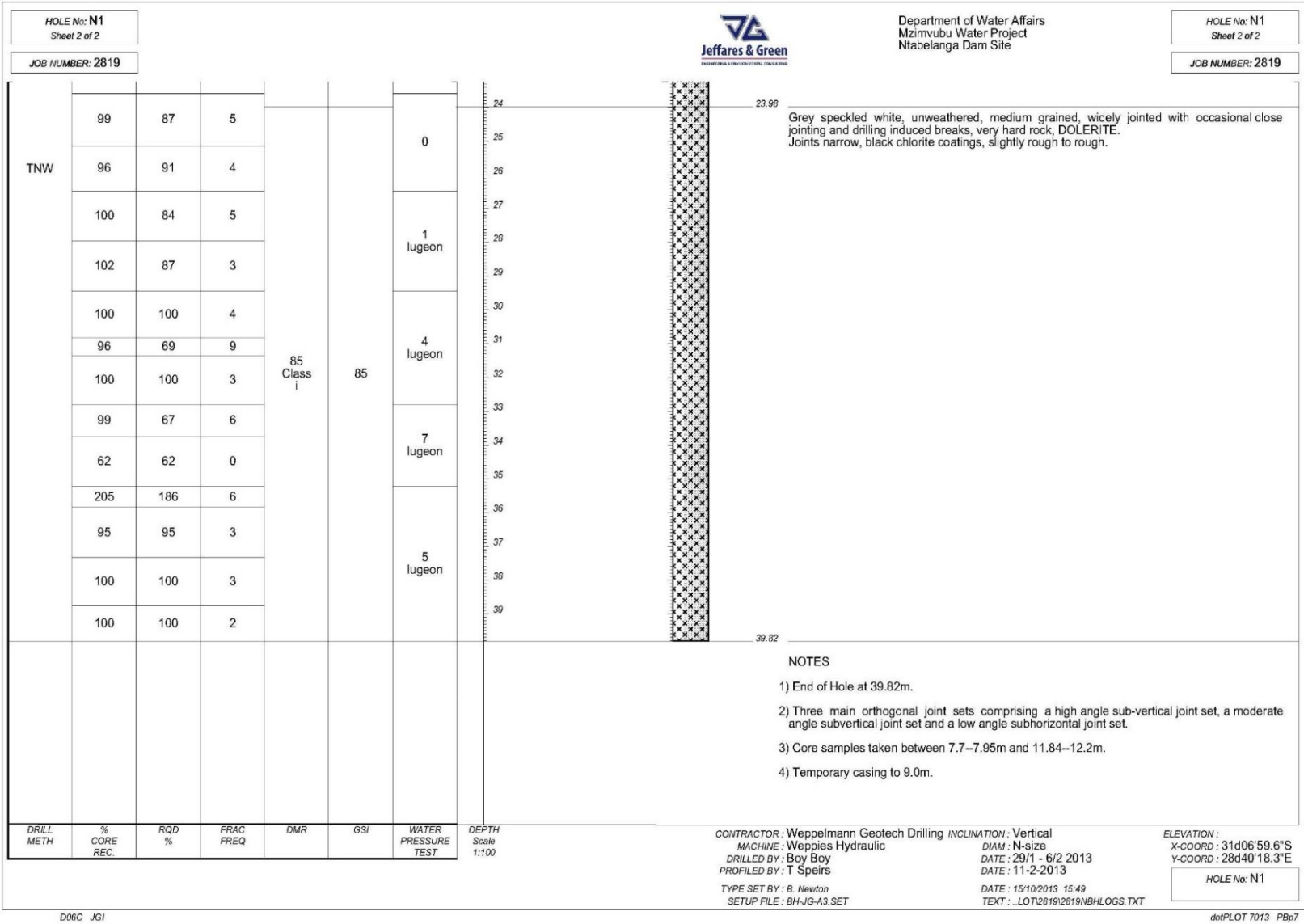


Fig C-33.2: Borehole Logs (N1)



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Report on Waterpressure Testing

SCHEME: Mzimvubu Water Project

BOREHOLE NR: N 1

DRILLER: Martin

DATE & Packer Description	STAGES	TESTING TIME	GAUGE REQUIRED PRESSURES	PRESURES ACTUAL PRESSURES	WATER INTAKE BY HOLE TOTAL LITRES
	METERS	REQUIRED MINUTES			
Single	FROM: 5.96m	10min	45	45	47063.2-47080.8= 17.6lt
		10min	80	50	47189.1-47300.5= 111.4lt
	TO: 8.98m	10min	115	50	47321.3-47394.3= 73 lt
		10min	80	80	47405.6-47472.1= 66.5lt
		10min	45	45	47467.3-47558.5= 84.9lt
Single	FROM: 8.98m	10min	80	80	
		10min	140	140	Packer could not seat
	TO: 11.84m	10min	200	200	in hole water seeping
		10min	140	140	out of borehole
		10min	80	80	
Single	FROM: 11.84m	10min	110	110	47908.6-47917.6= 9 lt
		10min	190	190	47929.7-47955.4= 25.7lt
	TO: 14.79m	10min	270	270	47957.5-48011.2= 53.7lt
		10min	190	190	48017.2-48049.7= 32.5lt
		10min	110	110	48050.8-48064.6= 13.8lt
Single	FROM: 14.79m	10min	135	135	48070.6-48070.6= 0lt
		10min	240	240	48077.6-48078.6= 10lt
	TO: 16.71m	10min	340	340	48085.3-48089.3= 4lt
		10min	240	240	48091.2-48091.2= 0lt
		10min	135	135	48097.1-48097.1= 0lt
Single	FROM: 17.00m	10min	155	155	48105.6-48126.6= 21 lt
		10min	270	270	48135.3-48238.6= 103lt
	TO: 20.00m	10min	385	300	48248.9-48335.1= 86.2lt
		10min	270	270	48339.6-48339.9= 0.3lt
		10min	155	155	48342.1-48348.8= 6.7lt
Double	FROM: 20.84m	10min	190	190	48349.5-48349.6= 0.1lt
	21.00m	10min	330	330	48357.5-48363.9= 6.4lt
	TO: 23.59m	10min	475	400	48369.5-48446.0= 76.5lt
	23.50m	10min	330	330	48454.5-48537.7= 83.2lt
		10min	190	190	48522.2-48547.4= 25.2lt
Single	FROM: 23.59m	10min	215	215	48556.5-48556.8= 0.3lt
	23.50m	10min	370	370	48561.2-48561.2= 0lt
	TO: 26.48m	10min	530	530	48567.4-48568.4= 1lt
	26.50m	10min	370	370	48575.6-48575.6= 0lt
		10min	215	215	48579.7-48579.7= 0lt
Double	FROM: 26.48m	10min	240	240	48582.3-48582.3= 0lt
	26.50m	10min	420	420	48588.2-48596.1= 7.9lt
	TO: 29.45m	10min	600	450	48606.0-48659.1= 53.1lt
		10min	420	420	48663.6-48712.6= 49lt
		10min	240	240	48716.1-48716.2= 0.1lt
Double	FROM: 29.45m	10min	270	270	48718.6-48719.0= 0.4lt
	29.50m	10min	470	400	48728.3-48786.9= 58.6lt
	TO: 32.81m	10min	665	400	48792.1-48863.2= 71.1lt
		10min	470	370	48874.3-48961.2= 89.9lt
		10min	270	270	48965.0-48965.0= 0lt
Double	FROM: 32.81m	10min	295	295	48987.4-48992.9= 5.5lt
	32.50m	10min	515	350	48998.2-49068.1= 69.9lt
	TO: 35.23mm	10min	735	350	49074.1-49134.8= 60.7lt
		10min	515	350	49144.4-49218.3= 73.9lt
		10min	295	295	49222.4-49222.5= 0lt
Single	FROM: 35.23m	10min	320	320	49256.1-49325.9= 69.8lt
	35.50m	10min	560	350	49333.5-49403.1= 69.6lt
	TO: END OF	10min	800	350	49409.1-49483.6= 74.5lt
	BOREHOLE	10min	560	350	49487.6-49577.8= 90.2lt
		10min	320	320	49581.9-49659.3= 77.4lt
REMARKS:					

Fig C-34: Water Pressure Testing Report (N1)



Fig C-35: Borehole N1 Core Box 1 of 6



Fig C-36: Borehole N1 Core Box 2 of 6



Fig C-37: Borehole N1 Core Box 3 of 6



Fig C-38: Borehole N1 Core Box 4 of 6



Fig C-39: Borehole N1 Core Box 5 of 6

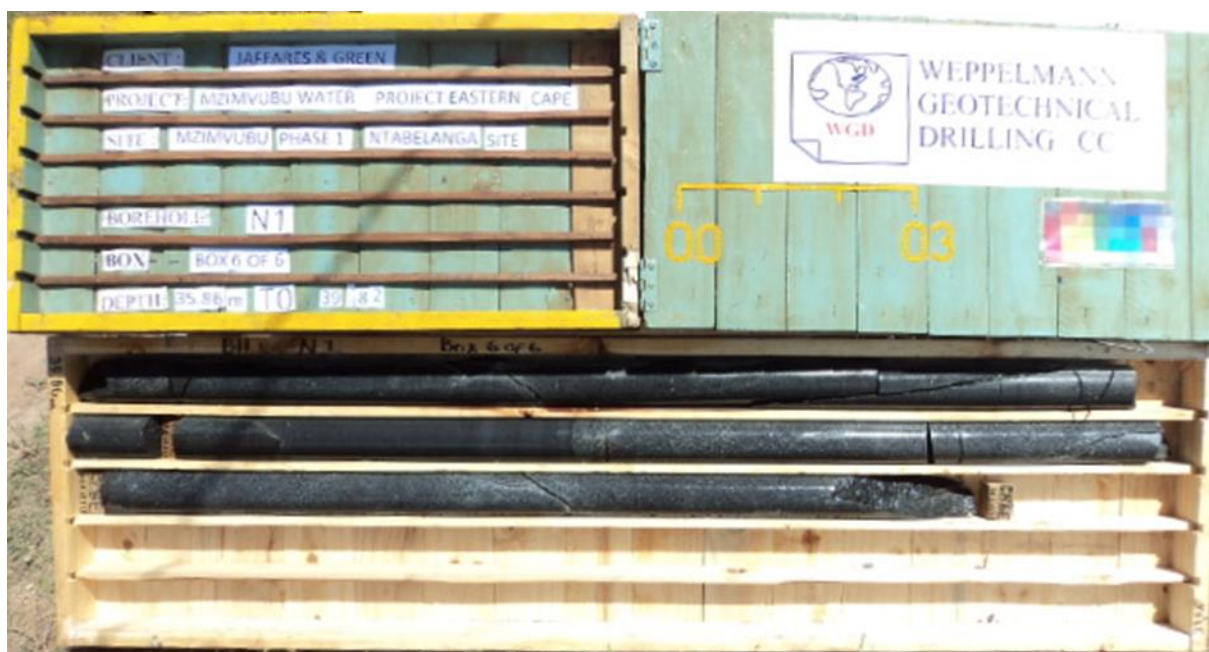


Fig C-40: Borehole N1 Core Box 6 of 6

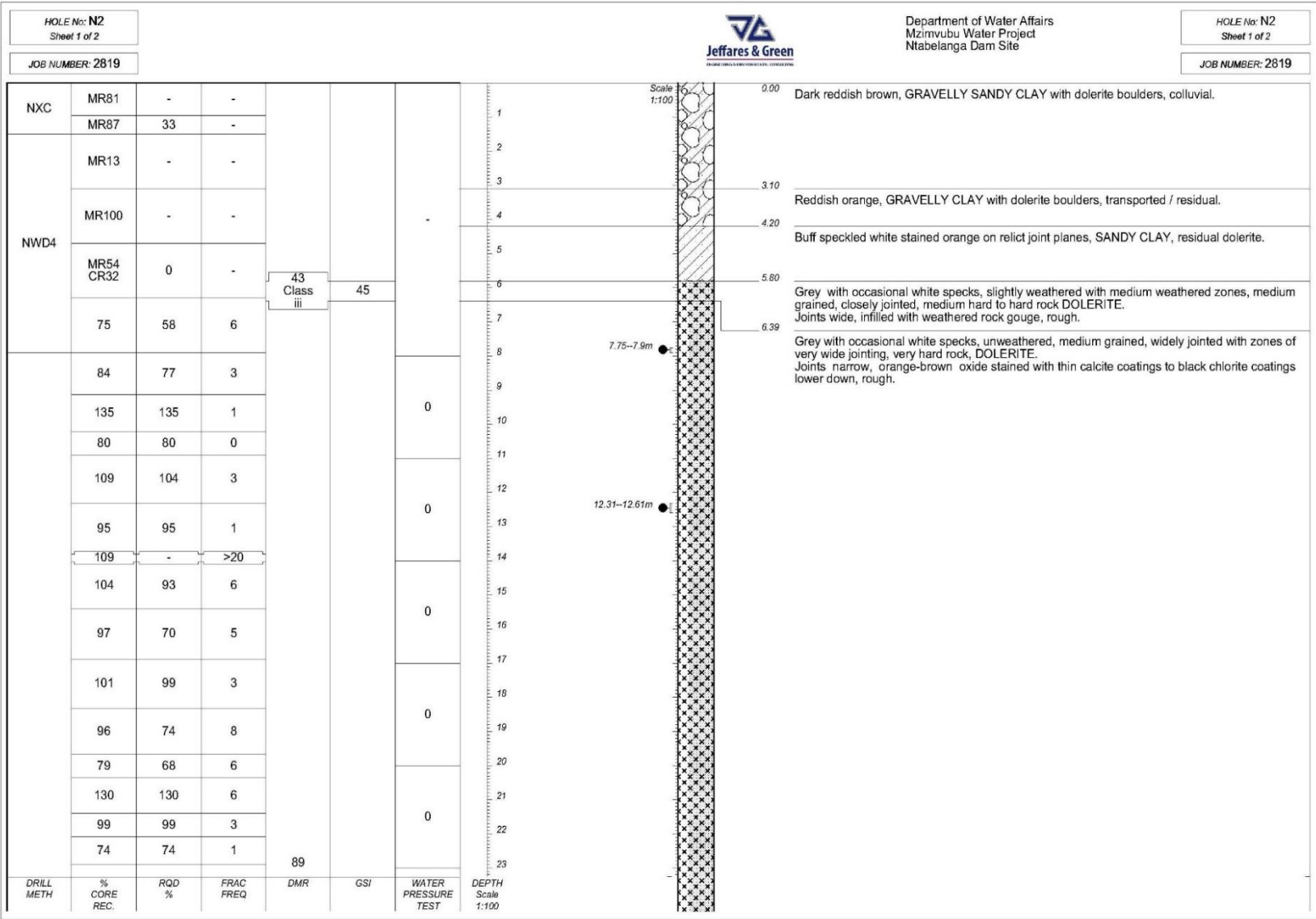


Fig C-41.1: Borehole Logs (N2)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

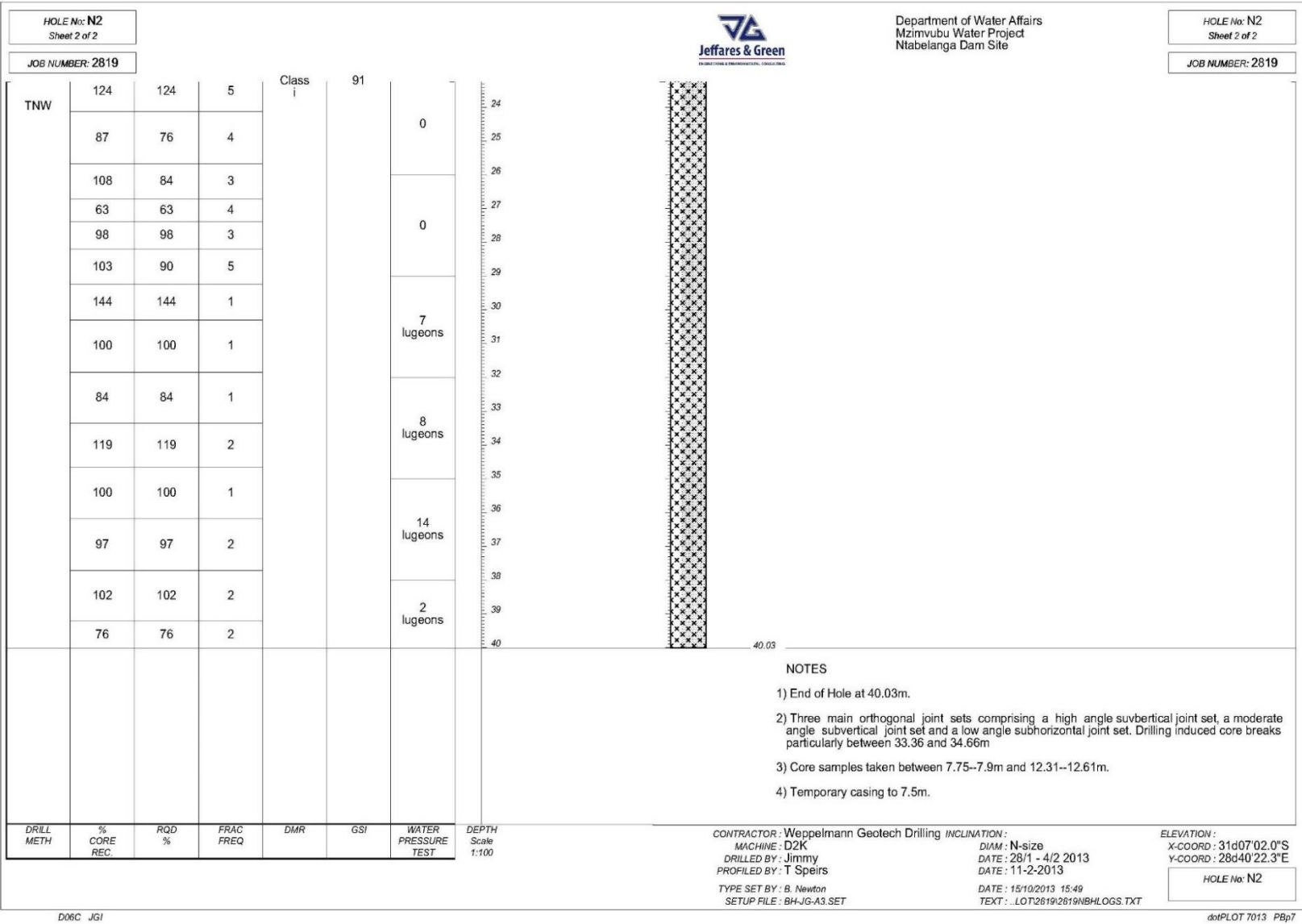


Fig C-41.2: Borehole Logs (N2)



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Report on Waterpressure Testing

SCHEME: Mzimvubu Water Project
 DRILLER: Shane

BOREHOLE NR: N 2

DATE & Packer Description	STAGES	TESTING TIME	GAUGE REQUIRED PRESSURES	PRESURES ACTUAL PRESSURES	WATER INTAKE BY HOLE TOTAL LITRES
11/02/2013	METERS	REQUIRED MINUTES			
Double	FROM: 8.00m	10min	70		50386.2-50386.2= 0lt
		10min	130		50391.9-50392.1= 0.2lt
	TO: 11.00m	10min	190		50395.7-50396.8= 1.1lt
		10min	130		50391.5-50398.8= 7.3lt
		10min	70		50399.9-50400.7= 0.8lt
Double	FROM: 11.00m	10min	100		50415.6-50415.6= 0lt
		10min	170		50417.1-50417.1= 0lt
	TO: 14.00m	10min	250		50418.8-50423.8= 50lt
		10min	170		50424.9-50424.9= 0lt
		10min	100		50425.6-50525.6= 0lt
Double	FROM: 14.00m	10min	125		50438.8-50439.0= 2 lt
		10min	220		50439.4-50439.4= 0lt
	TO: 17.00m	10min	320		50440.1-50443.2= 3.1lt
		10min	220		50444.6-50444.6= 0lt
		10min	125		50448.4-50448.4= 0lt
Double	FROM: 17.00m	10min	155		50462.0-50462.0= 0lt
		10min	270		50462.8-50462.8= 0lt
	TO: 20.00m	10min	385		50464.5-50464.5= 0lt
		10min	270		50466.0-50466.0= 0lt
		10min	155		50468.2-50468.2= 0lt
Double	FROM: 20.00m	10min	200		50412.0-50412.0= 0lt
		10min	350		50480.8-50481.6= 0.8lt
	TO: 23.00m	10min	500		50483.4-50504.1= 20.7lt
		10min	350		50525.5-50525.5= 0lt
		10min	200		50526.4-50526.4= 0lt
12/02/2013 Double	FROM: 23.00m	10min	290		50536.3-50536.3= 0lt
		10min	365		50538.1-50538.2= 0.1lt
	TO: 26.00m	10min	520		50546.3-50765.2= 218.9lt
		10min	365		50707.7-50707.7= 0lt
		10min	290		50709.3-50709.3= 0lt
Double	FROM: 26.00m	10min	235		50719.4-50719.4= 0lt
		10min	470		50722.5-50722.5= 0lt
	TO: 29.00m	10min	590		50732.7-50872.9= 140.2lt
		10min	470		50876.2-50876.2= 0lt
		10min	235		50877.7-50877.7= 0lt
Double	FROM: 29.00m	10min	265		50886.1-50886.1= 0lt
		10min	460		50890.4-50921.5= 31.1lt
	TO: 32.00m	10min	655	550kpa	50939.4-51184.0= 244.6lt
		10min	460		51188.6-51287.9= 99.3lt
		10min	265		51290.9-51290.9= 0lt
Double	FROM: 32.00m	10min	290		51297.9-51297.9= 0lt
		10min	510		51303.1-51385.9= 82.8lt
	TO: 35.00m	10min	725	700kpa	51399.4-51704.7= 305.3lt
		10min	510		51718.7-51843.6= 124.9lt
		10min	290		51847.1-51847.1= 0lt
Double	FROM: 35.00m	10min	315		51862.9-51862.9= 0lt
		10min	555		51885.4-52088.8= 203.4lt
	TO: 38.00m	10min	790	660kpa	52117.9-52394.7= 276.8lt
		10min	555		52418.5-52644.6= 226.1lt
		10min	315		52651.9-52651.9= 0lt
Single	FROM: 38.00m	10min	345		52676.3-52676.3= 0lt
		10min	600		52682.9-52872.3= 189.4lt
	TO: END OF BOREHOLE	10min	860	600kpa	52887.7-53088.8= 201.1lt
		10min	600		53102.1-53354.4= 252.3lt
		10min	345		53359.1-53359.1= 0lt
REMARKS:					

Fig C-42: Water Pressure Testing Report (N2)



Fig C-43: Borehole N2 Core Box 1 of 6



Fig C-44: Borehole N2 Core Box 2 of 6



Fig C-45: Borehole N2 Core Box 3 of 6



Fig C-46: Borehole N2 Core Box 4 of 6



Fig C-47: Borehole N2 Core Box 5 of 6



Fig C-46: Borehole N2 Core Box 6 of 6

APPENDIX D

PHASE 2 SITE PLANS

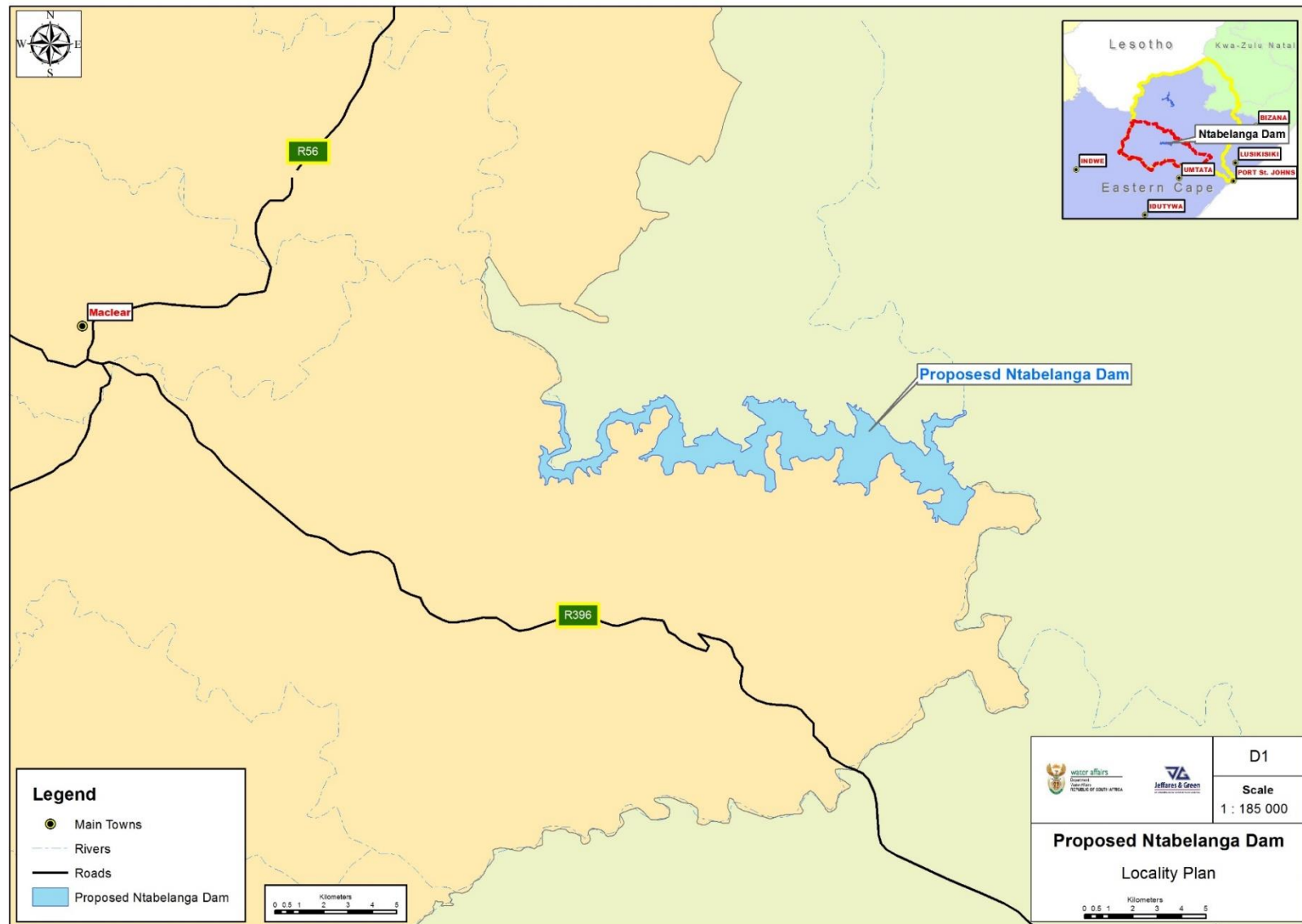


Fig D-1: Ntabelanga Locality Plan

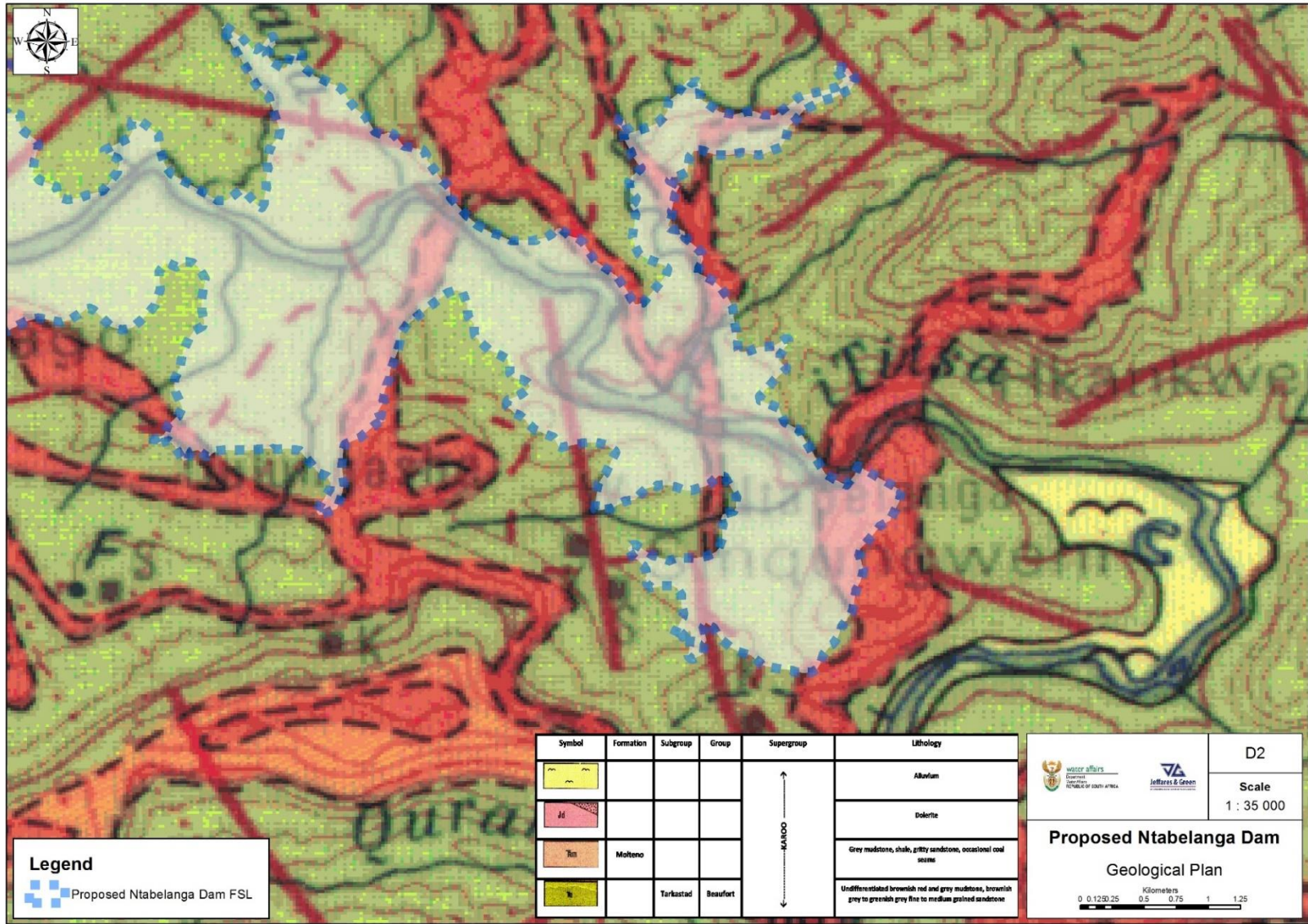


Fig D-2: Ntabelanga Geological Plan

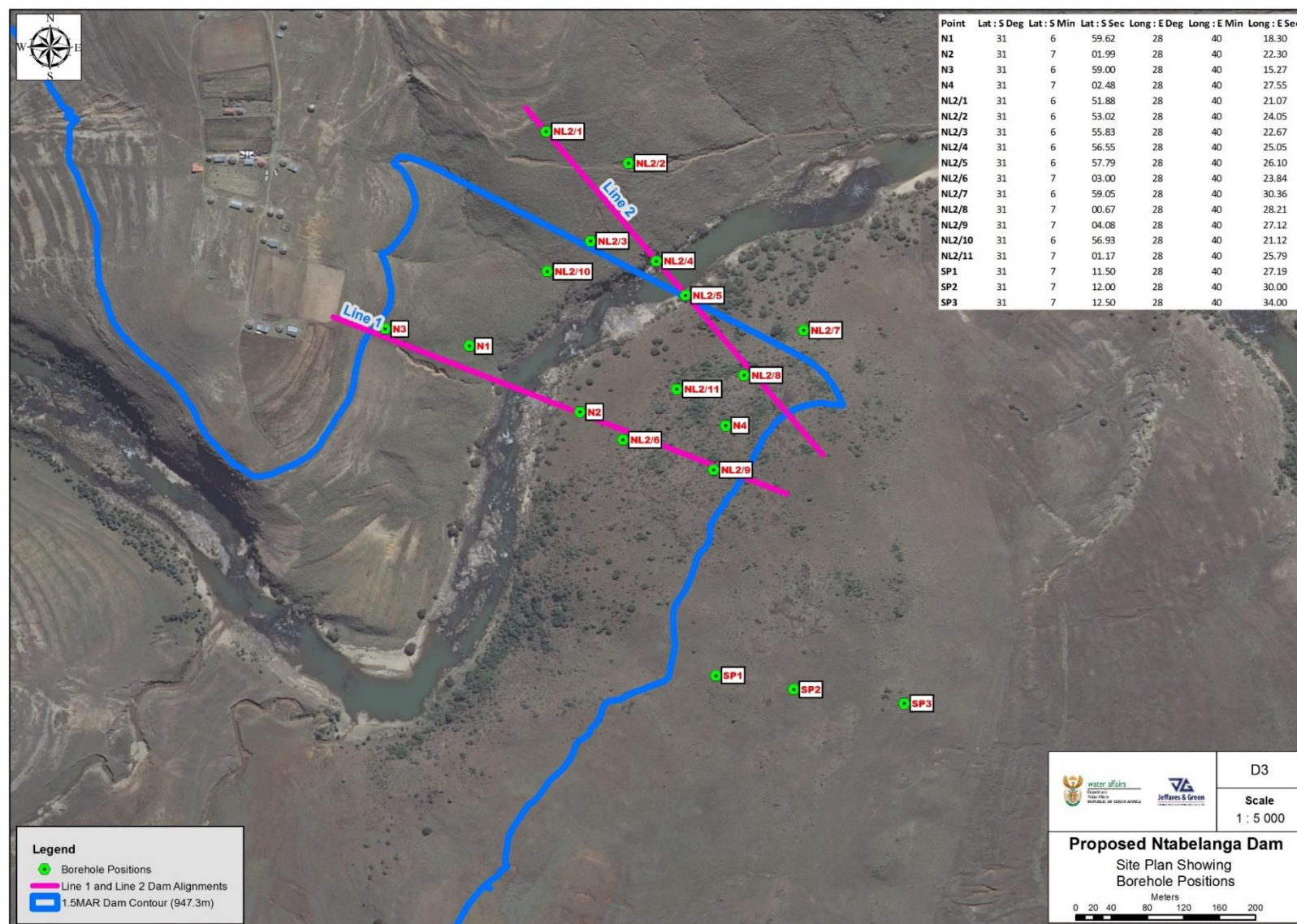


Fig D-3: Site Plan Showing Borehole Positions

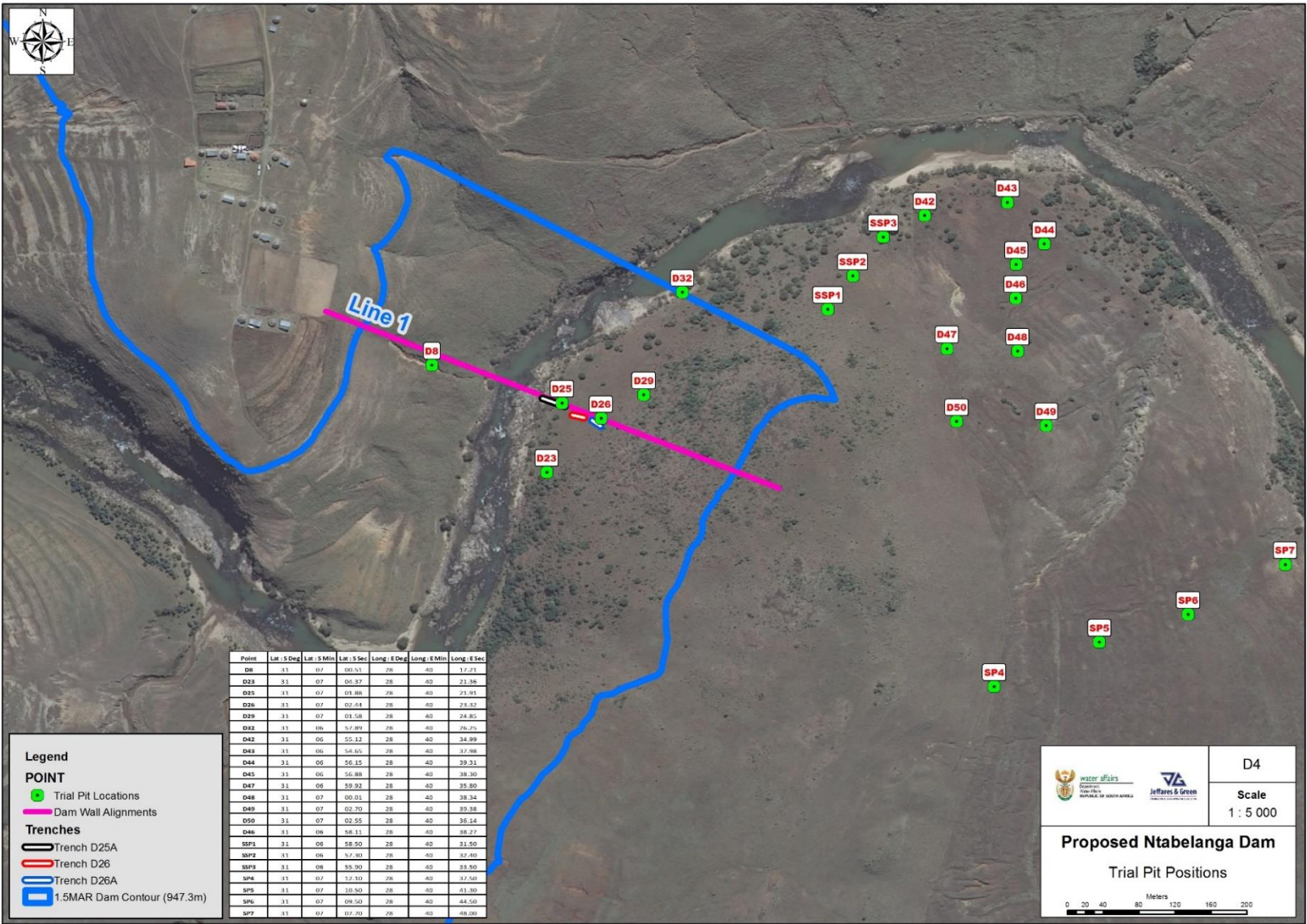


Fig D-4: Site Plan Showing Trial Pit Positions

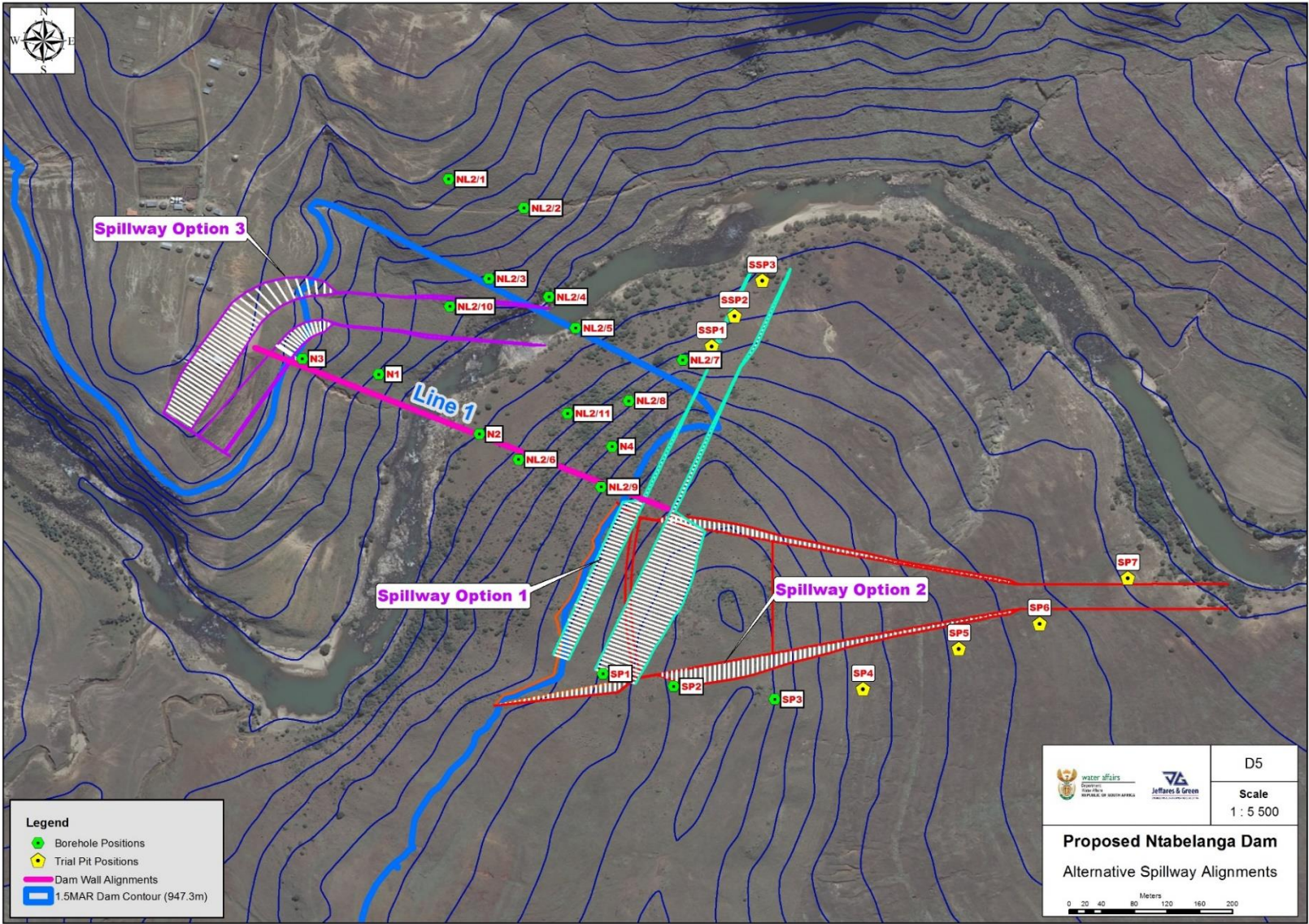


Fig D-5: Site Plan Showing Alternative Spillway Alignments



Fig D-6: Plan of Saddle Dam Showing Trial Pit Positions

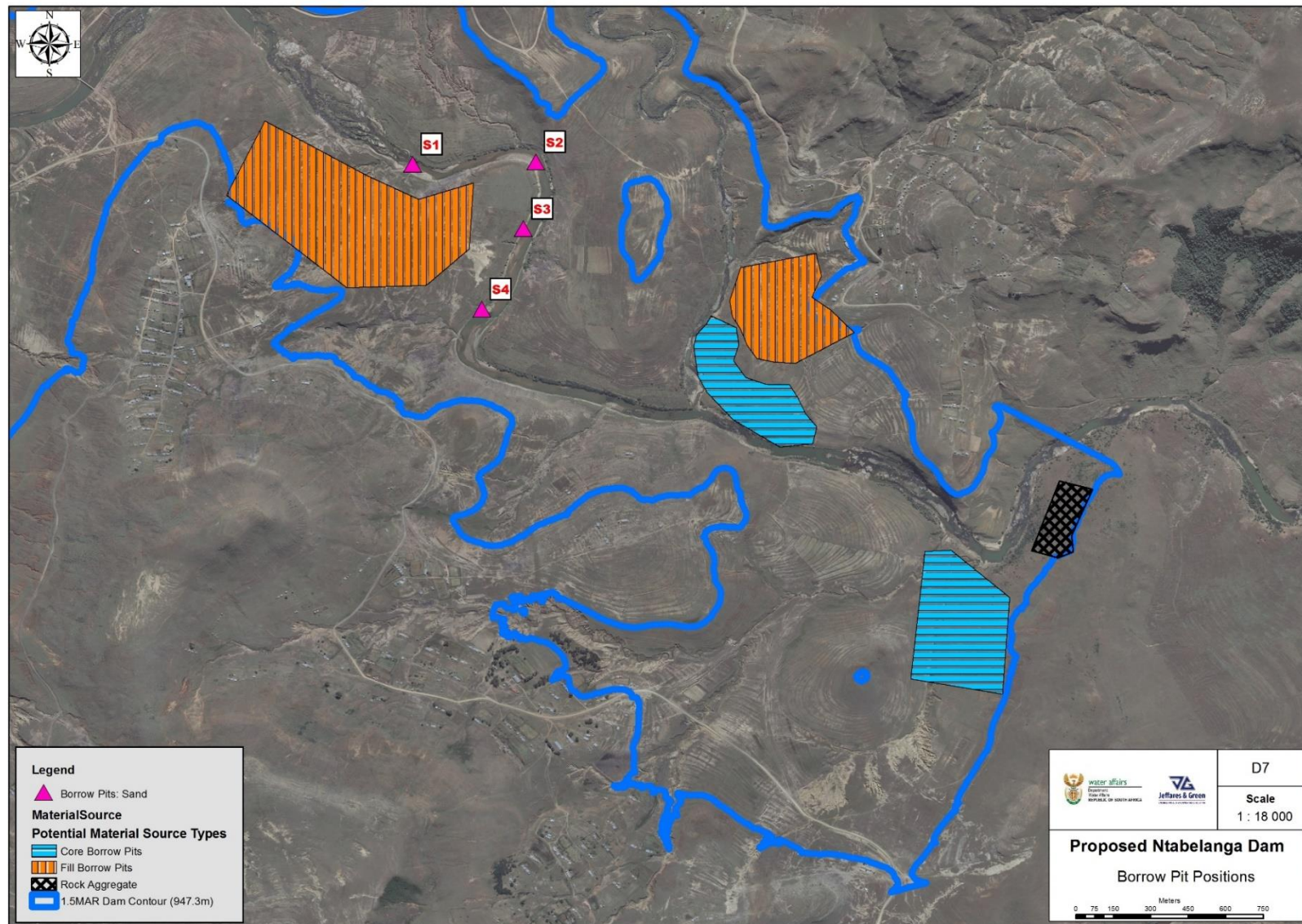


Fig D-7: Plan Showing Borrow Pit Locations



Fig D-8: Core Borrow Pit 1 Site Plan

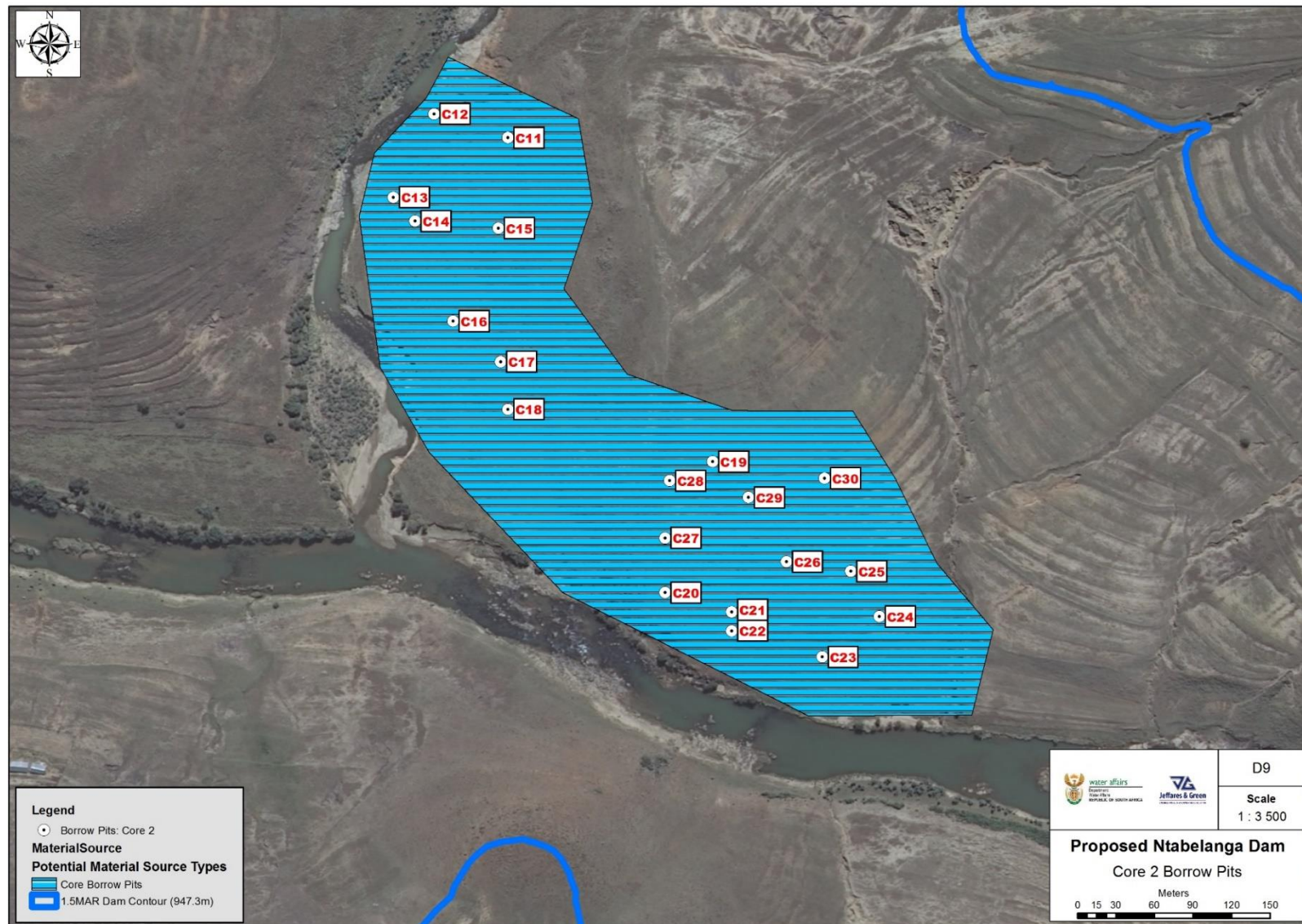


Fig D-9: Core Borrow Pit 2 Site Plan

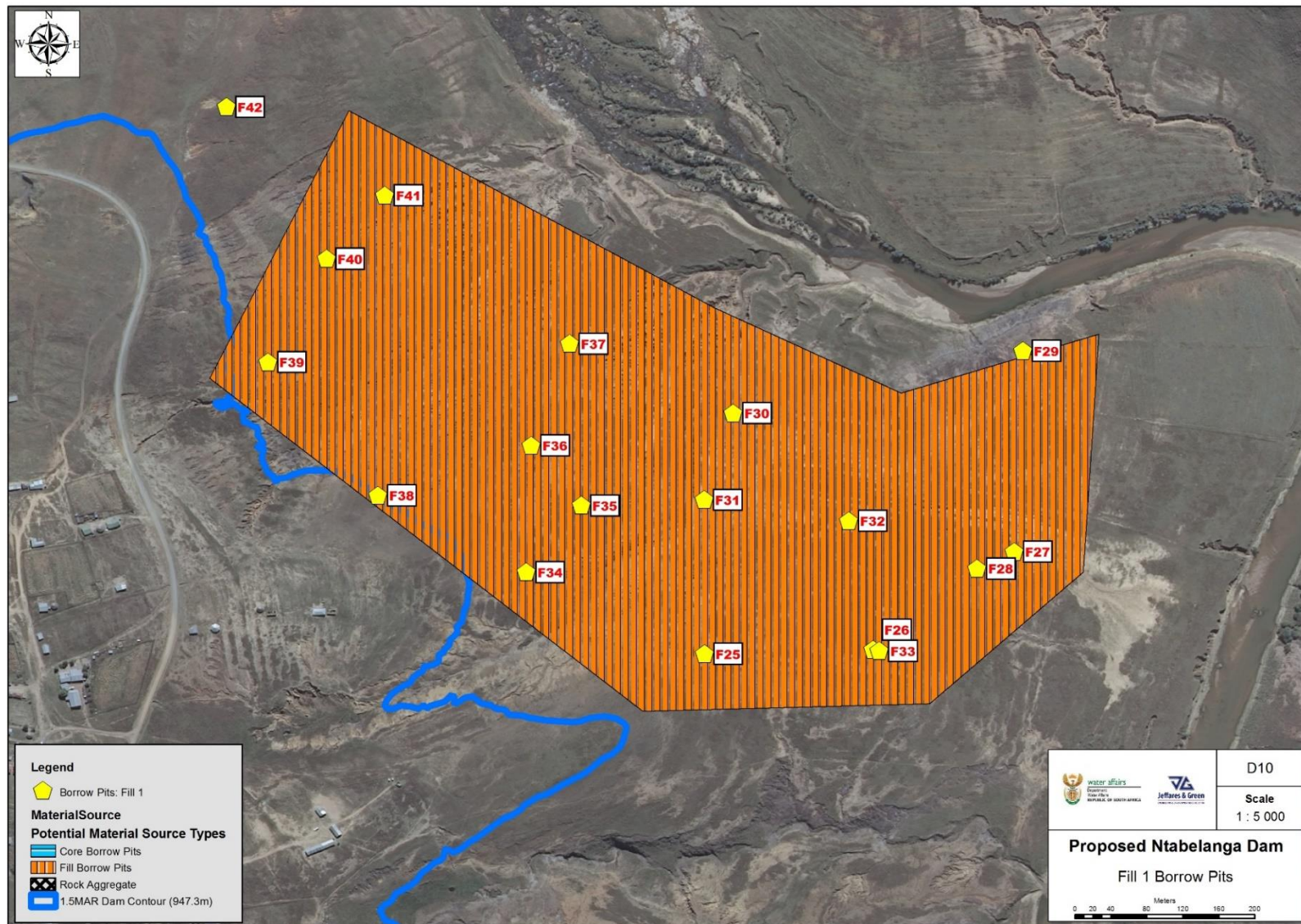


Fig D-10: Fill Borrow Pit 1 Site Plan

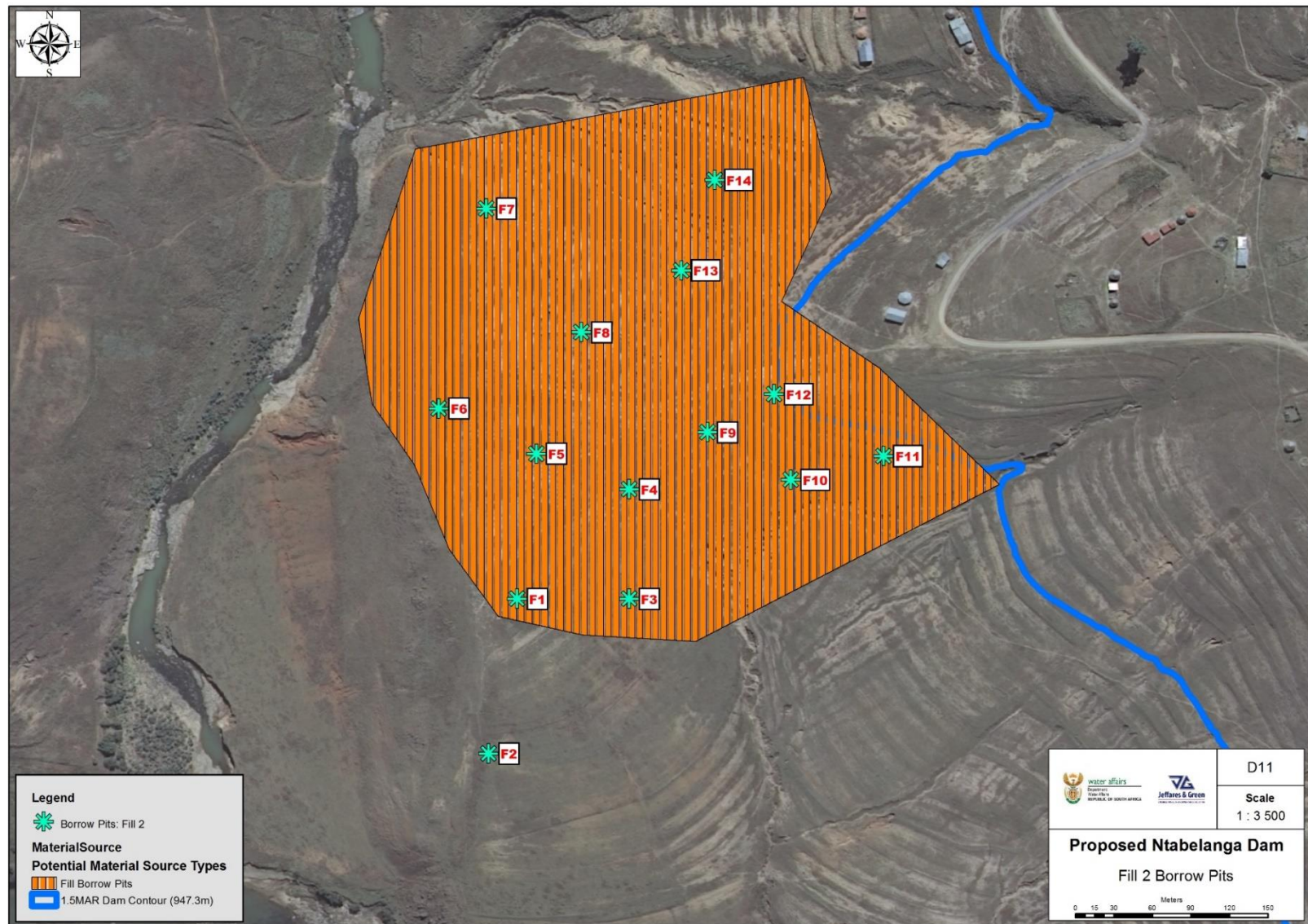


Fig D-11: Fill Borrow Pit 2 Site Plan

APPENDIX E

PHASE 2 BOREHOLE LOGS

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

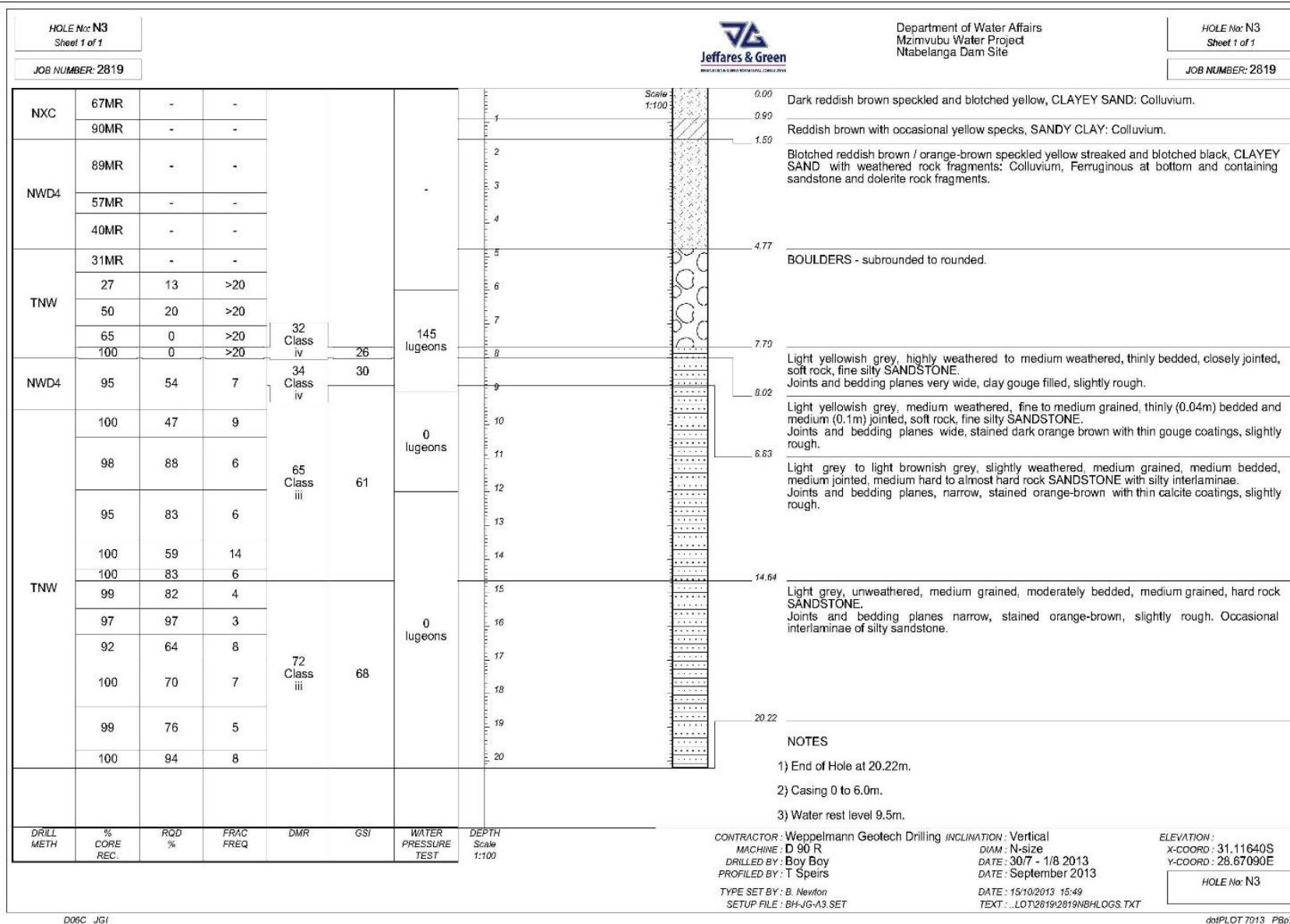


Fig E-1: Borehole Logs (N3)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river N 3

BOREHOLE NR: N 3

DRILLER: Boy Boy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESSURES	PRESURES	WATER INTAKE BY HOLE
06/08/2013	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
DP	From: 6.00m	10 min	55kpa	55kpa	405L
		10 min	95	95	462L
	TO 9.00m	10 min	135	135	615L
		10 min	95	95	334L
		10 min	55kpa	55kpa	240L
DP	FROM 9.00m	10 min	80kpa	80kpa	0
		10 min	140	140	0
	TO 12.00m	10 min	200	200	0
		10 min	140	140	0
		10 min	80kpa	80kpa	0
09/08/2013 SP	FROM 12.00m	10 min	110kpa	110kpa	0
		10 min	190	190	0
	TO End of BH	10 min	270	270	0
		10 min	190	190	0
		10 min	110kpa	110kpa	0

REMARKS:

Fig E-2: Water Pressure Testing Report (N3)



Fig E-3: Borehole N3 Core Box 1 of 3



Fig E-4: Borehole N3 Core Box 2 of 3



Fig E-5: Borehole N3 Core Box 3 of 3

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

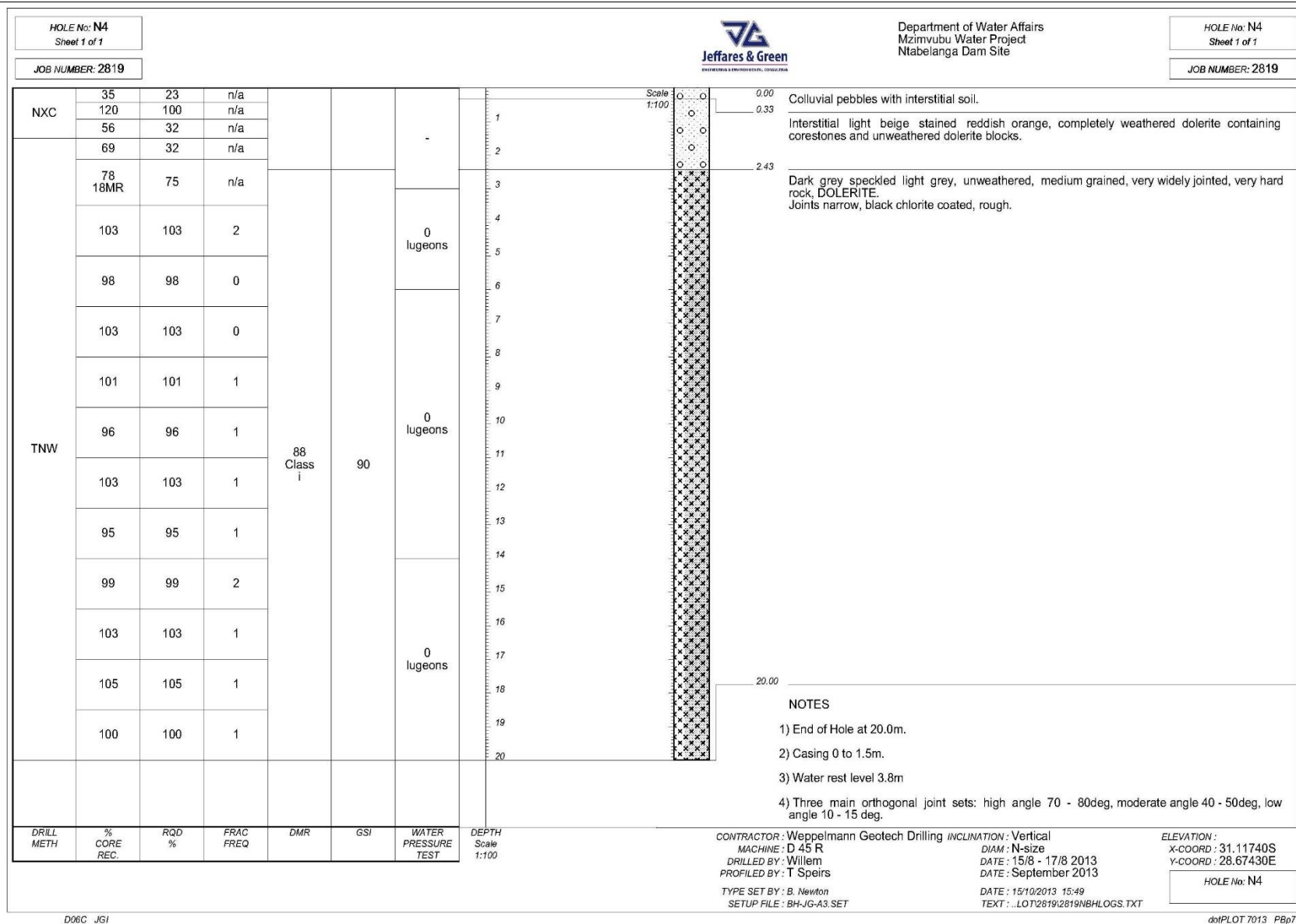


Fig E-6: Borehole Logs (N4)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river N 4

BOREHOLE NR: N 4

DRILLER: Willem

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESSURES	PRESURES	WATER INTAKE BY HOLE
19/08/2013	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
DP	From: 3.00m	10 min	25kpa	25kpa	0
		10 min	50	50	0
	TO 6.00m	10 min	70	70	0
		10 min	50	50	0
		10 min	25kpa	25kpa	0
DP	FROM 8.00m	10 min	70kpa	70kpa	0
		10 min	130	130	0
	TO 14.00m	10 min	180	180	1 L
		10 min	130	130	0
		10 min	70kpa	70kpa	0
SP	FROM 14.00m	10 min	125kpa	125kpa	0
		10 min	220	220	0
	TO End of BH	10 min	320	320	6 L
		10 min	220	220	0
		10 min	125kpa	125kpa	0

REMARKS:

Fig E-7: Water Pressure Testing Report (N4)



Fig E-8: Borehole N4 Core Box 1 of 3



Fig E-9: Borehole N4 Core Box 2 of 3



Fig E-10: Borehole N4 Core Box 3 of 3

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

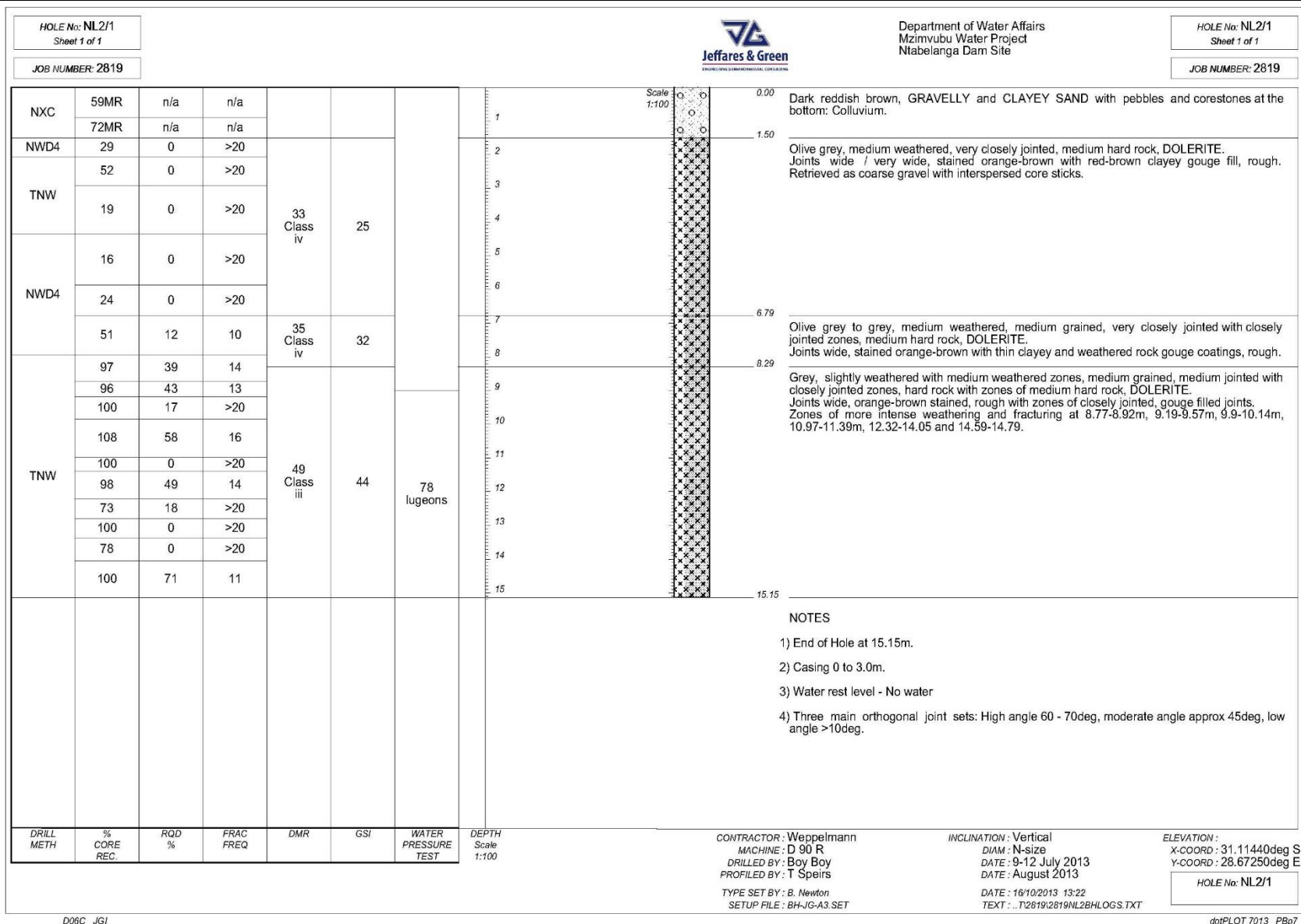


Fig E-11: Borehole Logs (NL2/1)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/1

DRILLER: Boy Boy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESURES		WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
14-Jul	From: 9.00m	10	140kpa	140kpa	46.9L
		10	180kpa	180kpa	65.2L
	TO	10	200kpa	200kpa	1103L
	15.15m	10	180kpa	180kpa	990L
		10	140kpa	140kpa	668L

REMARKS:

Fig E-12: Water Pressure Testing Report (NL 2/1)



Fig E-13: Borehole NL 2/1 Core Box 1 of 2



Fig E-14: Borehole NL 2/1 Core Box 2 of 2

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

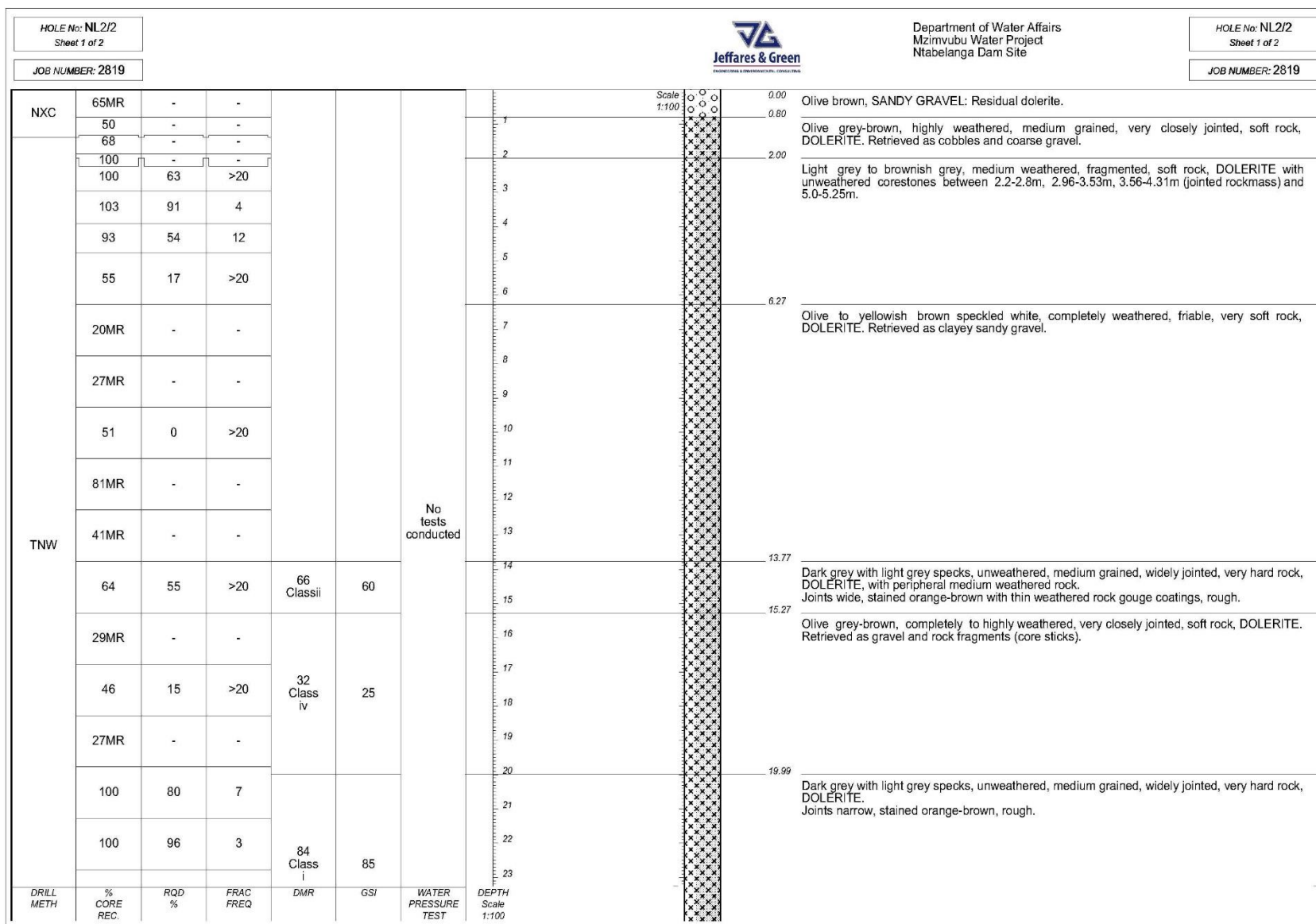


Fig E-15-1: Borehole Logs (NL 2/2)

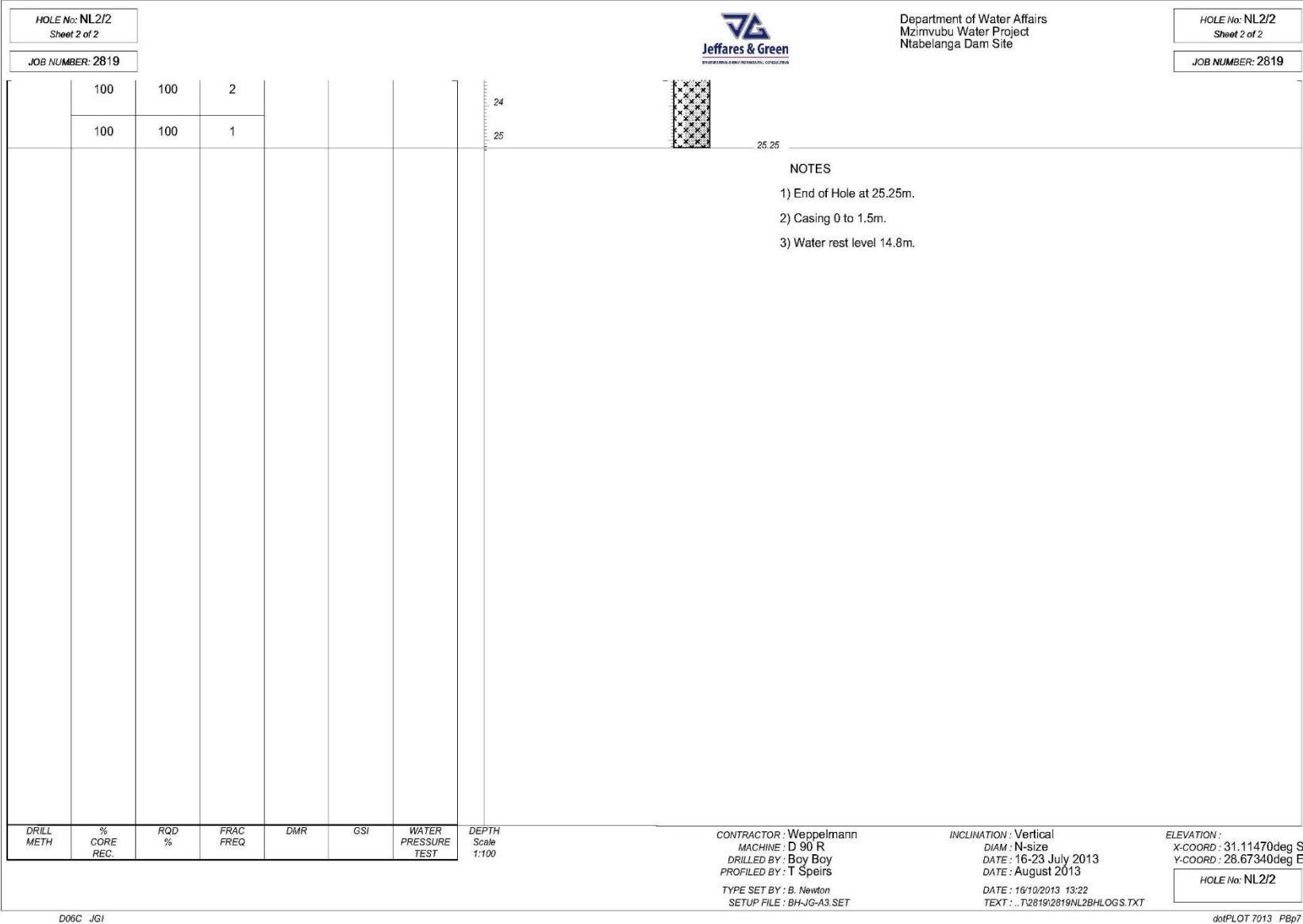


Fig E-15-2: Borehole Logs (NL 2/2)



Fig E-16: Borehole NL 2/2 Core Box 1 of 3



Fig E-17: Borehole NL 2/2 Core Box 2 of 3



Fig E-18: Borehole NL 2/2 Core Box 3 of 3

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

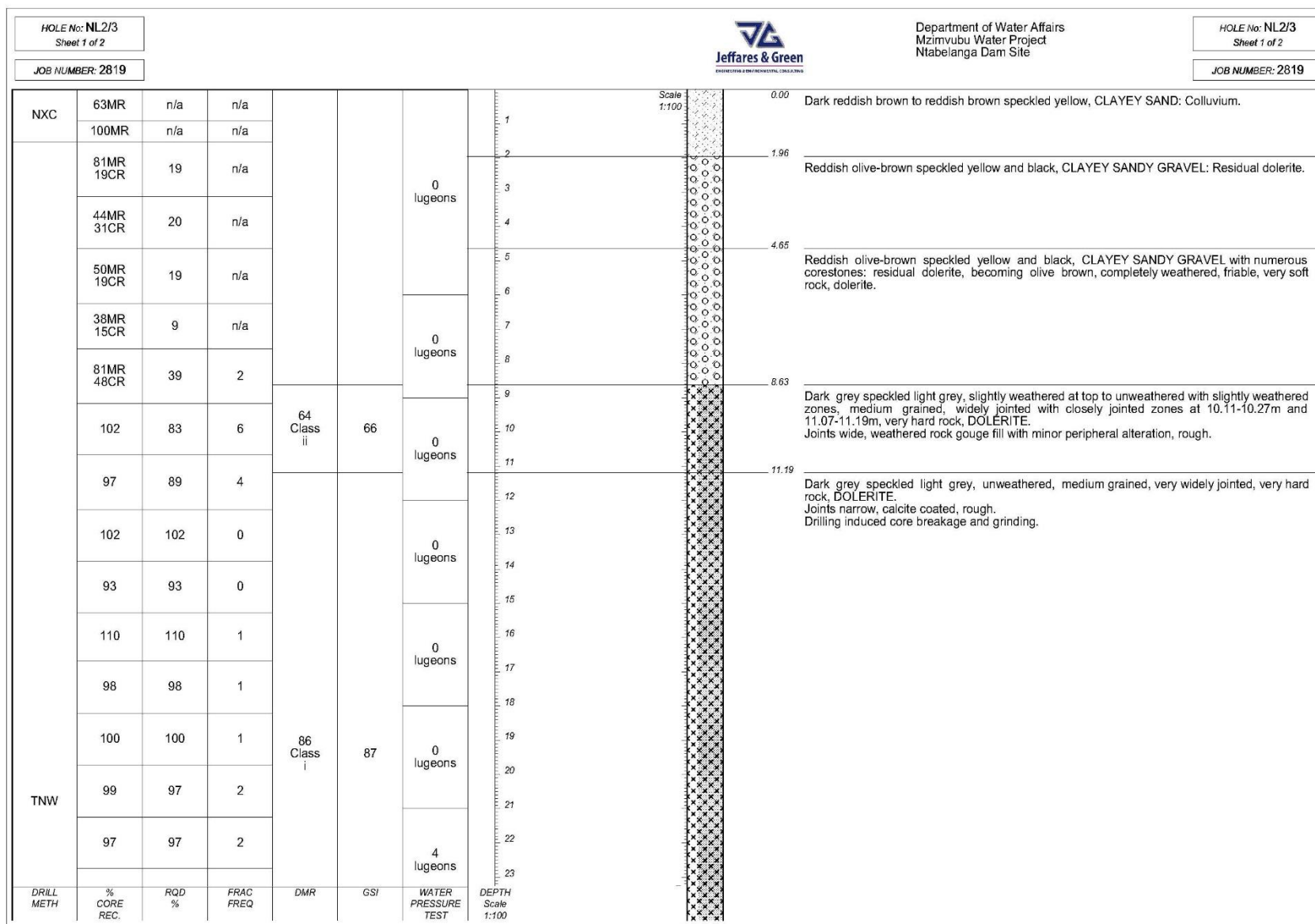


Fig E-19-1: Borehole Logs (NL 2/3)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

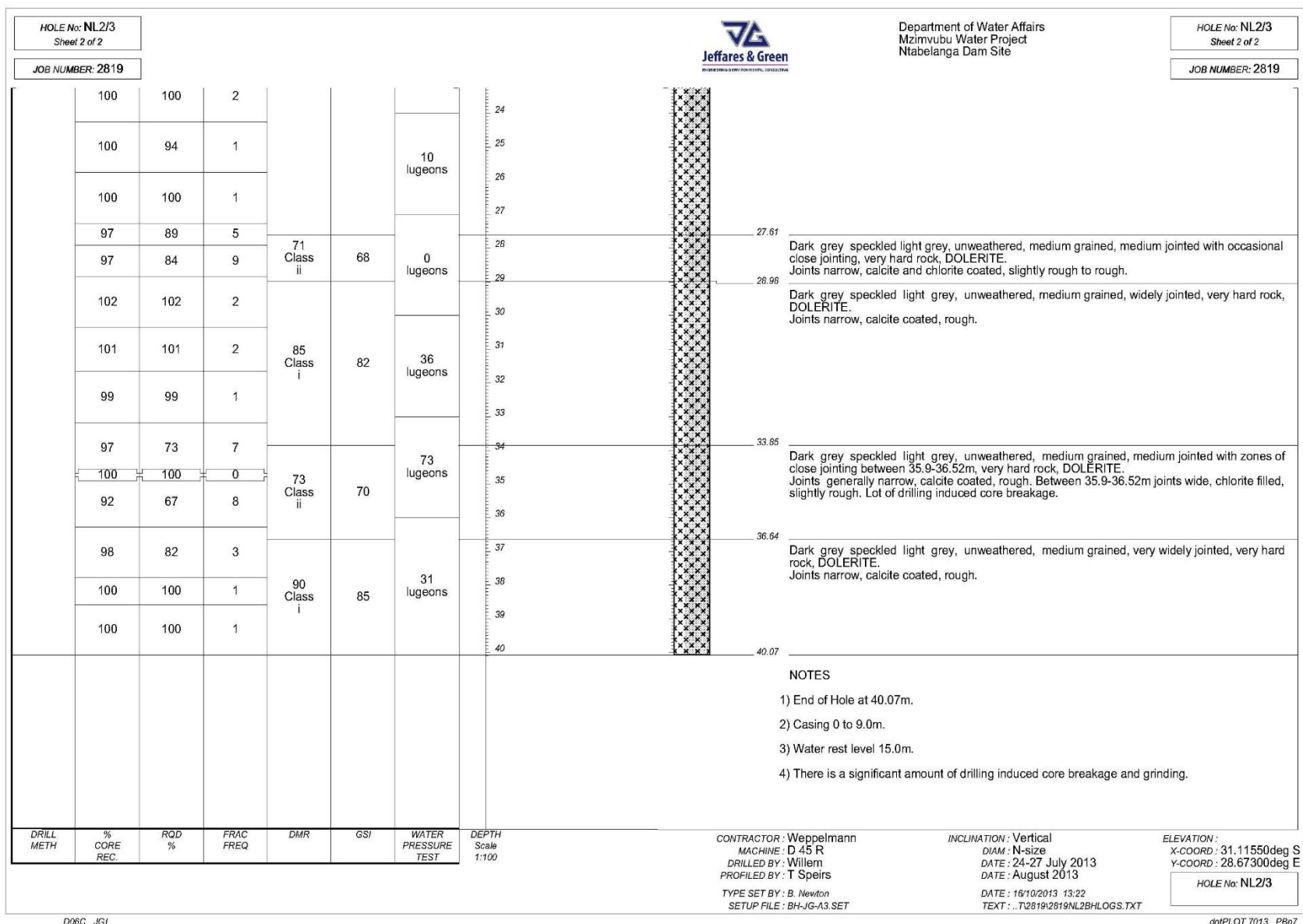


Fig E-19-2: Borehole Logs (NL 2/3)



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Report on Waterpressure Testing

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SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/3

DRILLER: Boyboy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE	PRESURES	WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
29/07/2013 DP	FROM 6.00m	10	45kpa	45kpa	190L
		10	80kpa	80kpa	9L
	TO 9.00m	10	115kpa	115kpa	261L
		10	80kpa	80kpa	90L
		10	115kpa	115kpa	0
DP	FROM 9.00m	10	70kpa	70kpa	0
		10	130kpa	130kpa	1L
	TO 12.00m	10	180kpa	180kpa	0
		10	130kpa	130kpa	0
		10	70kpa	70kpa	0
DP	FROM 12.00m	10	100kpa	100kpa	0
		10	170kpa	170kpa	0
	TO 15.00m	10	250kpa	250kpa	0
		10	170kpa	170kpa	0
		10	100kpa	100kpa	0
DP	FROM 15.00m	10	125kpa	125kpa	0
		10	220kpa	220kpa	480L
	TO 18.00m	10	320kpa	320kpa	107L
		10	220kpa	220kpa	0
		10	125kpa	125kpa	0
DP	FROM 18.00m	10	155kpa	155kpa	0
		10	270kpa	270kpa	0
	TO 21.00m	10	358kpa	358kpa	0
		10	270kpa	270kpa	0
		10	155kpa	155kpa	0
DP	FROM 21.00m	10	180kpa	180kpa	0
		10	320kpa	320kpa	684L
	TO 24.00M	10	450kpa	450kpa	1115L
		10	320kpa	320kpa	430L
		10	180kpa	180kpa	20L
DP	FROM 24.00m	10	210kpa	210kpa	29L
		10	365kpa	365kpa	0
	TO 27.00m	10	520kpa	520kpa	715L
		10	365kpa	365kpa	360L
		10	210kpa	210kpa	61L
DP	FROM 27.00m	10	235kpa	235kpa	2L
		10	410kpa	410kpa	542L
	TO 30.00m	10	590kpa	590kpa	721L
		10	410kpa	410kpa	458L
		10	235kpa	235kpa	0
DP	FROM 30.00m	10	265kpa	265kpa	250L
		10	460kpa	460kpa	962L
	TO 33.00m	10	655kpa	590kpa	731L
		10	460kpa	460kpa	567L
		10	265kpa	265kpa	289L
29/07/2013 DP	FROM 33.00m	10	300kpa	300kpa	692L
		10	520	510	1162L
	TO 36.00m	10	745	510	1121L
		10	520	510	1062L
		10	300kpa	300kpa	766L
SP	FROM 36.00m	10	325kpa	325kpa	32L
		10	570	570	241L
	TO End of hole	10	815	600	723L
		10	570	570	711L
		10	325kpa	325kpa	59L

REMARKS:

Fig E-20: Water Pressure Testing Report (NL 2/3)



Fig E-21: Borehole NL 2/3 Core Box 1 of 6



Fig E-22: Borehole NL 2/3 Core Box 2 of 6



Fig E-23: Borehole NL 2/3 Core Box 3 of 6



Fig E-24: Borehole NL 2/3 Core Box 4 of 6



Fig E-25: Borehole NL 2/3 Core Box 5 of 6



Fig E-26: Borehole NL 2/3 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

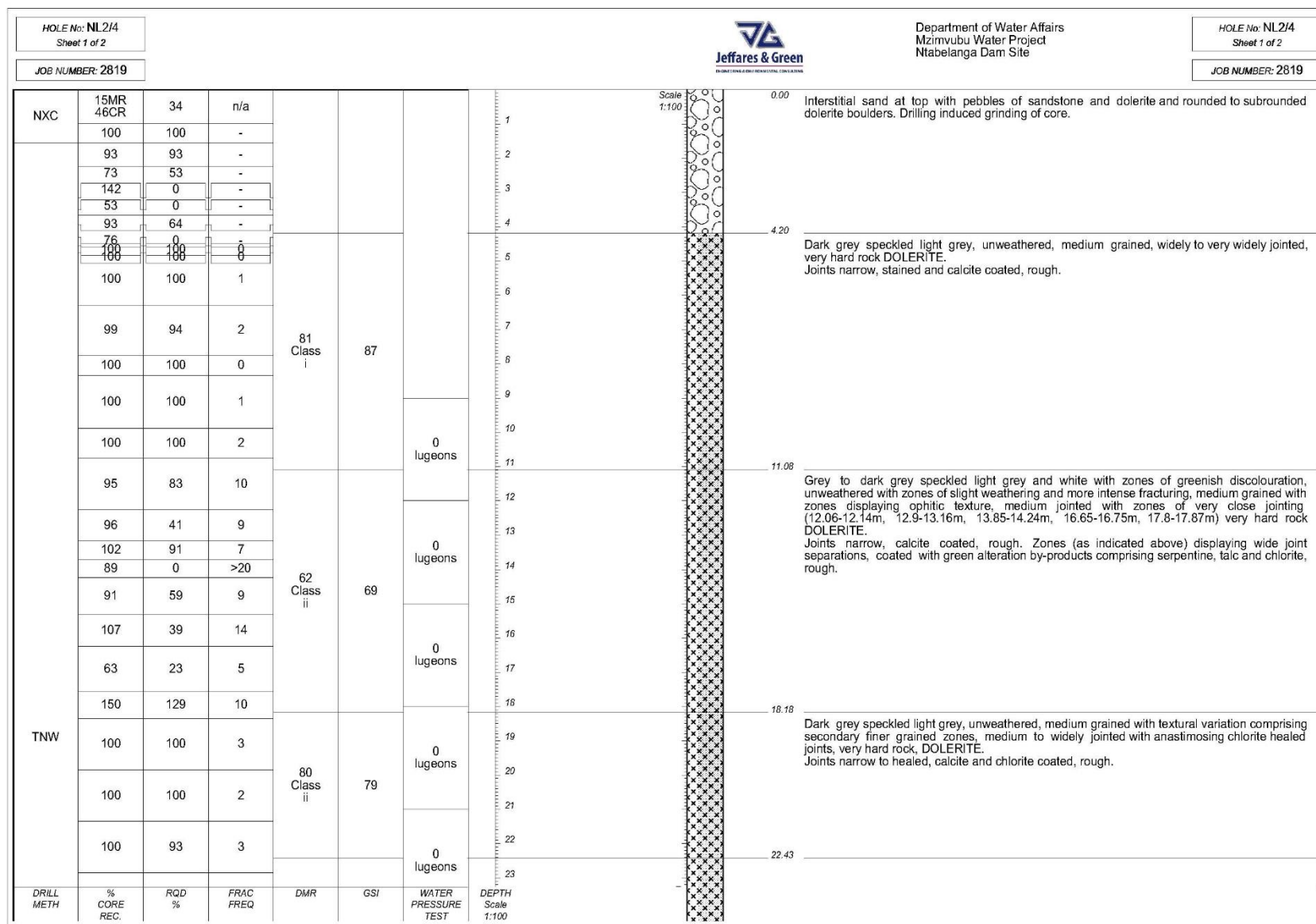


Fig E-27-1: Borehole Logs (NL 2/4)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

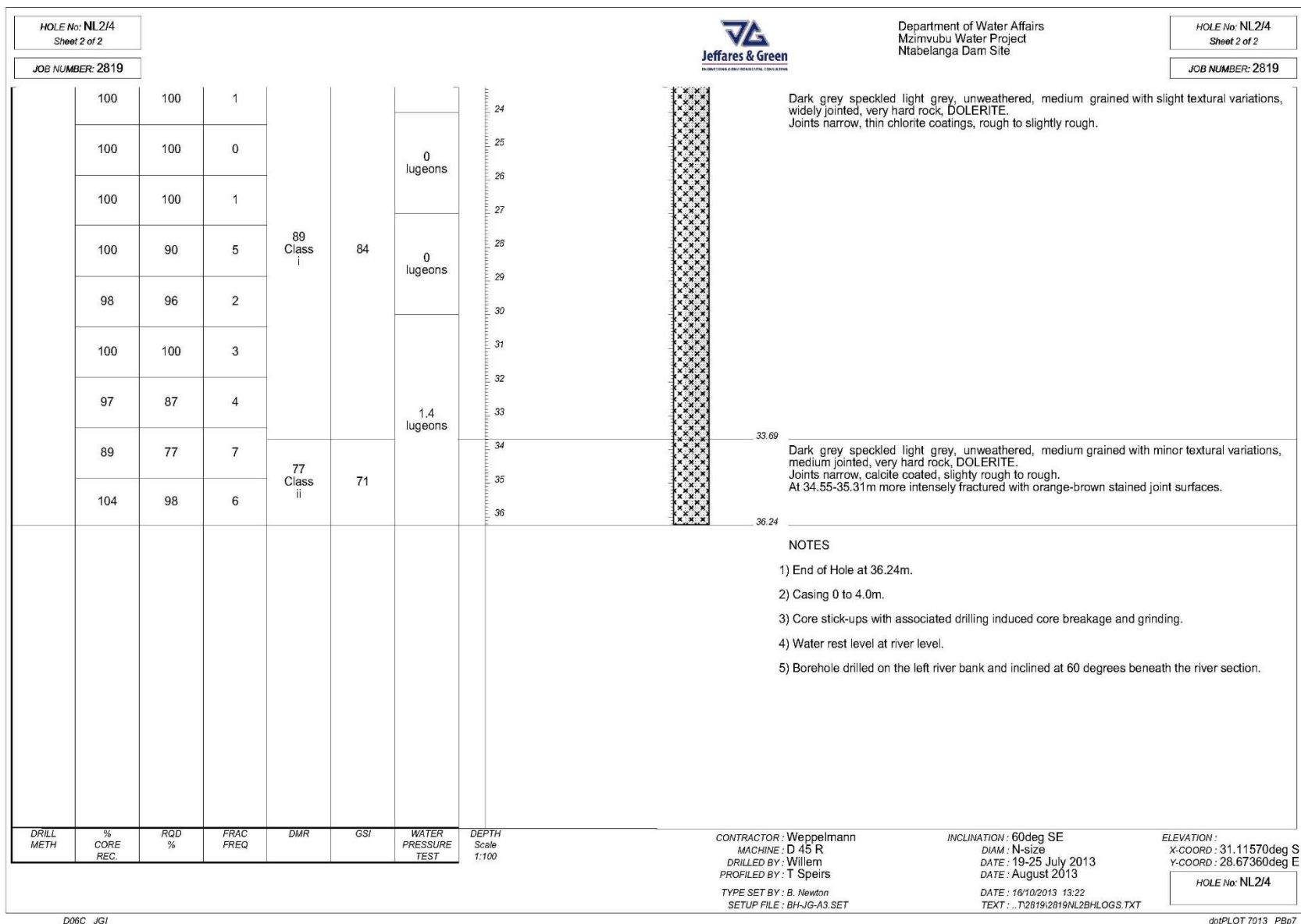


Fig E-27-2: Borehole Logs (NL 2/4)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/4

DRILLER: Willem

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESURES		WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
26/07/2013 DP	FROM 9.00m	10	45kpa	45kpa	0L
		10	65	65	0L
	TO 12.00m	10	90	90	0L
		10	65	65	0L
		10	35kpa	35kpa	0L
DP	FROM 12.00m	10	45kpa	45kpa	0L
		10	80	80	0L
	TO 15.00m	10	115	115	0L
		10	80	80	0L
		10	45kpa	45kpa	0L
DP	FROM 15.00m	10	55kpa	55kpa	0L
		10	95	95	0L
	TO 18.00m	10	135	135	0L
		10	95	95	0L
		10	55kpa	55kpa	0L
DP	FROM 18.00m	10	70kpa	70kpa	0L
		10	130	130	0L
	TO 21.00m	10	180	180	0L
		10	130	130	0L
		10	70kpa	70kpa	0L
DP	FROM 21.00m	10	145kpa	145kpa	0L
		10	255	255	0L
	TO 24.00m	10	360	360	0L
		10	255	255	0L
		10	145kpa	145kpa	0L
21-Jul DP	FROM 24.00m	10	165kpa	165kpa	0L
		10	285	285	0L
	TO 27.00M	10	405	405	0L
		10	285	285	0L
		10	165kpa	165kpa	0L
DP	FROM 27.00m	10	190kpa	190kpa	0L
		10	330	330	0L
	TO 30.00m	10	475	475	10L
		10	330	330	0L
		10	190kpa	190kpa	0L
SP	FROM 30.00m	10	215kpa	215kpa	0L
		10	365	365	33L
	TO End of hole	10	520	520	136L
		10	365	365	0L
		10	215kpa	215kpa	0L

REMARKS:

Fig E-28: Water Pressure Testing Report (NL 2/4)



Fig E-29: Borehole NL 2/4 Core Box 1 of 6



Fig E-30: Borehole NL 2/4 Core Box 2 of 6



Fig E-31: Borehole NL 2/4 Core Box 3 of 6



Fig E-32: Borehole NL 2/4 Core Box 4 of 6



Fig E-33: Borehole NL 2/4 Core Box 5 of 6



Fig E-34: Borehole NL 2/4 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

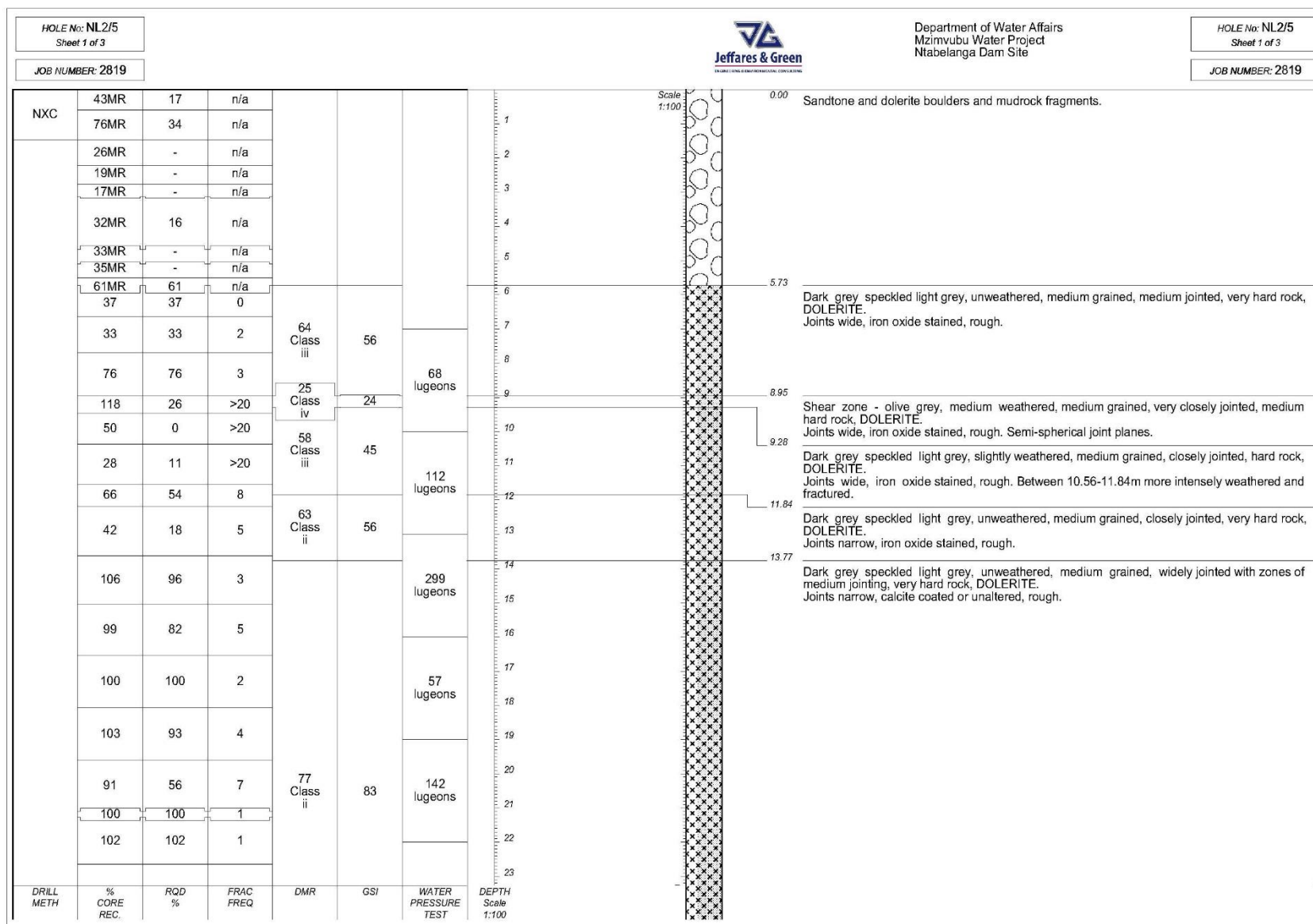


Fig E-35-1: Borehole Logs (NL 2/5)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

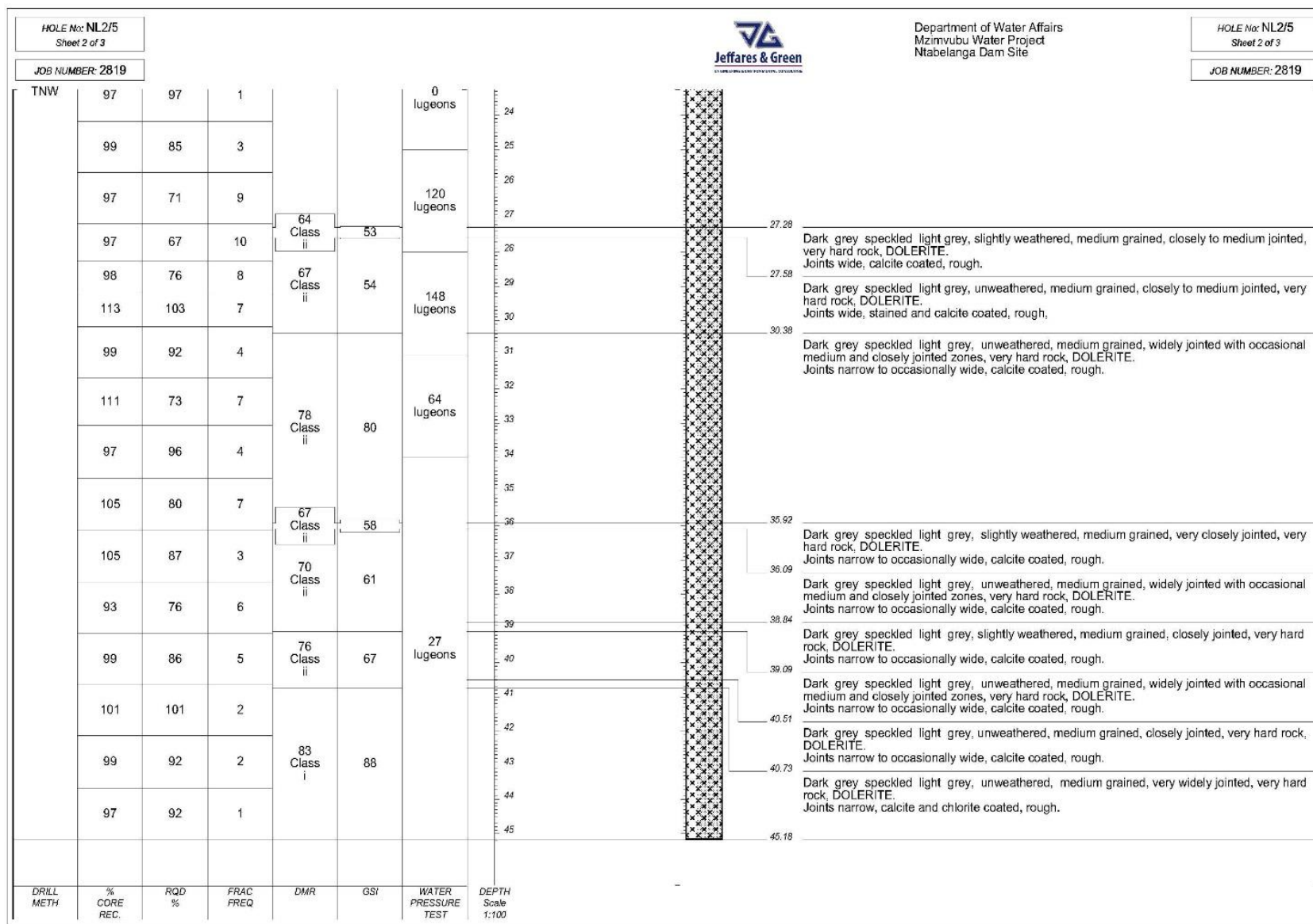



Fig E-35-2: Borehole Logs (NL 2/5)

HOLE No: NL2/5 Sheet 3 of 3		 Jeffares & Green <small>ANALYSIS AND ENGINEERING CONSULTANTS</small>		Department of Water Affairs Mzimvubu Water Project Ntabelanga Dam Site		HOLE No: NL2/5 Sheet 3 of 3	
JOB NUMBER: 2819						JOB NUMBER: 2819	
<div style="float: right; width: 30%;"> <p>NOTES</p> <p>1) End of Hole at 14.18m.</p> <p>2) Casing 0 to 7.0m.</p> <p>3) Water rest level 3.5m (4.0m down borehole).</p> <p>4) Three main orthogonal joint sets: high angle 60 - 70 deg, moderate angle approx. 45deg, low angle >10deg.</p> <p>5) Borehole drilled on the right river bank and inclined at 60 degrees beneath the river section.</p> </div>							
DRILL METH	% CORE REC.	RQD %	FRAC FREQ	DMR	GSI	WATER PRESSURE TEST	DEPTH Scale 1:100
				CONTRACTOR : Weppelmann MACHINE : D 90 R DRILLED BY : Boy Boy PROFILED BY : T Speirs TYPE SET BY : B. Newton SETUP FILE : BH-JG-A3.SET		INCLINATION : 60deg NW DIAM : N-size DATE : 8-15 August 2013 DATE : September 2013 DATE : 16/10/2013 13:22 TEXT : ...T2819\2819\NL2BHLOGS.TXT	
						ELEVATION : X-COORD : 31.11610deg S Y-COORD : 28.67390deg E <div style="border: 1px solid black; padding: 2px; width: fit-content; margin-top: 5px;"> HOLE No: NL2/5 </div>	

D06C JGI

dotPLOT 7013 PBp7

Fig E-35-3: Borehole Logs (NL 2/5)



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SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/5

DRILLER: Boy boy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESURES		WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
14/07/2013 DP	FROM 7.00m	10	45kpa	45kpa	7 L
		10	80	80	120L
	TO 10.00m	10	115	115	223L
		10	80	80	164L
		10	45kpa	45kpa	39L
DP	FROM 10.00m	10	65kpa	65kpa	328L
		10	110	110	413L
	TO 13.00m	10	160	160	537L
		10	110	110	373L
		10	65kpa	65kpa	352L
DP	FROM 13.00m	10	80kpa	80kpa	1399L
		10	140	140	946L
	TO 16.00m	10	200	200	1126L
		10	140	140	862L
		10	80kpa	80kpa	717L
DP	FROM 16.00m	10	100kpa	100kpa	239L
		10	170	170	325L
	TO 19.00m	10	250	250	391L
		10	170	170	297L
		10	100kpa	100kpa	171L
DP	FROM 19.00m	10	125kpa	125kpa	935L
		10	220	220	1241L
	TO 22.00m	10	320	320	1363L
		10	220	220	1208L
		10	125kpa	125kpa	890L
DP	FROM 22.00m	10	155kpa	155kpa	0L
		10	270	270	0L
	TO 25.00M	10	385	385	558L
		10	270	270	0L
		10	155kpa	155kpa	0L
15/07/2013 DP	FROM 25.00m	10	170kpa	170kpa	723L
		10	300	300	1067L
	TO 28.00m	10	430	430	1547L
		10	300	300	1006L
		10	170kpa	170kpa	803L
DP	FROM 28.00m	10	190kpa	190kpa	0L
		10	330	330	1153L
	TO 31.00m	10	475	475	1557L
		10	330	330	1424L
		10	190kpa	190kpa	843L
DP	FROM 31.00m	10	215kpa	215kpa	0L
		10	380	380	726L
	TO 34.00m	10	545	545	1035L
		10	380	380	745L
		10	215kpa	215kpa	0L
SP	FROM 34.00m	10	245kpa	245kpa	675L
		10	430	430	1223L
	TO End of Borehole	10	610	610	1547L
		10	430	430	1703L
		10	245kpa	245kpa	704L

REMARKS:

Fig E-36: Water Pressure Testing Report (NL 2/5)



Fig E-37: Borehole NL 2/5 Core Box 1 of 6



Fig E-38: Borehole NL 2/5 Core Box 2 of 6



Fig E-39: Borehole NL 2/5 Core Box 3 of 6



Fig E-40: Borehole NL 2/5 Core Box 4 of 6



Fig E-41: Borehole NL 2/5 Core Box 5 of 6



Fig E-42: Borehole NL 2/5 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

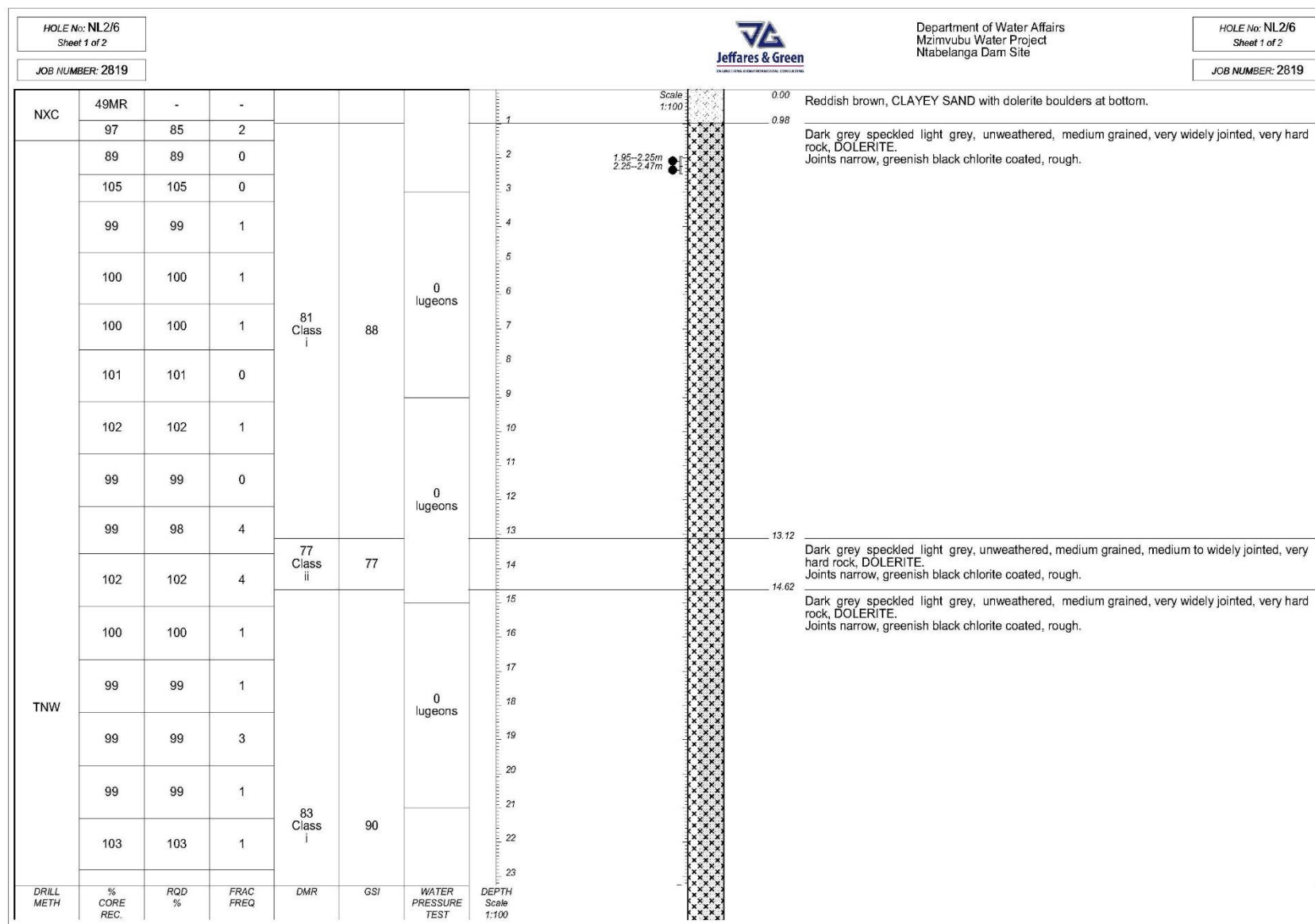


Fig E-43-1: Borehole Logs (NL 2/6)

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GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

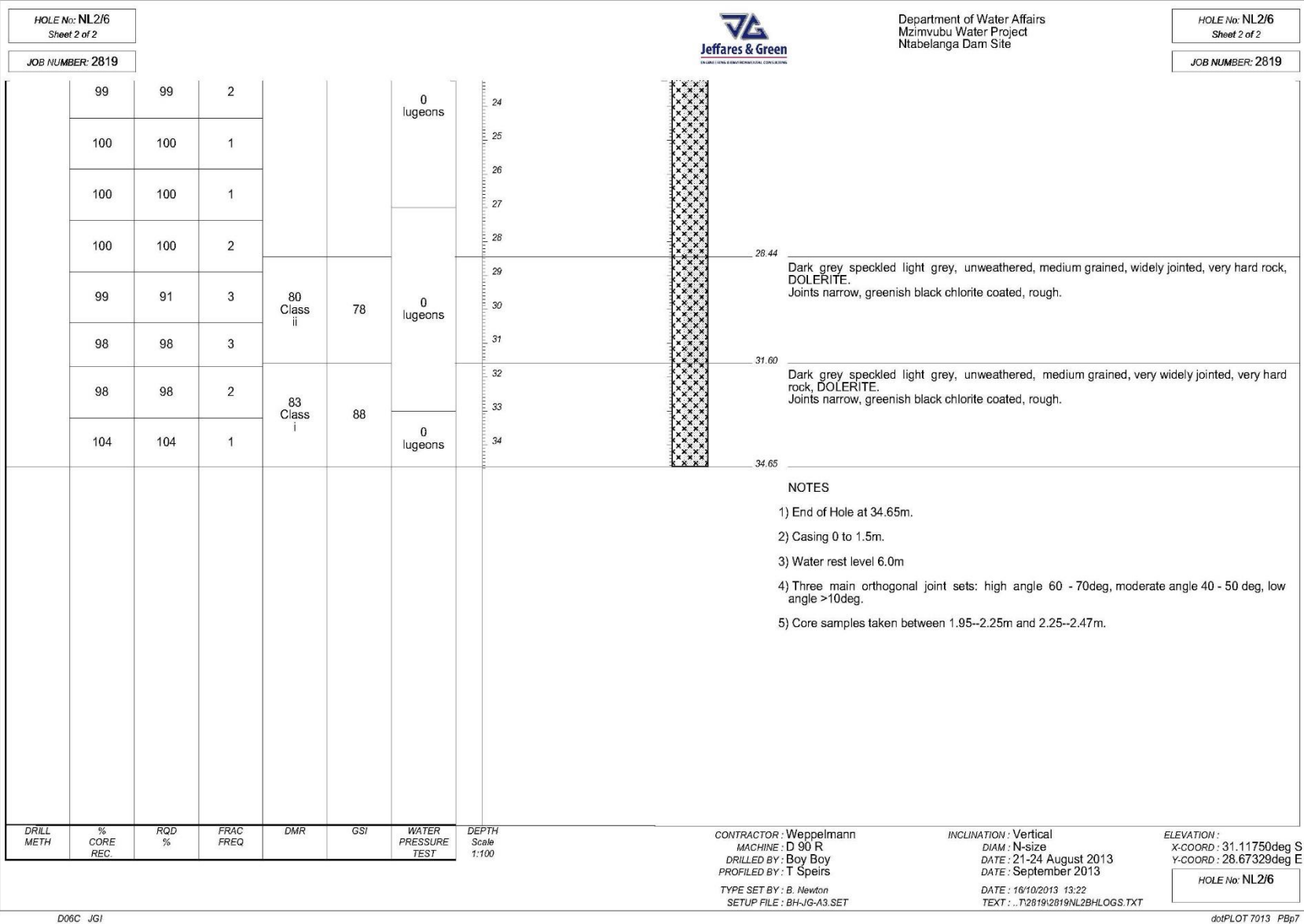


Fig E-43-1: Borehole Logs (NL 2/6)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/6

DRILLER: Boy-Boy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE	PRESURES	WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
23/08/2013 DP	FROM	10 min	25 kpa		0 L
	3,00	10 min	50		0
	TO	10 min	70		0
	9,00	10 min	50		0
		10 min	25		0
DP	FROM	10 min	80 kpa		0 L
	9,00	10 min	140		0
	TO	10 min	200		0
	15,00	10 min	140		0
		10 min	80		0
DP	FROM	10 min	135 kpa		0 L
	15,00	10 min	240		0
	TO	10 min	340		0
	21,00	10 min	240		0
		10 min	135		0
DP	FROM	10 min	190 kpa		0 L
	21,00	10 min	330		0
	TO	10 min	475		0
	27,00	10 min	330		0
		10 min	190		0
DP	FROM	10 min	245 kpa		0 L
	27,00	10 min	430		0
	TO	10 min	610		0
	33,00	10 min	430		0
		10 min	245		0
SP	FROM	10 min	300 kpa		0 L
	33,00	10 min	520		0
	TO	10 min	745		0
	34.65	10 min	520		0
		10 min	300		0

REMARKS:

Fig E-44: Water Pressure Testing Report (NL 2/6)



Fig E-45: Borehole NL 2/6 Core Box 1 of 5



Fig E-46: Borehole NL 2/6 Core Box 2 of 5



Fig E-47: Borehole NL 2/6 Core Box 3 of 5



Fig E-48: Borehole NL 2/6 Core Box 4 of 5



Fig E-49: Borehole NL 2/6 Core Box 5 of 5

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

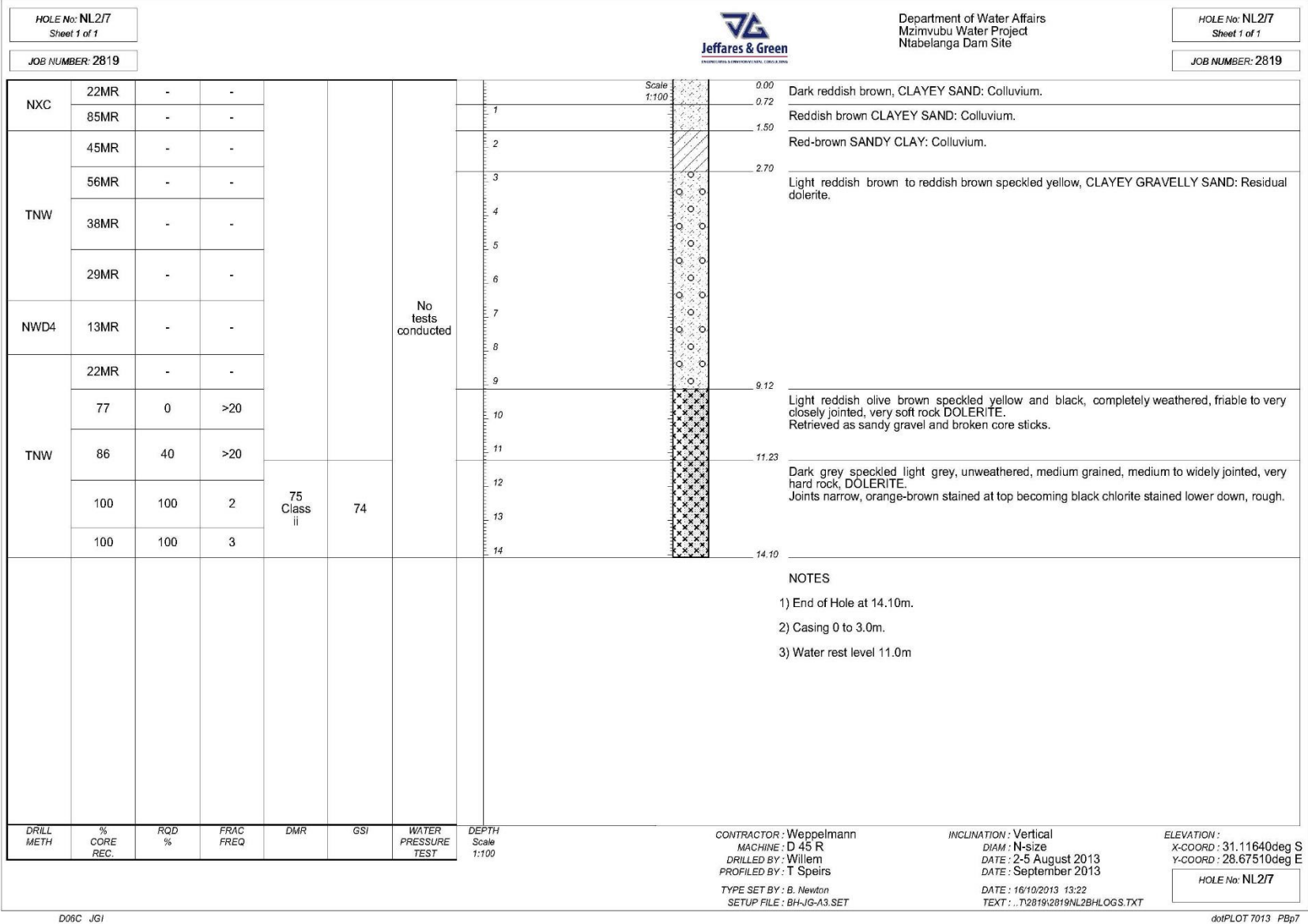


Fig E-50: Borehole Logs (NL 2/7)



Fig E-51: Borehole NL 2/7 Core Box 1 of 2



Fig E-51: Borehole NL 2/7 Core Box 2 of 2

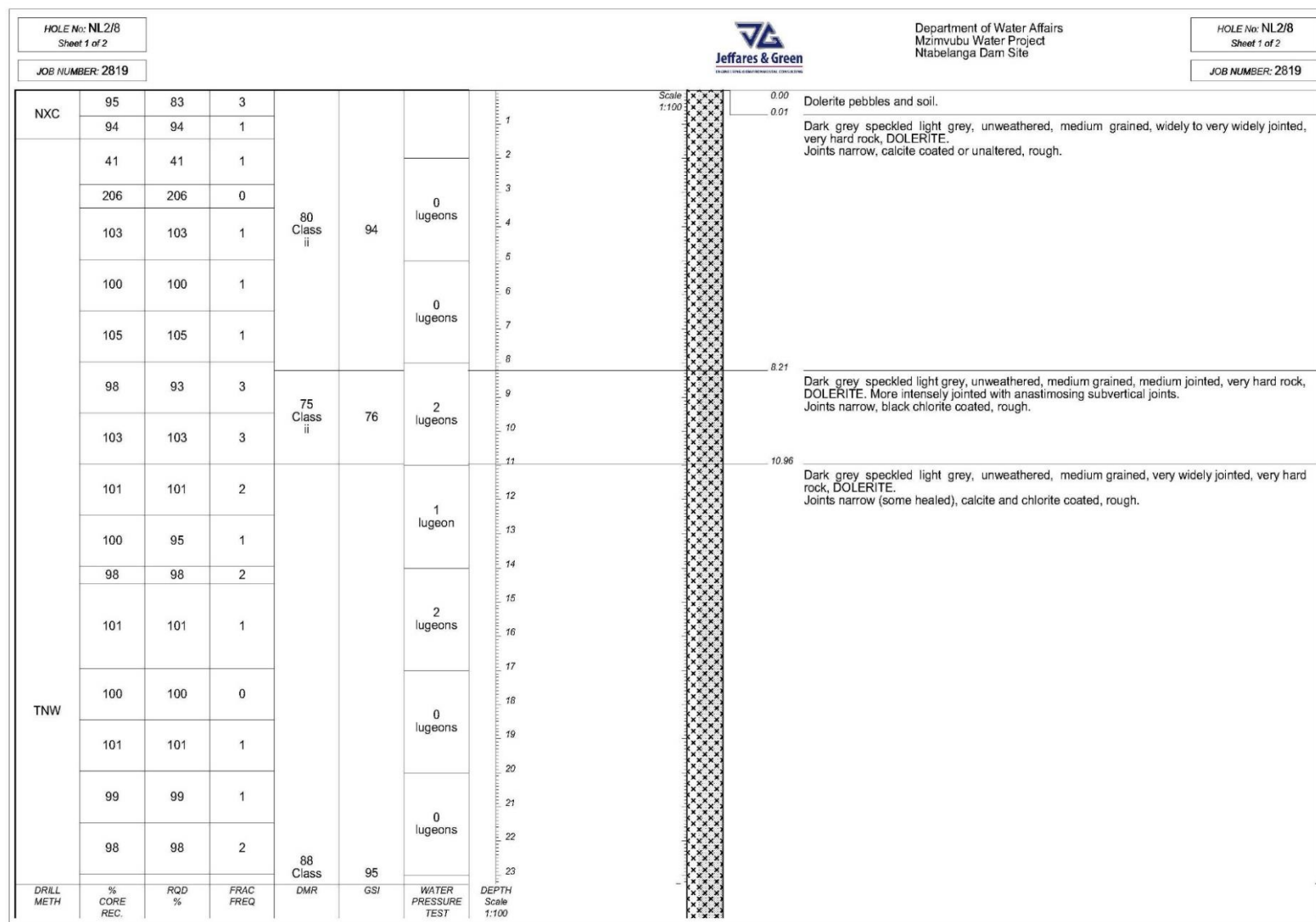


Fig E-52-1: Borehole Logs (NL 2/8)

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GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

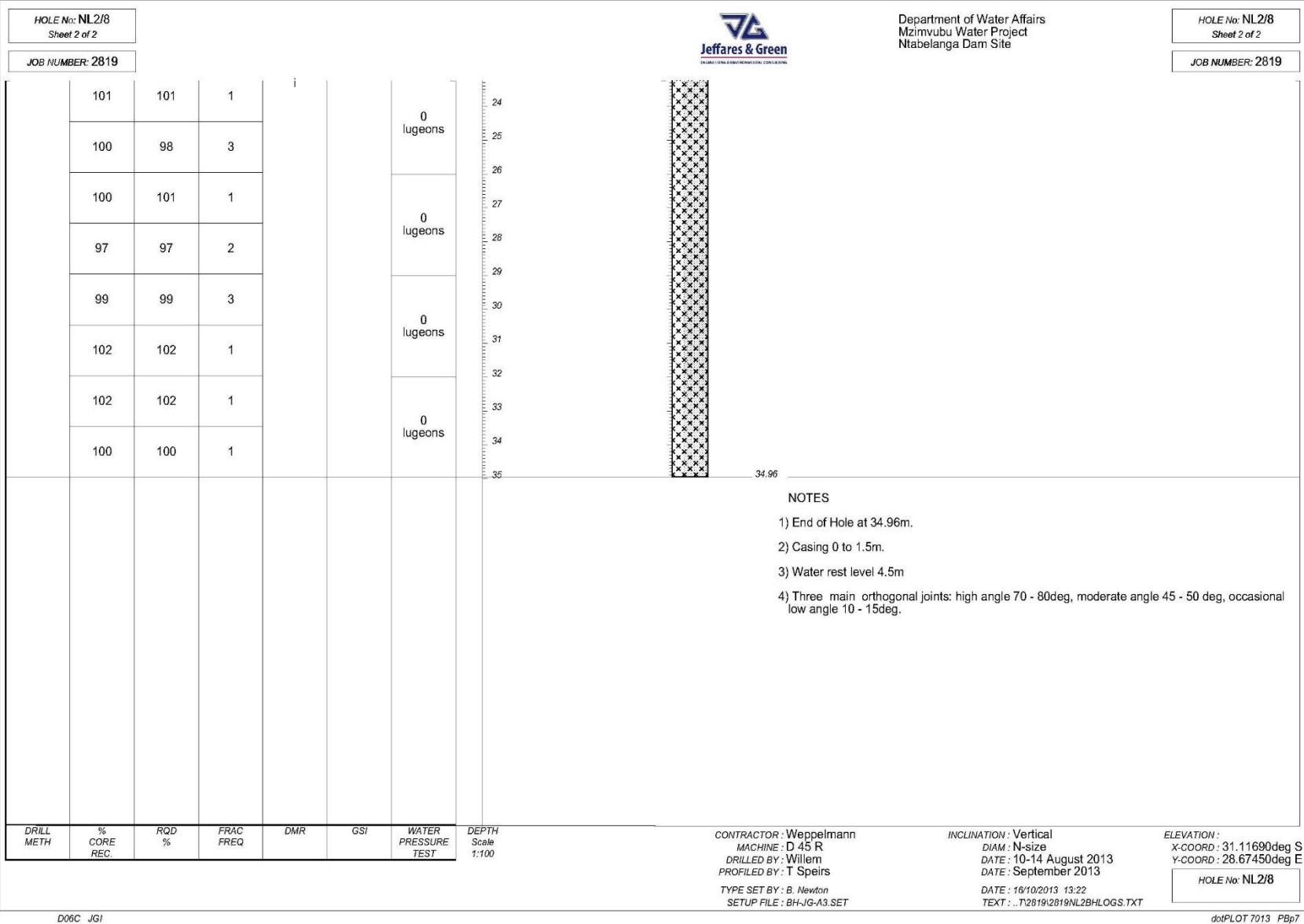


Fig E-52-2: Borehole Logs (NL 2/8)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/8

DRILLER: Willem

DATE & Packer Description	STAGES	TESTING TIME	GAUGE PRESURES		WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
DP	FROM 2.00m	10	20kpa	20kpa	74L
		10	30	30	4L
	TO 5.00m	10	45	45	1L
		10	30	30	0L
		10	20kpa	20kpa	0L
DP	FROM 5.00m	10	45kpa	45kpa	0L
		10	80	80	0L
	TO 8.00m	10	115	115	1L
		10	80	80	0L
		10	45kpa	45kpa	0L
DP	FROM 8.00m	10	70kpa	70kpa	3L
		10	130	130	25L
	TO 11.00m	10	180	180	11L
		10	130	130	20L
		10	70kpa	70kpa	2L
DP	FROM 11.00m	10	100kpa	100kpa	6L
		10	170	170	24L
	TO 14.00m	10	250	250	0L
		10	170	170	1L
		10	100kpa	100kpa	3L
DP	FROM 14.00m	10	125kpa	125kpa	6L
		10	220	220	6L
	TO 17.00m	10	320	320	108L
		10	220	220	6L
		10	125kpa	125kpa	15L
DP	FROM 17.00m	10	155kpa	155kpa	264L
		10	270	270	6L
	TO 20.00m	10	385	385	0L
		10	270	270	1L
		10	155kpa	155kpa	1L
DP	FROM 20.00m	10	180kpa	180kpa	3L
		10	320	320	2L
	TO 23.00m	10	450	450	6L
		10	320	320	2L
		10	180kpa	180kpa	1L
DP	FROM 23.00m	10	210kpa	210kpa	2L
		10	365	365	2L
	TO 26.00m	10	520	520	4L
		10	365	365	5L
		10	201kpa	201kpa	3L
14/08/2013 DP	FROM 26.00m	10	325kpa	325kpa	4L
		10	410	410	5L
	TO 29.00m	10	590	590	2L
		10	410	410	7L
		10	325kpa	325kpa	3L
DP	FROM 29.00m	10	265kpa	265kpa	3L
		10	460	460	1L
	TO 32.00m	10	665	665	2L
		10	460	460	4L
		10	265kpa	265kpa	3L
SP	FROM 32.00m	10	290kpa	290kpa	3L
		10	510	510	6L
	TO End of Borehole	10	725	725	5L
		10	510	510	1L
		10	290kpa	290kpa	2L

REMARKS:

Fig E-53: Water Pressure Testing Report (NL 2/8)



Fig E-54: Borehole NL 2/8 Core Box 1 of 5



Fig E-55: Borehole NL 2/8 Core Box 2 of 5



Fig E-56: Borehole NL 2/8 Core Box 3 of 5



Fig E-57: Borehole NL 2/8 Core Box 4 of 5



Fig E-58: Borehole NL 2/8 Core Box 5 of 5

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

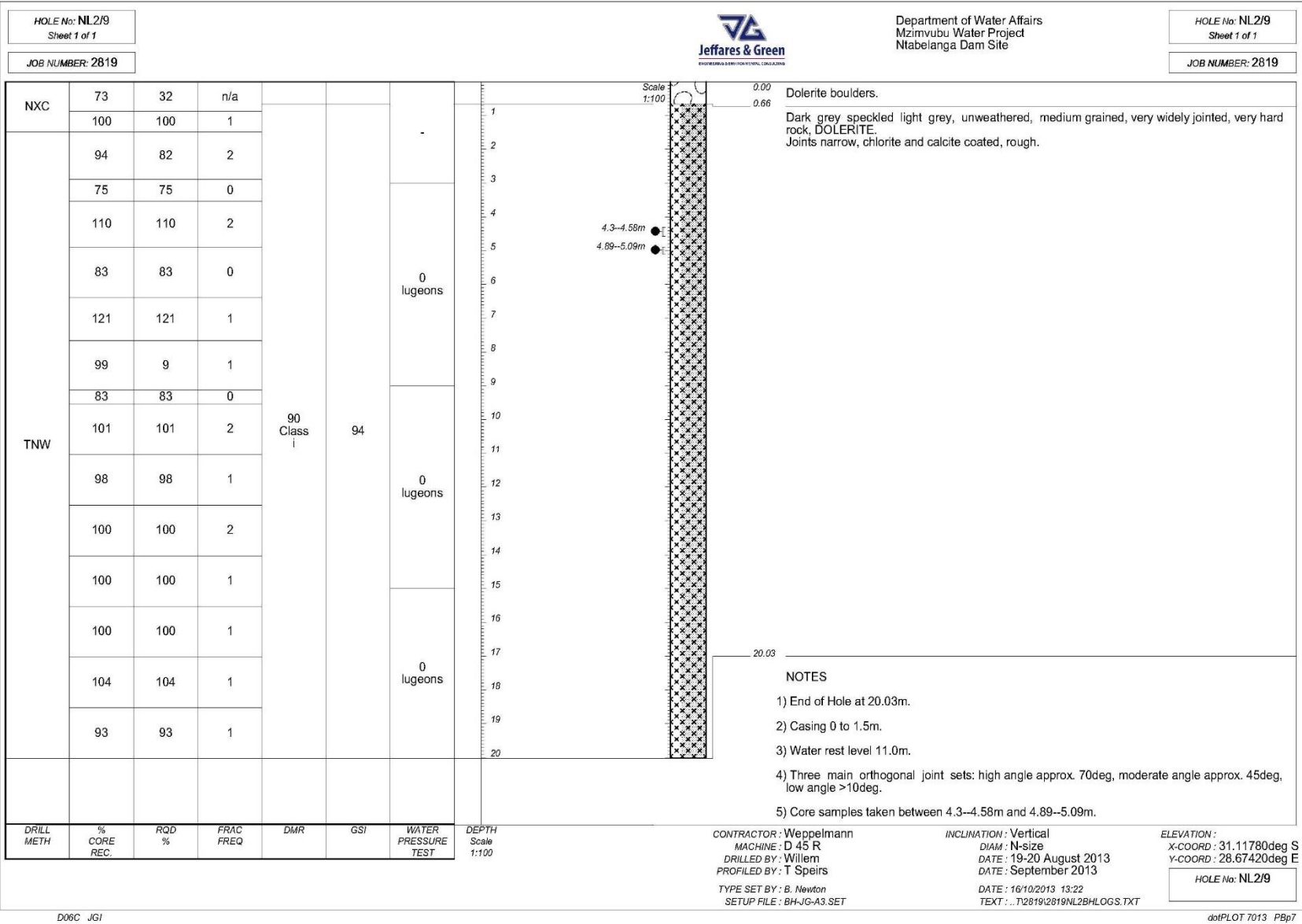


Fig E-59: Borehole Logs (NL 2/9)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/9

DRILLER: Willem

DATE & Packer Description	STAGES	TESTING TIME	GAUGE	PRESURES	WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
22/08/2013 DP	FROM	10 min	25 kpa		0 L
	3	10 min	50		0
	TO	10 min	70		0
	9	10 min	50		0
		10 min	25		0
DP	FROM	10 min	80 kpa		0 L
	9	10 min	140		0
	TO	10 min	200		0
	15	10 min	140		0
		10 min	80		0
SP	FROM	10 min	135 kpa		0 L
	15	10 min	240		0
	TO	10 min	340		0
	20.03	10 min	240		0
		10 min	135		0

REMARKS:

Fig E-60: Water Pressure Testing Report (NL 2/9)



Fig E-61: Borehole NL 2/9 Core Box 1 of 3



Fig E-62: Borehole NL 2/9 Core Box 2 of 3



Fig E-63: Borehole NL 2/9 Core Box 3 of 3

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

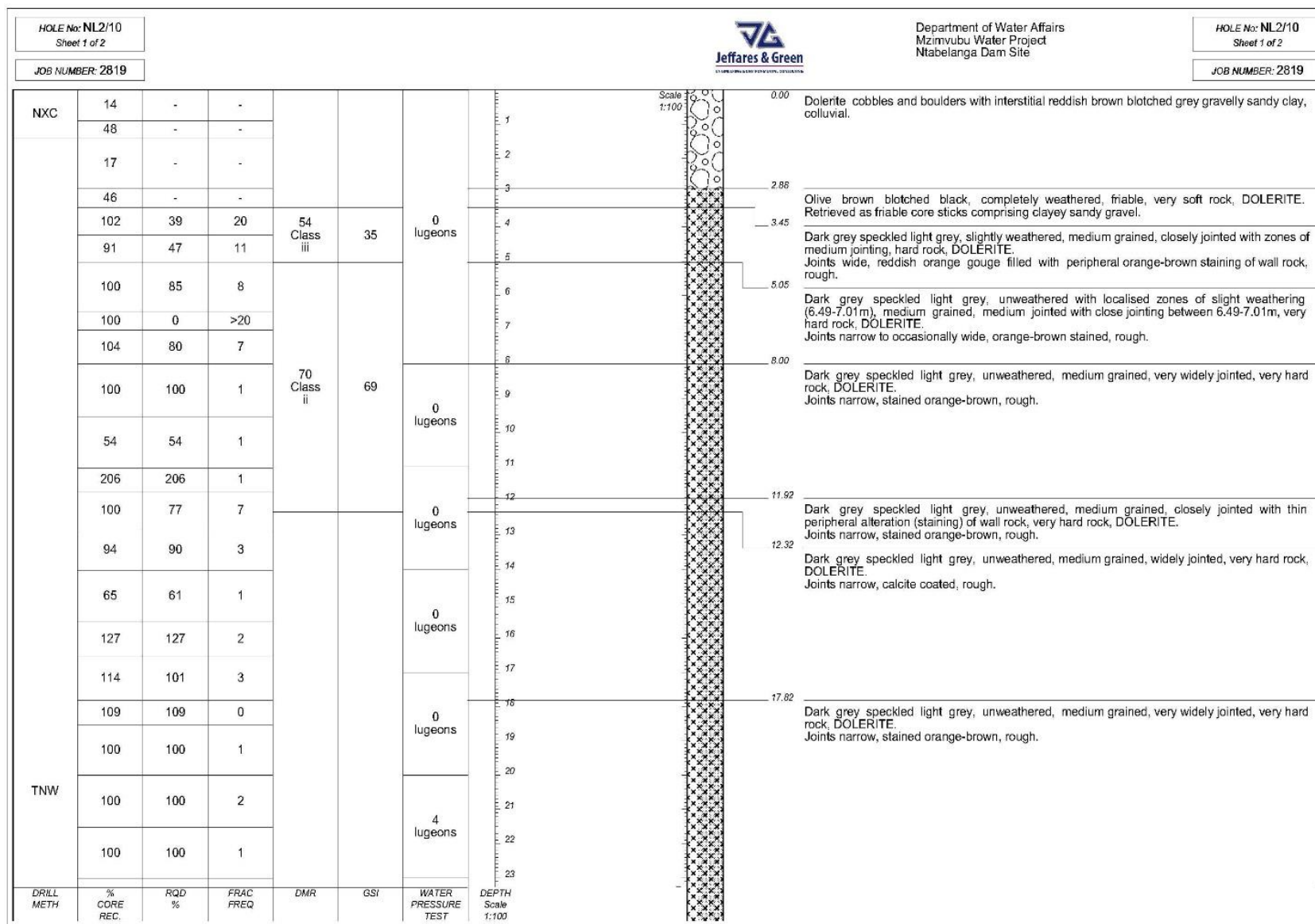


Fig E-64-1: Borehole Logs (NL 2/10)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

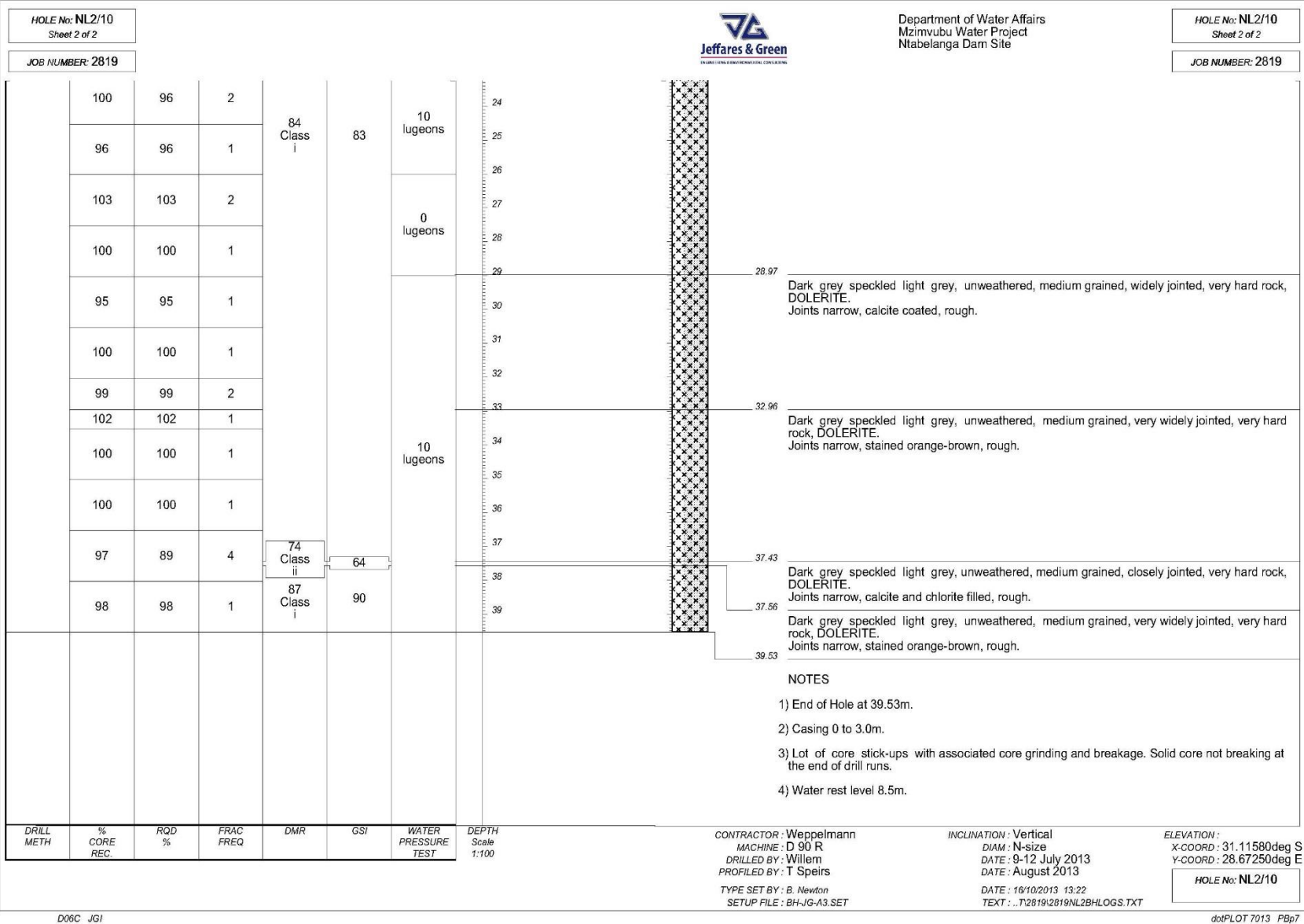


Fig E-64-2: Borehole Logs (NL 2/10)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river
 DRILLER: Willem

BOREHOLE NR: NL 2/10

DATE & Packer Description	STAGES	TESTING TIME	GAUGE	PRESURES	WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
20-Jul DP	FROM 5.00m	10	45kpa	45kpa	190L
		10	80kpa	80kpa	9L
	TO 8.00m	10	115kpa	115kpa	261L
		10	80kpa	80kpa	90L
		10	115kpa	115kpa	0
DP	FROM 8.00m	10	70kpa	70kpa	0
		10	130kpa	130kpa	1L
	TO 11.00m	10	180kpa	180kpa	0
		10	130kpa	130kpa	0
		10	70kpa	70kpa	0
DP	FROM 11.00m	10	100kpa	100kpa	0
		10	170kpa	170kpa	0
	TO 14.00m	10	250kpa	250kpa	0
		10	170kpa	170kpa	0
		10	100kpa	100kpa	0
DP	FROM 14.00m	10	125kpa	125kpa	0
		10	220kpa	220kpa	480L
	TO 17.00m	10	320kpa	320kpa	107L
		10	220kpa	220kpa	0
		10	125kpa	125kpa	0
DP	FROM 17.00m	10	155kpa	155kpa	0
		10	270kpa	270kpa	0
	TO 20.00m	10	358kpa	358kpa	0
		10	270kpa	270kpa	0
		10	155kpa	155kpa	0
21-Jul DP	FROM 20.00m	10	180kpa	180kpa	0
		10	320kpa	320kpa	684L
	TO 23.00M	10	450kpa	450kpa	1115L
		10	320kpa	320kpa	430L
		10	180kpa	180kpa	20L
DP	FROM 23.00m	10	210kpa	210kpa	29L
		10	365kpa	365kpa	0
	TO 26.00m	10	520kpa	520kpa	715L
		10	365kpa	365kpa	360L
		10	210kpa	210kpa	61L
DP	FROM 26.00m	10	235kpa	235kpa	2L
		10	410kpa	410kpa	542L
	TO 29.00m	10	590kpa	590kpa	721L
		10	410kpa	410kpa	458L
		10	235kpa	235kpa	0
SP	FROM 29.00m	10	265kpa	265kpa	250L
		10	460kpa	460kpa	962L
	TO	10	655kpa	590kpa	731L
		10	460kpa	460kpa	567L
		10	265kpa	265kpa	289L

REMARKS: Single packer used from 29.00m to bottom of BH. Due to bubble packer not advancing closure of BH

Fig E-65: Water Pressure Testing Report (NL 2/10)



Fig E-66: Borehole NL 2/10 Core Box 1 of 6



Fig E-67: Borehole NL 2/10 Core Box 2 of 6



Fig E-68: Borehole NL 2/10 Core Box 3 of 6



Fig E-69: Borehole NL 2/10 Core Box 4 of 6



Fig E-70: Borehole NL 2/10 Core Box 5 of 6



Fig E-71: Borehole NL 2/10 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
 GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

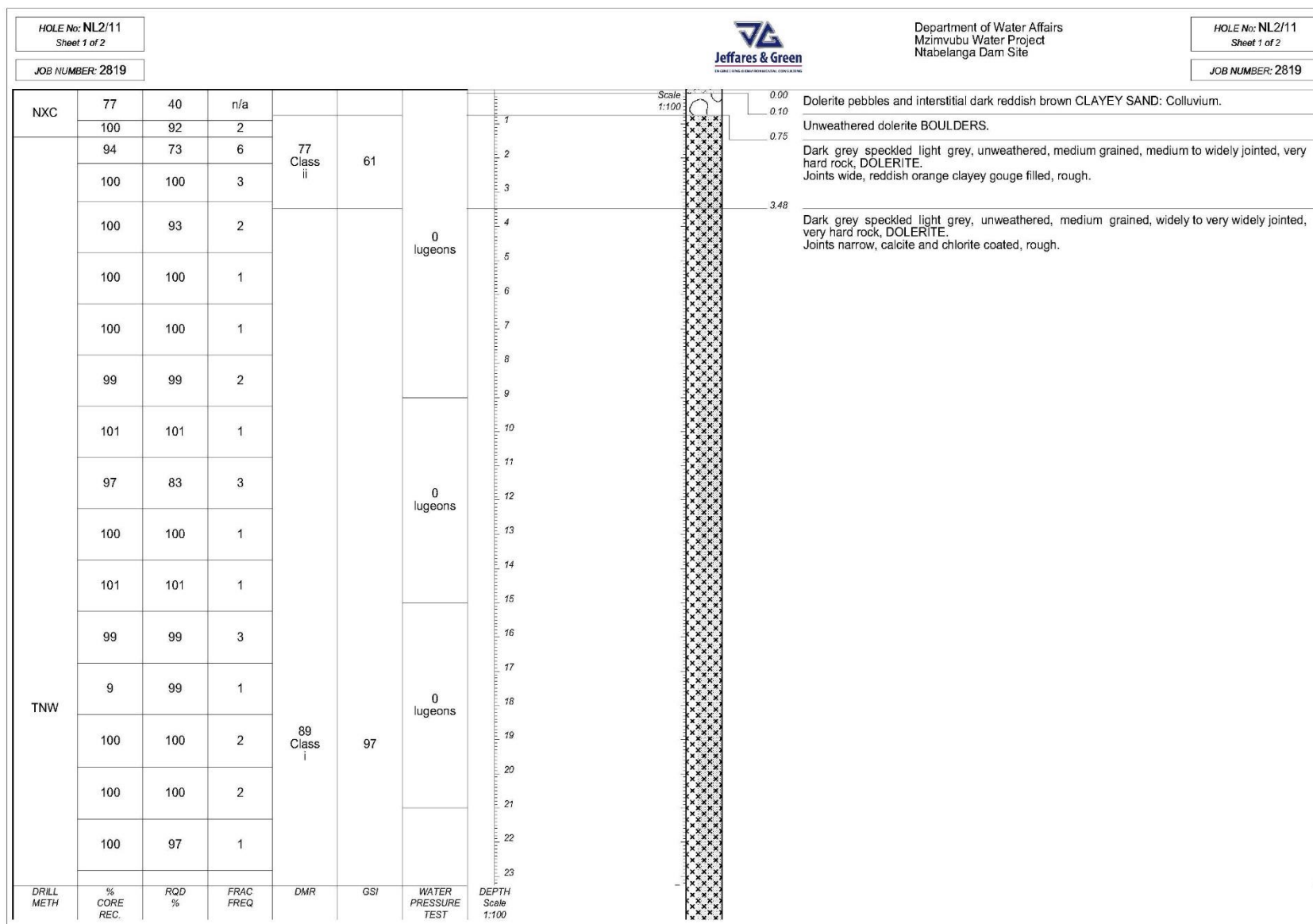


Fig E-72-1: Borehole Logs (NL 2/11)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

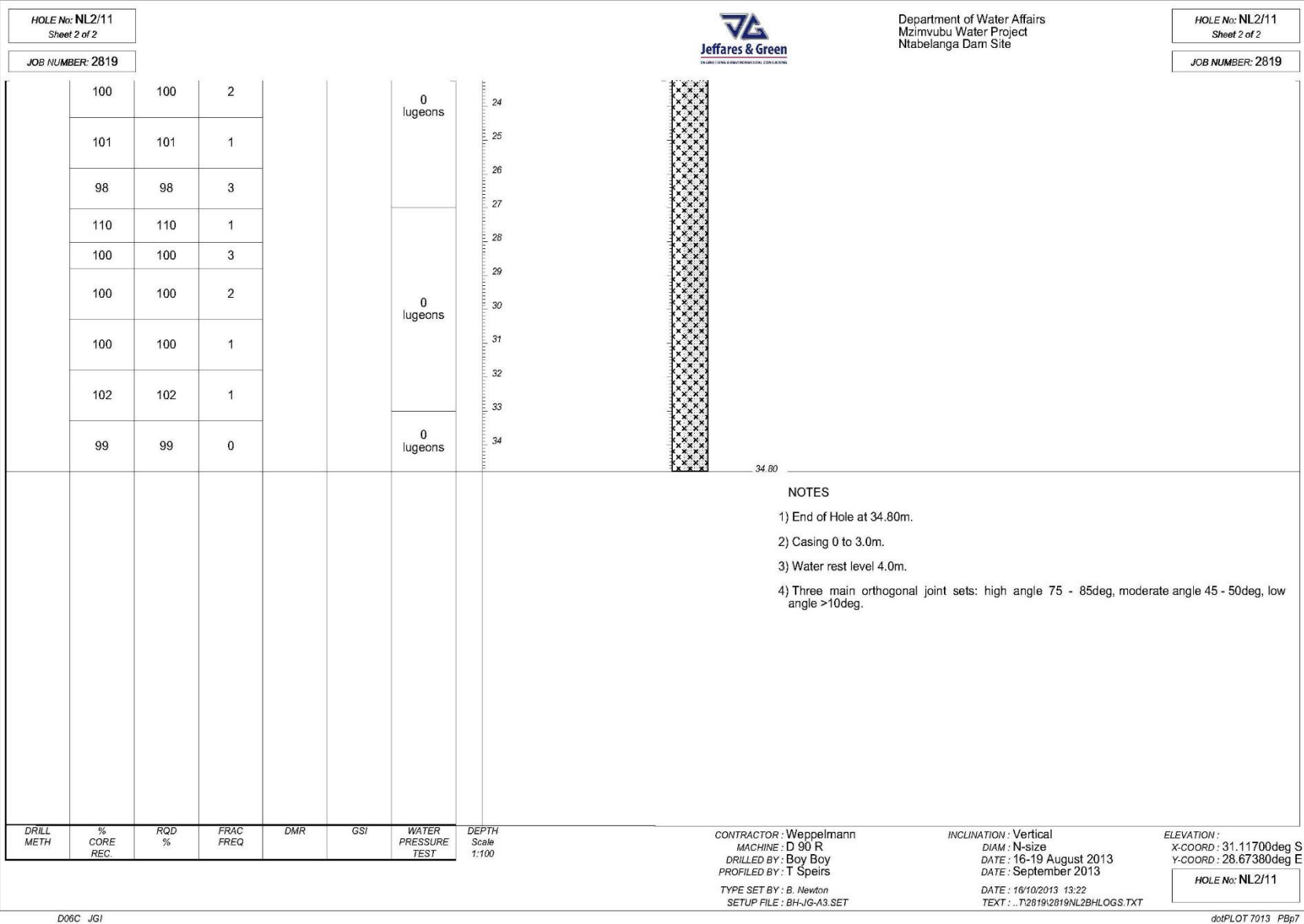


Fig E-72-2: Borehole Logs (NL 2/11)



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Report on Waterpressure Testing

SCHEME: Mzimvubu river

BOREHOLE NR: NL 2/11

DRILLER: Boyboy

DATE & Packer Description	STAGES	TESTING TIME	GAUGE	PRESURES	WATER INTAKE BY HOLE
	METERS	REQUIRED MINUTES	REQUIRED PRESSURES	ACTUAL PRESSURES	TOTAL LITRES
20/08/2013 DP	FROM 3.00m	10	25 kpa		0 L
		10	50		0
	TO 9.00m	10	70		0
		10	50		0
		10	25		0
DP	FROM 9.00m	10	80 kpa		0 L
		10	140		0
	TO 15.00m	10	200		0
		10	140		0
		10	80		0
DP	FROM 15.00m	10	135 kpa		0 L
		10	240		0
	TO 21.00m	10	340		0
		10	240		0
		10	135		0
DP	FROM 21.00m	10	190 kpa		0 L
		10	330		0
	TO 27.00m	10	475		0
		10	330		0
		10	190		0
DP	FROM 27.00m	10	245 kpa		0 L
		10	430		0
	TO 33.00m	10	610		0
		10	430		0
		10	245		0
SP	FROM 33.00m	10	300 kpa		0 L
		10	520		0
	TO 34.80M	10	745		0
	End of hole	10	520		0
		10	300		0

REMARKS:

Fig E-73: Water Pressure Testing Report (NL 2/11)



Fig E-74: Borehole NL 2/11 Core Box 1 of 6



Fig E-75: Borehole NL 2/11 Core Box 2 of 6



Fig E-76: Borehole NL 2/11 Core Box 3 of 6



Fig E-77: Borehole NL 2/11 Core Box 4 of 6



Fig E-78: Borehole NL 2/11 Core Box 5 of 6



Fig E-79: Borehole NL 2/11 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

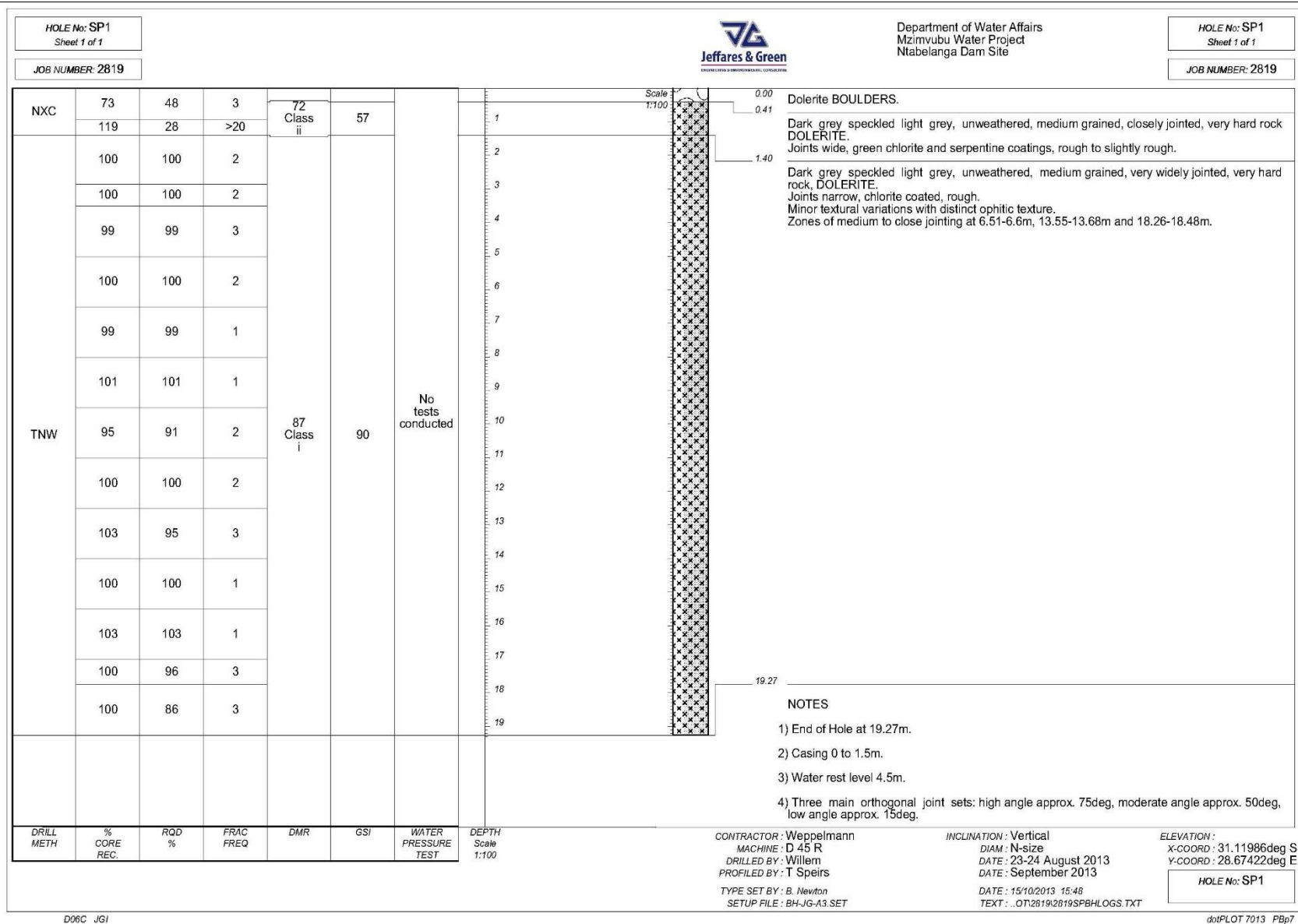


Fig E-80: Borehole Logs (SP 1)



Fig E-81: Borehole SP 1 Core Box 1 of 3



Fig E-82: Borehole SP 1 Core Box 2 of 3



Fig E-83: Borehole SP 1 Core Box 3 of 3

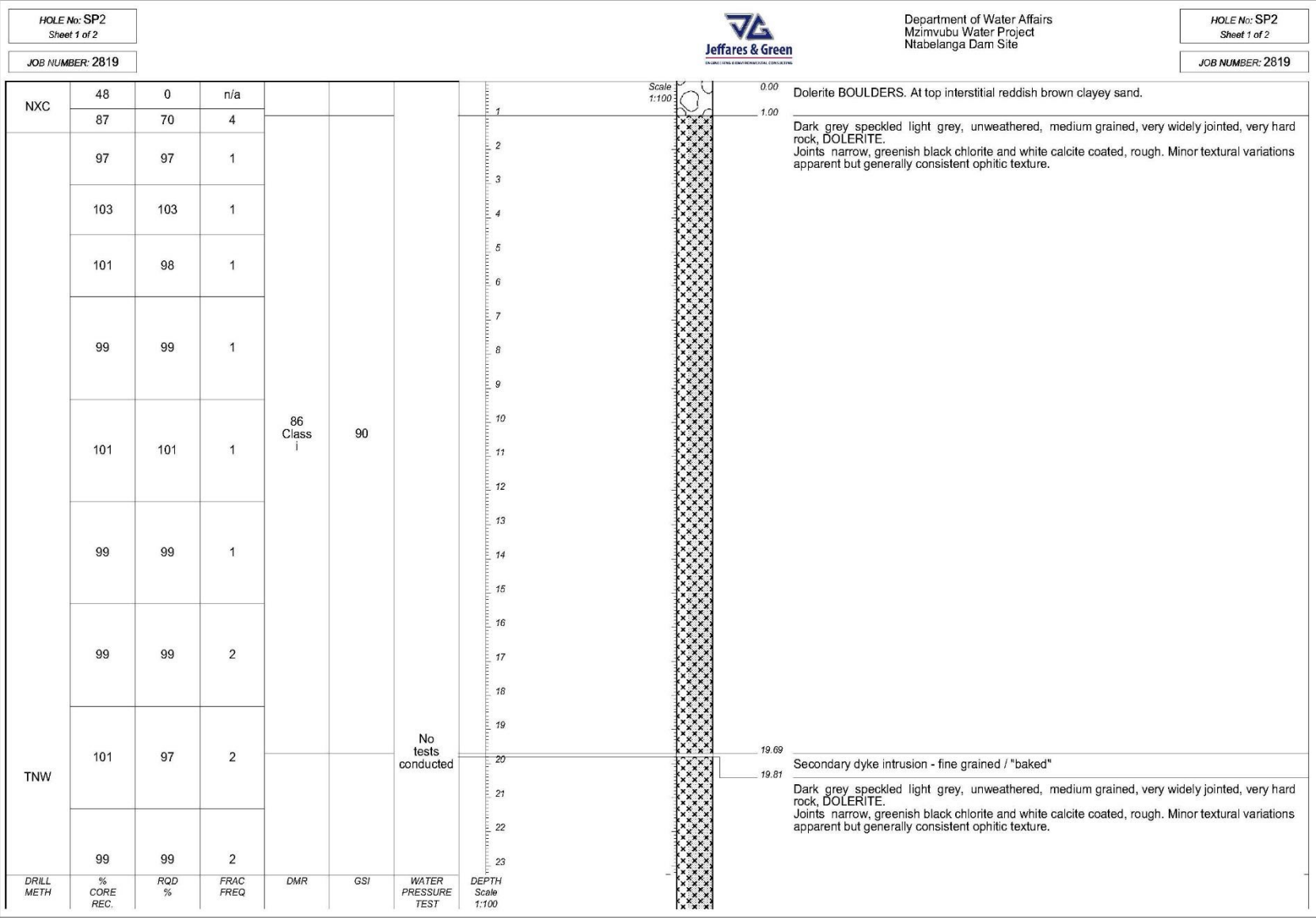


Fig E-84-1: Borehole Logs (SP 2)

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

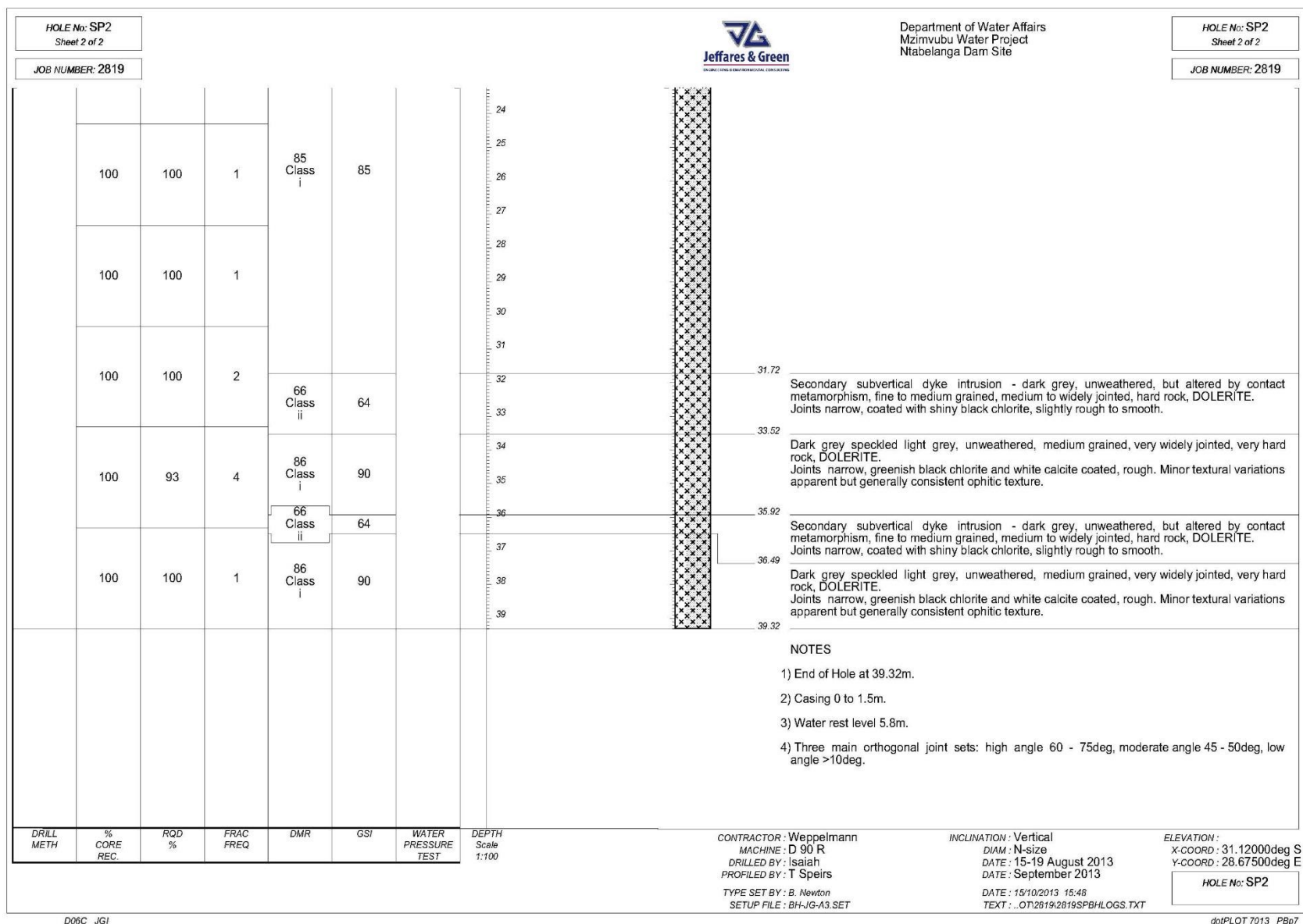


Fig E-84-2: Borehole Logs (SP 2)



Fig E-85: Borehole SP 2 Core Box 1 of 6



Fig E-86: Borehole SP 2 Core Box 2 of 6



Fig E-87: Borehole SP 2 Core Box 3 of 6



Fig E-88: Borehole SP 2 Core Box 4 of 6



Fig E-89: Borehole SP 2 Core Box 5 of 6



Fig E-90: Borehole SP 2 Core Box 6 of 6

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

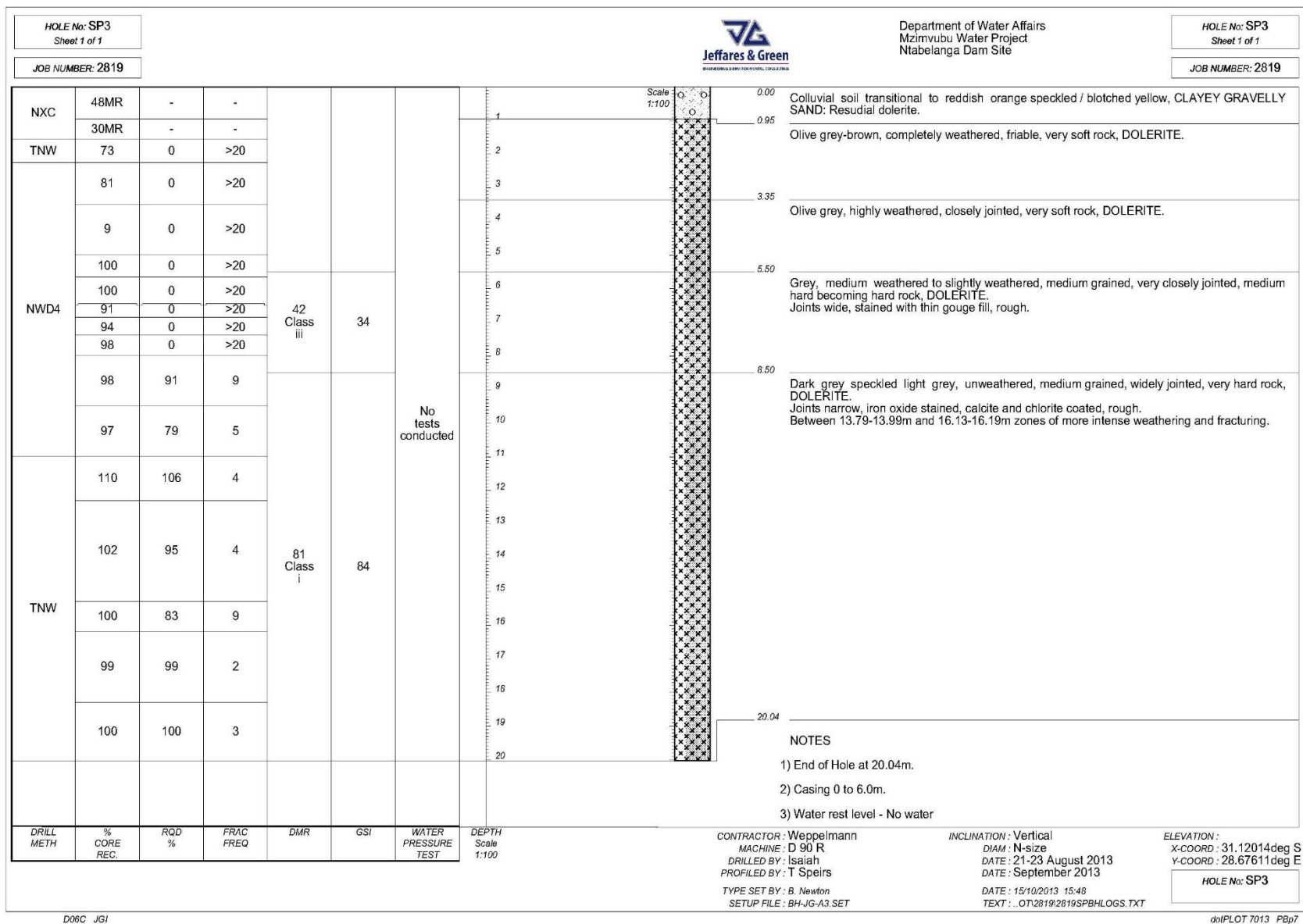


Fig E-91: Borehole Logs (SP 3)



Fig E-92: Borehole SP 3 Core Box 1 of 3



Fig E-93: Borehole SP 3 Core Box 2 of 3



Fig E-94: Borehole SP 3 Core Box 3 of 3

APPENDIX F

COUNCIL FOR GEOSCIENCE REPORT ON SEISMIC REFRACTION AND ELECTRICAL RESISTIVITY SURVEYS



Council for Geoscience



Council for Geoscience

Report on the Refraction Seismic and Electrical Resistivity surveys

Prepared for

Jeffares & Green (Pty) Ltd for the Ntabelanga dam site feasibility study.

By

M. Sethobya, P. Nyabeze and R. Legotlo.

Council for Geoscience, South Africa

Project No: C0- 2010-5122

Report No:2013-0257

Confidential

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Executive Summary

Refraction seismic and Electrical Resistivity tomography(ERT) surveys were conducted as part of the Mzimvubu water project at the Ntabelanga Dam site along the Tsitsa river, by the Council for Geoscience on behalf of Jefferson and Green(Pty) Ltd as part of their geotechnical investigations. The main aims of the surveys were to accurately determine;

1. the thickness of the overburden (transported and residual soils) that overly the bedrock
2. the depth to bedrock and
3. Determine the rippability of the profile at the dam site

The surveys were carried out at predetermined lines at each side of the river. For purposes of easy data management, each portion (spread of measured line) was treated as an individual line. A total of 4 lines were surveyed. See figure 1. All the lines were sampled at 5m intervals for both the Seismics and ERT surveys. Data was collected at exactly the same points/stations for the two techniques to ensure accuracy in comparing the results. The 24 channel Seistronox seismograph was used to do the seismic surveys. A sledge hammer and base plate were used as a source of energy.

Very high quality shots were observed with stacking and repeat shots being taken for quality control purposes. For the ERT surveys, an IRIS automated resistivity meter-Syscal Pro Switch 72 was employed to acquire ground resistivity data. The lines were then marked with a handheld Garmin SCx60. The topography for data processing was surveyed using a submeter accuracy Leica RS20 differential GPS.

1 INTRODUCTION

1.1 BACKGROUND

The Council for Geoscience was appointed by Jeffares & Green (Pty) Ltd in August 2013 to conduct Geophysical Seismic and multi-Electrode Resistivity Tomography (ERT) Investigations. The investigations were to be carried out at specifically selected lines at the intended Ntabelanga Dam site along the Tsitsa river, for the Mzimvu Water project near the town of Tsolo, Eastern Cape province. The seismic surveys were meant to augment the drilling being carried out by the client and to allow interpolation between and extrapolation from borehole data in order to determine overburden thickness, depth to bedrock and to determine the rippability of the profile at the dam site location as part of the engineering properties classification for the dam design.

The specified survey areas as per the terms of reference are summarized in Table 1 with a total of 810m having been marked for the Seismic and ERT surveys.

Table 1

Location	Line Length	Measured length(Seismics)	Measured length(ERT)	Borehole/s intersected
Line 1	180m	180m	180m	NL29, NL26 & N2.
Line 2	180m	180m	270m	N2
Line 3	180m	180m	180m	N3
Line 4	180m	180m	180m	N1

1.2 OBJECTIVES

As part of the augmentation of the drilling program information, the main aims of the seismic investigations were to accurately determine;

1. the thickness of the overburden (transported and residual soils) that overly the bedrock
2. the depth to bedrock and
3. Determine the rippability of the profile at the dam site location
- 4.

The seismic and ERT survey results are also to be used for interpolation between and extrapolation from borehole data.

2 GEOLOGY OF THE AREA.

The area falls within the Ntabene formation of the Molteno subgroup in the main Karoo sequence. Predominant lithological bodies are the sandstones, red mudstones and shale, with dolerite intrusions(Johnson et al,2006),which are clearly mapped around the survey area. Position of the survey area follows a dolerite outcrop on the south-eastern side of the river and a relatively thick mudstone cover overlying sandstone beds in the western side of the river(figure 1). As a dam design strategy, excavation is envisaged to reach depths of the competent dolerite body to ensure support of the foundation structure.

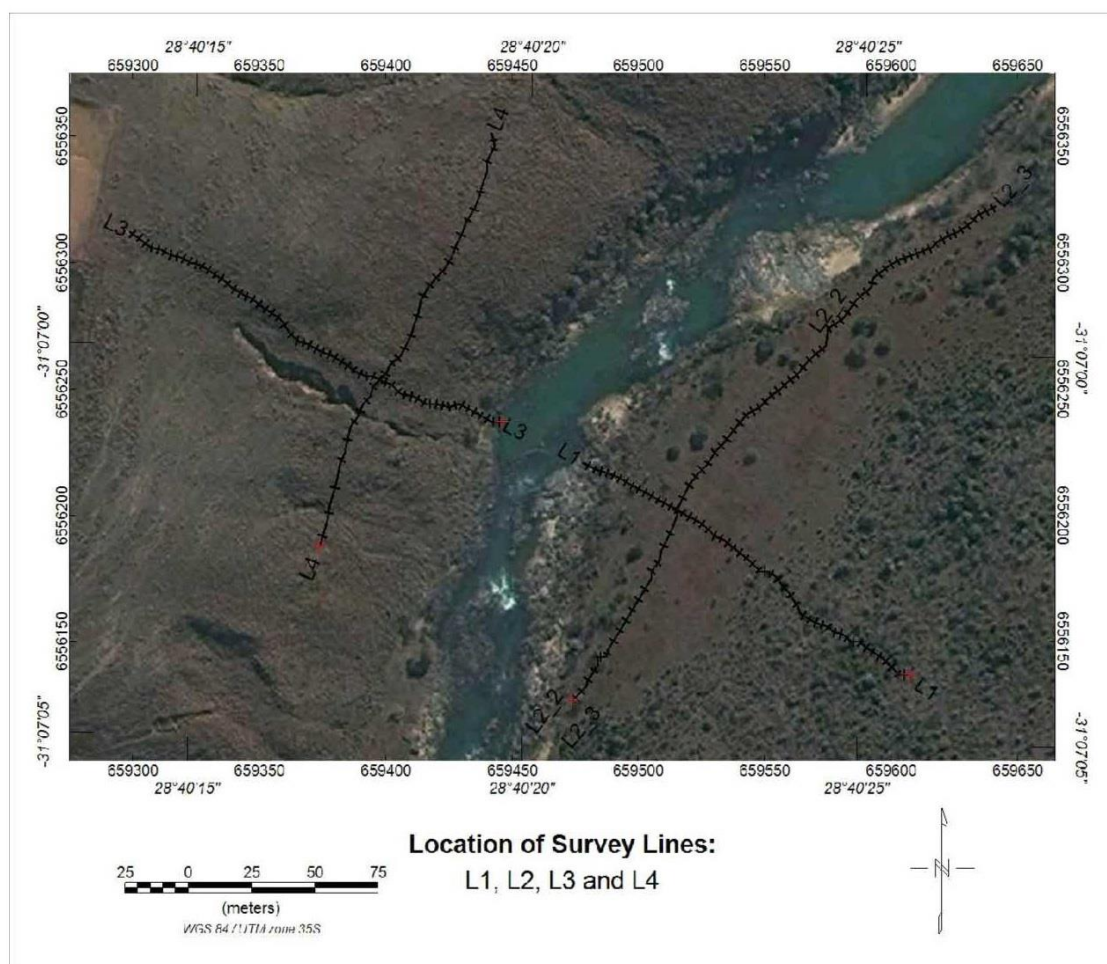


Figure 1 :The survey area showing location of the surveyed lines. The red marks indicate the start positions of the Seismics and ERT lines



3 METHODOLOGY

3.1 SEISMIC METHOD OVERVIEW

Seismic methods measure the velocity of energy transmitted through the soil and rocks. Inferences can be made from observed velocities and then be used to determine subsurface information that include depth to bedrock, bedrock topography, rippability of geological layers as well as other geological information such as the presence of faults, fractures, shear zones and water. The method has an advantage of less interference common with other methods as it can be applied to investigations located near power lines, ferrous objects and areas with saturated clays and those with topographic irregularities.

3.2 SEISMIC DATA ACQUISITION AND QUALITY CONTROL

The Ras-24 is an exploration seismograph that is manufactured by Seistronix in the USA. This instrument is designed to carry out seismic refraction surveys and has the capability of using up to 24 channels to collect data in the field. The Ras 24 uses two seismic cables that are connected to a set of 24 geophones. The maximum distance between the géophones is 5m (as specified by the cable), with the maximum length being 115m. Distance between the geophones depends on the depth of investigation and the objectives of the survey. The Ras-24 permits the user to stack multiple shots on top of each other, which in-turn increase the data quality and minimise the noise. The acquisition parameters (sample interval, record length, delay, filters, stack mode and stack polarity) are chosen by looking at the geology of the area. If the parameters do not seem suitable when the survey is started, the parameters can be changed on site. Figure 2 shows the Seistronix Ras 24 seismograph with the trigger cable and the battery source connected to it.

To improve data quality stacking of shots was used per shot location in order to increase the signal to noise ratio. Depending on the signal strength of the arrivals a minimum of two signals were stacked if the arrival breaks were clear and distinct and in some cases up to twenty signals or more were stacked in order to amplify the signal to noise ratio especially for the off-set shots. For every shot location at least one or more repeat shot records were taken as an additional quality control measure for use during the data processing.

The Leica RS20 Differential GPS was used to take the coordinates of each geophone location and where poor satellite reception was encountered interpolation using the Leica program was done.



Figure 2. The seistronix Ras-24 seismograph with a battery source connected to it.

3.3 ELECTRIC RESISTIVITY TOMOGRAPHY (ERT)- METHOD OVERVIEW

Multi-electrode resistivity tomography (ERT) surveys deduce the subsurface resistivity distribution by making measurements on the ground surface. From these measurements, the true resistivity of the subsurface can be estimated. The main principle of ground electrical resistivity is based on that, the distribution of electrical potential in the ground around a current-carrying electrode depends on the electrical resistivity and distribution of surrounding soils and rocks. The resistivity survey consist of current and potential electrodes, the current is directly injected into the ground by two electrodes (C1 and C2) and the voltage measured by two potential electrodes (P1 and P2) as illustrated in Figure 3.

The true resistivity of the subsurface can be determined by inversion of the measured apparent resistivity values using a computer program. The current and potential electrodes are arranged in a linear array like Schlumberger, Wenner and dipole-dipole arrays. Each array is capable of performing a certain objective of the study; therefore the choice of the array is dependent on the nature of the study and the efficiency in acquiring data.

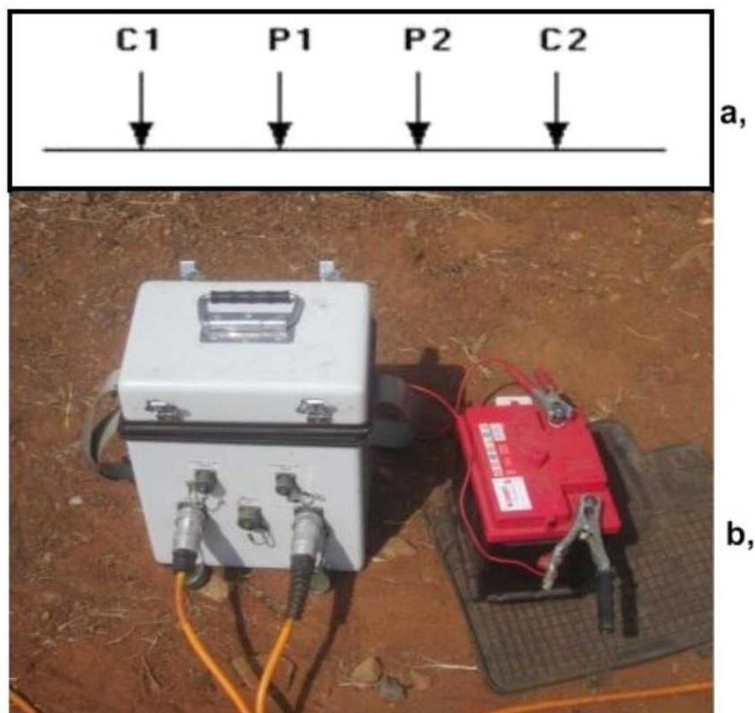


Figure 3. a, Illustration of the dipole-dipole electrode configuration as used in resistivity survey to measure subsurface resistivity. b, The IRIS Syscal Pro Switch 72 multi electrode resistivity instrument with a battery source.

3.4 ERT DATA ACQUISITION AND QUALITY CONTROL

ERT data was acquired using Syscal Pro Switch 72 multi electrode resistivity instrument (Figure 3). The instrument uses multi-core cables for controlling a set of 72 electrodes connected in a line. Resistivity data is measured automatically and stored in an internal memory. It has an internal 12V battery and an option to use an external battery for increased operation hours.

Dipole-dipole array was used to acquire data at 5 m electrode spacing to ensure more detailed data is acquired and maximum depth coverage at high lateral resolution.



4 DATA SUMMARY

4.1 SEISMICS

All lines were measured to a length of 180m owing to the nature of the seismic cables being used. Each cable measures a length of 60m(a single spread), thereby allowing 3 spreads per line. Efforts were made to measure lines at their exact locations and to cover the area closest to the river as best as possible.

4.2 ERT

All lines were measured to a distance of 180m using both the dipole dipole and Schlumberger arrays. The ERT lines were measured at the same positions where seismic data was collected, barring line 2, which had a 90m extension in the Northeastern direction(Figure 9).

A summary of the survey lines and coordinates is given in table 1.

Table 1: Summary of seismic and ERT traverses details as picked by the Leica DGPS.

Line	Length	Start Coordinates		End Coordinates	
Name	(m)	Lat	Long	Lat	Long
Line 1	180	-31.11781°	28.673819°	-31.11709°	28.6724991°
Line 2	180	-31.11793°	28.672465°	-31.11663°	28.673464°
Line 3	180	-31.116922°	28.672119°	-31.116267°	28.670562°
Line 4	180	-31.117380°	28.671368°	-31.115903°	28.672053°
Line 2_ext	270	-31.11793°	28.672465°	-31.11611°	28.674196°



5 DATA PROCESSING AND INTERPRETATION

5.1 SEISMICS

Data was dumped onto a PC from the Seismograph on a daily basis after field work. Shots were analysed for obvious noise and each shot was compared with its duplicate since 2 shots were taken per every shot location as a quality control procedure. At each shot location, multiple stacks were taken to ensure that high data quality is maintained. A method called the Plus-Minus method whereby the forward and reverse traveltimes are used to determine the depth to bedrock under each geophone was then used to do interpretation. This method entails entering the first arrivals for all shot configurations along the spread, plotting of traveltimes curves (using the spreadsheet plotting function), selection of the seismic velocities, and some simple column manipulation (Fourie and Odgers, 1995). The spreadsheet will then automatically calculate the parameters needed to determine the depth to the refractors and allows for elevation corrections.

Forward and reverse traveltimes are plotted against offset, from which the seismic velocity of the weathering layer and the refractor(s) may be determined. These velocities are then used to calculate the geometrical factor known as the k- factor for the refraction spread. The k-factor is then multiplied by the 'Plus' values to provide the depth to the refractor at each receiver location.

The 'Plus' values are obtained by adding the forward and reverse traveltimes at each receiver and subtracting the total traveltimes from the sum whilst the 'Minus' values calculated by subtracting the forward from the reverse at each receiver station. A plot of the minus versus the offset provides information on the refractor velocity given by:

(Refractor velocity = 2 x the slope of the Minus curve)

A reference velocity range plot is used to differentiate and interpret different rock types and formation based on their responses to seismic wave propagation.(figure 4)

5.2 ERT

After the data acquisition phase, data is stored in the internal memory of the instrument and downloaded onto a computer. The resistivity measurements are reduced to apparent resistivity values using the Prosys 11 software. The data is then interpreted using a 2D model that consists of a large number of rectangular blocks. A computer program (RES2DINV) is used to determine the resistivity of the blocks for the calculated apparent resistivity values to agree with the field measured values. Using the modeling program, 2D models of the subsurface resistivity are

generated. The modeled results are then exported to "XYZ" format and geo-referenced for 2D gridding in Geosoft software.

6 RESULTS

The results will be presented and discussed per specific line for both the techniques. The tables included in this section will represent the relative results comparisons for each line and deduced interpretations. Seismics results will be presented as 2D sections along the measured lines. ERT survey results are presented as 2D resistivity-depth models with the location of boreholes projected onto the models where applicable.

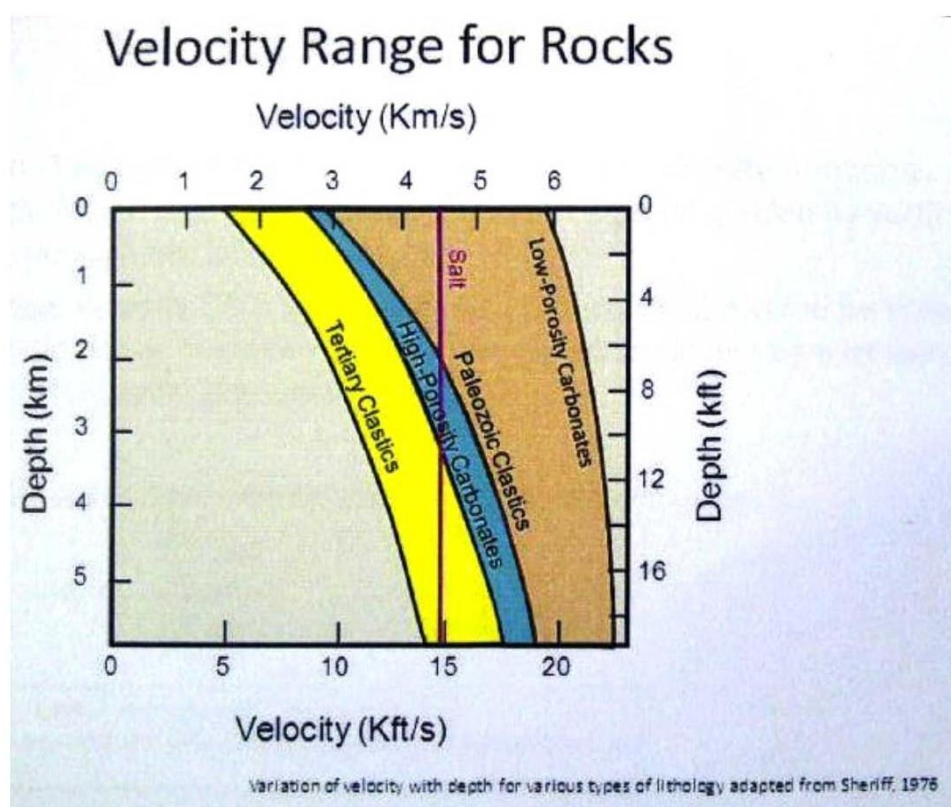


Figure 4. Reference seismic velocity range plot for rocks.(Adopted from Sheriff 1978, American Association of petroleum geologists.)

6.1 Line 1

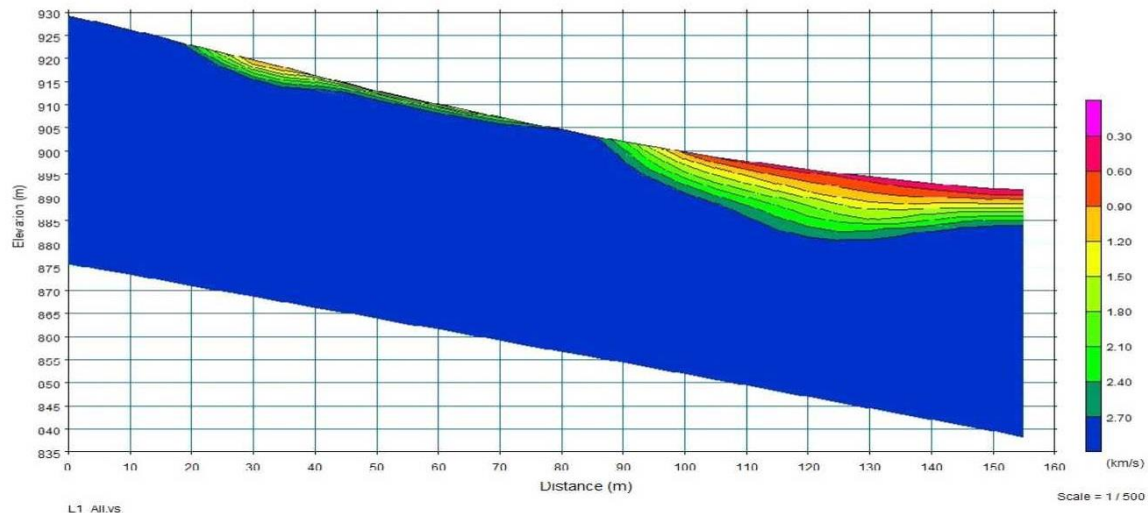


Figure 5. Seimics section along line 1.

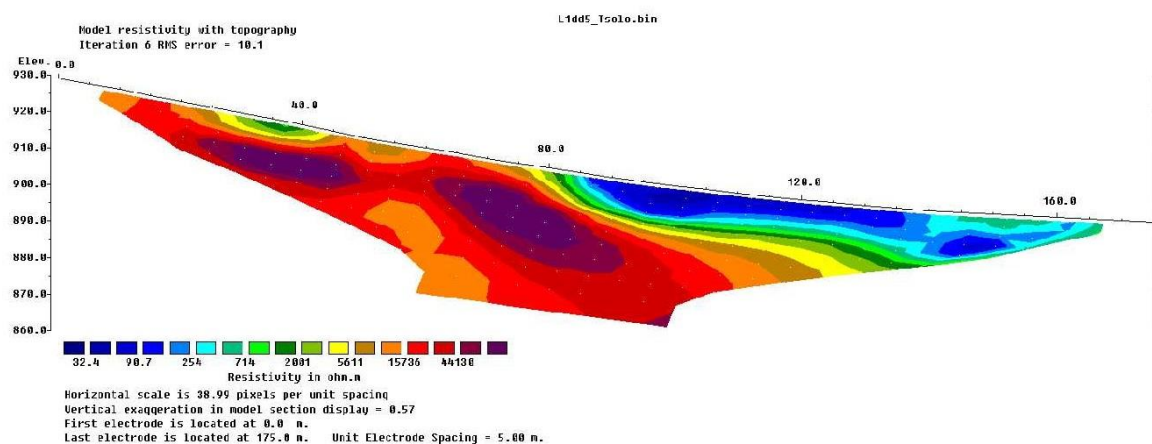


Figure 6. ERT section along line 1 (Dipole dipole array)

Results discussions-Line 1

The sections on this line shows a competent and well exposed dolerite outcrop that extent from the start of line to the river. Closer to the river the dolerite is covered by thin overburden comprising some clayey gravel and partly saturated residium. The sections concurs well with results from the logged borehole (N2) which is intersected by this line. The dorerite exhibits high resistivities and high seismic velocities in the range $\pm 2.5\text{km/h}$ or higher, which is usual for hard rocks. The loose and unconsolidated material (gravel and residium) closer to the river at line 1 will be easily excavatable,

the dolerite will present some challenges as it is a hard competent rock. Interpretations of the results acquired with both the techniques on line 1 are presented in table 2.

Table 2

Layer	Model velocity (km/s)	Model Resistivity (Ohm.m)	Depth range (m)	Soil/rock type
Layer 1	0.3-0.9	(Layer 1) 32-300	0 – 6(@120-180m)	clayey gravel and partially saturated residium
Layer 2	0.9-2.9	(Layer 2) 300-44000	0-(>)40(@0-90m)	Hard, competent dolerite

Boreholes:

NL29 is positioned at -30m from start of line 1.

NL26 is intersected at 75m on line 1.

N2 is intersected at 135m on line 1.

6.2 Line 2

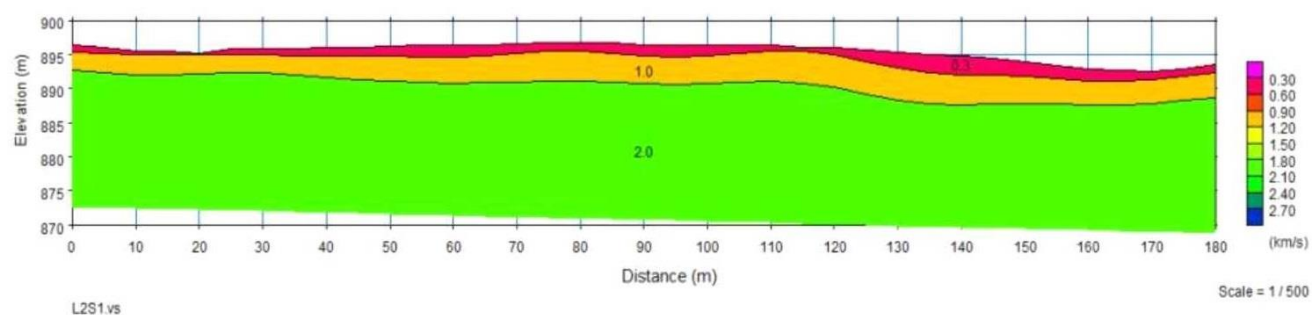


Figure 7. Modelled Seismic section along line 2.

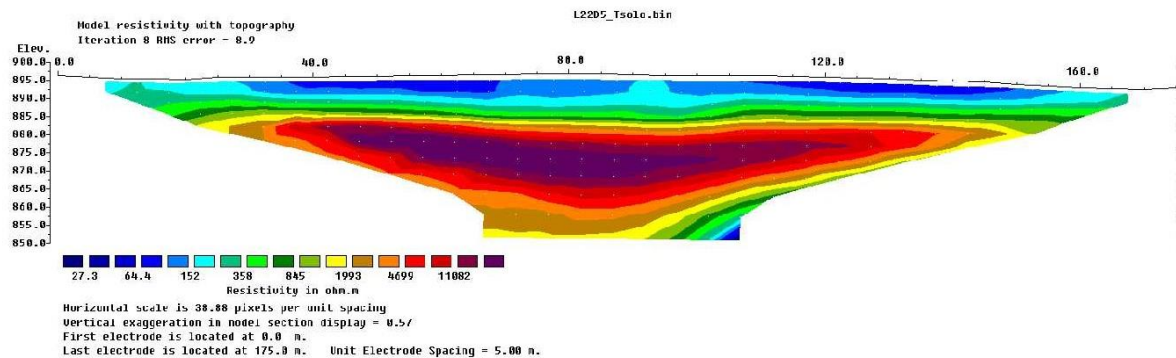


Figure 8. ERT section along line 2.

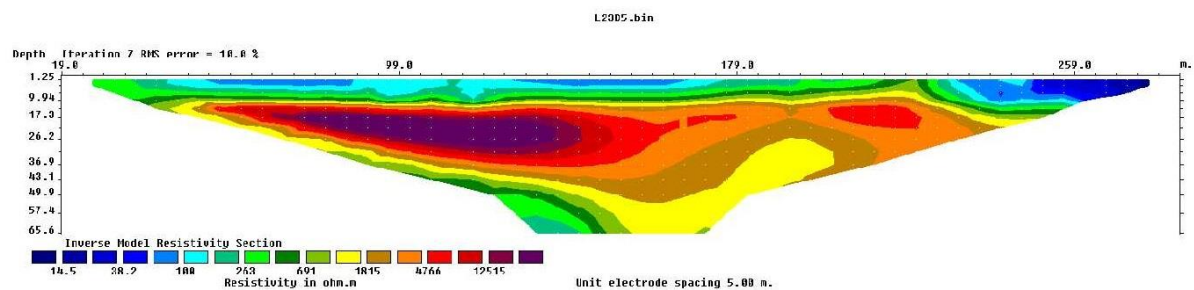


Figure 9. ERT section along line 2, with the extended portion.(270m)

Results discussions- Line 2

Along line 2, the overlying clayey gravel overburden varies in thickness depending on the close proximity of the measured position to the river. At the start of the line, the top material is thin, but along the remainder of the stretch it varies between 5-6m. The dolerite body is totally covered along this spread of the line and it stretches in depth throughout the line. Line 2 follows the direction of the river and thus the overlying material is partially saturated, exhibiting low resistivity, while the dolerite exhibits high resistivities and high seismic velocities in the range ± 2.5 km/h or higher. The overlying loose material (gravel and residium) closer to the river along line 2 will be easily excavatable, the dolerite will present some challenges as it is a hard competent rock. Figure 9 shows the extended portion of line 2, with very little changes from the original spread. Interpretations of the results acquired with both the techniques on line 2 are presented in table 3.

Line 2 intersects borehole N2 at position 87m. The borehole log concurs with the results of the seismic and ERT techniques applied across it.

Table 3

Layer	Model velocity (km/s)	Model Resistivity (Ohm.m)	Depth range (m)	Soil/rock type
Layer 1	0.1-0.6	90-300	0-6	Reddish Sandy clay, Colluvial
Layer 2	0.6-1.5	300-656	6-7	Gravells, dolerite residuals
Layer 3	1.5- 3	656-70000	7-(>)40	Dolerite, hard and competent

6.3 Line 3

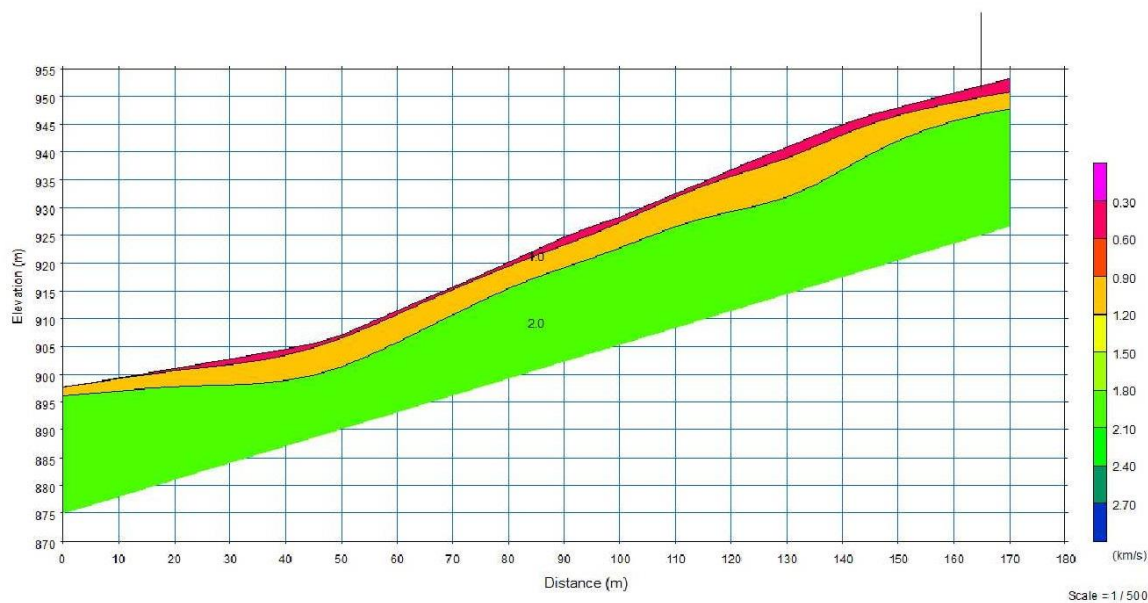


Figure 10. Modelled seismic section along line 3.

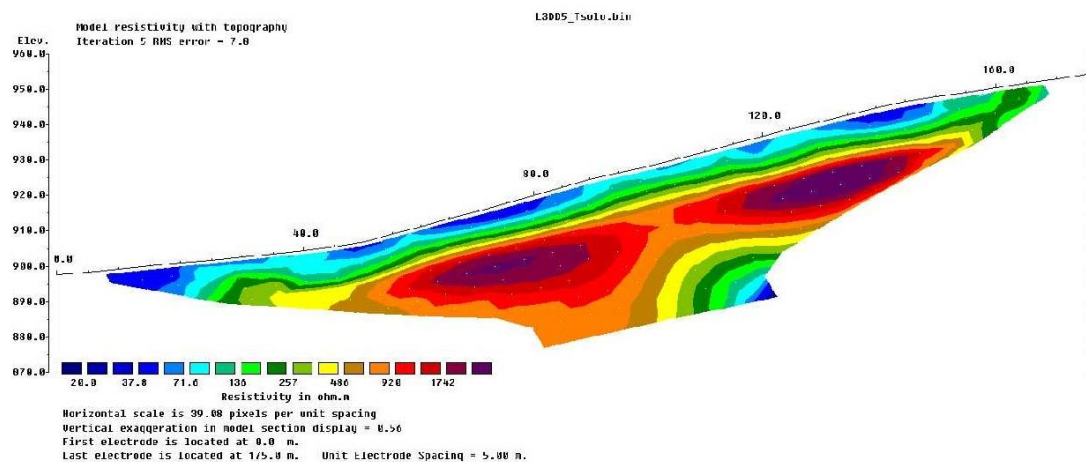


Figure 11. ERT section along line 3 (dipole-dipole)



Figure 12. An image showing the relative depth extend of the thick overlying material, some dark grey-brownish colluvium and highly metamorphosed sandtones in an exposure zone along the position of line 3.

Results Discussions-Line 3

Line 3 starts at the river and climbing on the steeply sided ridge oriented NW of the river. The ERT and seismic sections at this location depicts a fairly conductive layer of moist clayey sand or colluvium extending to depths $\pm 1.5\text{m}$ covering most parts of this line. Figure 14 indicate clearly the depth of the residual material overlying the sandstones/dolerite along line 3. The dark coloured clayey sand at the top is thin and loose, followed by some subrounded to rounded thick coubles/boulders of weathered sandstone that extend to approximately 7m. The thickness of the overburden is almost constant throughout the line, except for the area nearby the river, where the sandstone is nearly exposed. The competent and resistive sandstone bedrock is found below 7m along whole length of the line, extending deep. Interpretations of the results acquired with both the techniques on line 3 are presented in table 4.

Table 4

Layer	Model velocity (km/s)	Model Resistivity (Ohm.m)	Depth range (m)	Soil/rock type
Layer 1	0.1-0.9	20-37.8	0-1.5	Clay,sand
Layer 2	0.9-1.5	37.8-71.6	1.5-7	Weathered sandstone
Layer 3	2-3	71.8-3000	7-(>)40	Hard, competent sandstone

Line 3 intersects borehole N3 at around 135m.

6.4 Line 4

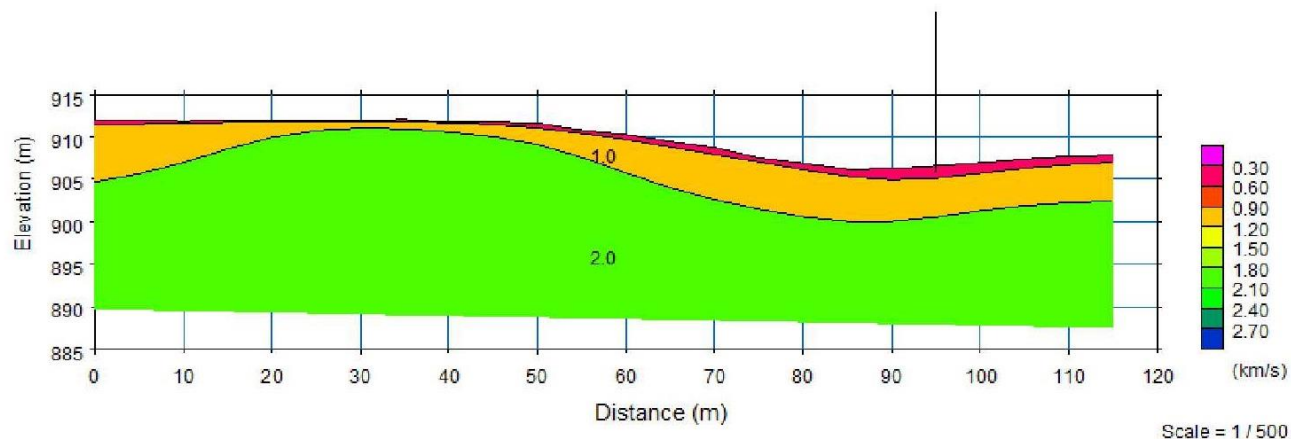


Figure 13. Modelled seismic section along line 4.

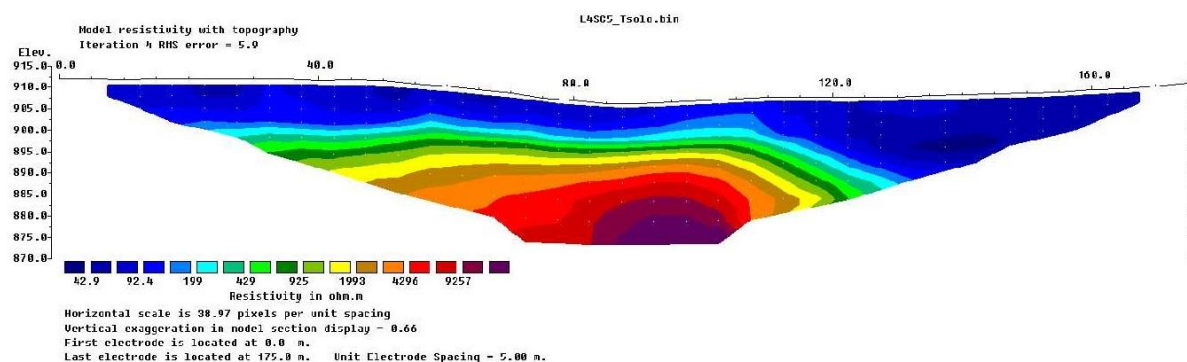


Figure 14. An ERT section along line 4.

Results discussions- Line 4

Line 4 lies parallel to line 2, but on other side of the river(west) trending SW-N. The results along this line shows a relatively thick overburden cover at the start of the line, thinning in the middle and becoming increasingly thick again towards the end of the spread. The sections shows presence of a lowly resistive layer covering the total length of the spread of probably clayey sand and loose residium. These layers are followed by a relatively hard and competent bedrock with high seismic velocities, ranging around 1.5km/s to ± 2.7 km/s. The highly resistive layer with corresponding high seismic velocity layer is interpreted to be either a fresh sandstone or an extension of the dolerite to



the west, which also extends deep. Interpretations of results acquired with both the techniques on line 4 are presented in table 5.

Table 5

Layer	Model velocity (km/s)	Model Resistivity (Ohm.m)	Depth range (m)	Soil/rock type
Layer 1	0.3-0.9	25-50	0-0.5	Reddish brown clay, Colluvium
Layer 2	0.9-1.5	50-400	0.5-6	Dolerite/sandstone residium
Layer 3	1.5-2.7	400-9000	6-(>)40	Dolerite/Sandstone

Line 4 intersects borehole N1 at 110m.

7 CONCLUSIONS AND RECOMMENDATIONS

Seismic refraction data and Electrical Resistivity tomography (ERT) surveys of a high signal to noise ratio were collected along the four(4) lines. The results of the seismic data interpretation shows a strong and precise correlation between the thickness of the low velocity layer and the depth of weathering as observed in the existing boreholes at all the surveyed lines. The obtained low velocities and low resistivity results ranging between about 0.3km/s and 0.9km/s and low resistivity values may be interpreted as indicating presence of loose and unconsolidated material overlying the bedrock at these locations. The highly resistive areas with corresponding high seismic velocities above 1.0km/s or higher, indicate hard competent rock, of either dolerite or fresh sandstone material. The Seismics and ERT results collected at this area correlate very well with the borehole data and thus can be used for correctly determining engineering properties for dam design purposes at this location.



8 REFERENCES

Fourie, S.J and Odgers, T.J., Spreadsheet Interpretation of Seismic Refraction Data, Computers and Geosciences, Vol 21, No. 2, pp.273-277, 1995. Elsevier Science Ltd.

Loke, M.H., Electrical imaging surveys for environmental and engineering studies. A practical guide to 2-D and 3-D surveys, 1999.

Johnson M.R., Visser J.N.J., Wickens H.de V., Christie A.D.M., Roberts D.L and Brandl G. Sedimentary rocks of the Karoo Supergroup in: Johnson, M.R., Anhaeusser, C.R. and Thomas, R.J. (Eds.) The Geology of South Africa, Geological Society of South Africa, Johannesburg / Council for Geoscience, Pretoria, 2006.

Sheriff Y., 1976. Reference seismic velocity range plot for rocks, in O.Yilmaz, Seismic Data Analysis: Processing, Inversion and Interpretation of seismic data. Volume 1, 2008.

Iris Instruments : <http://www.iris-instruments.com/>

Seistronix website : http://www.seistronix.com/ras_g.htm

APPENDIX G

TRIAL PIT PROFILE DESCRIPTIONS

G1:

DAM TRIAL PITS

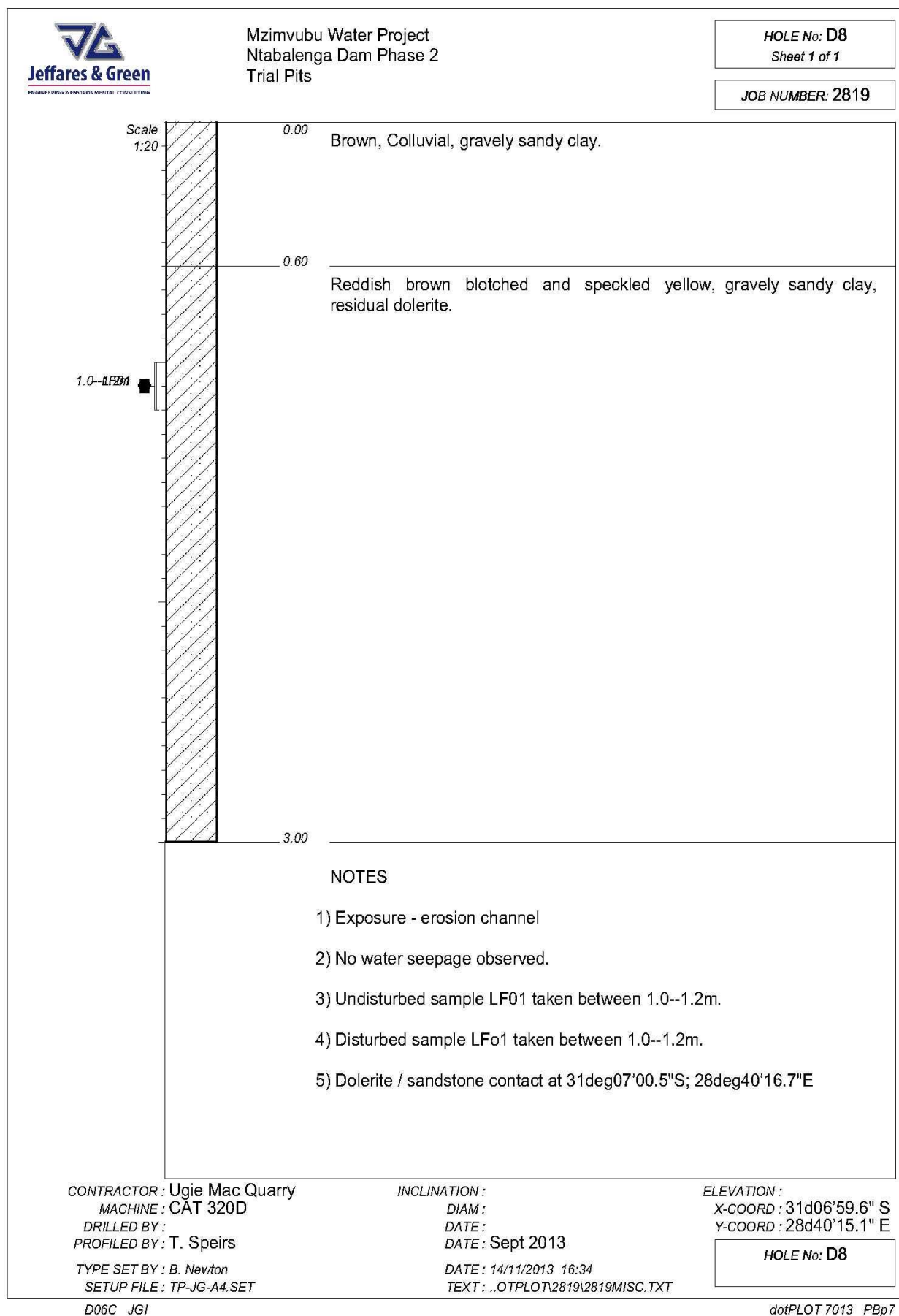


Fig G-1: Dam Trial Pits Hole No: D8

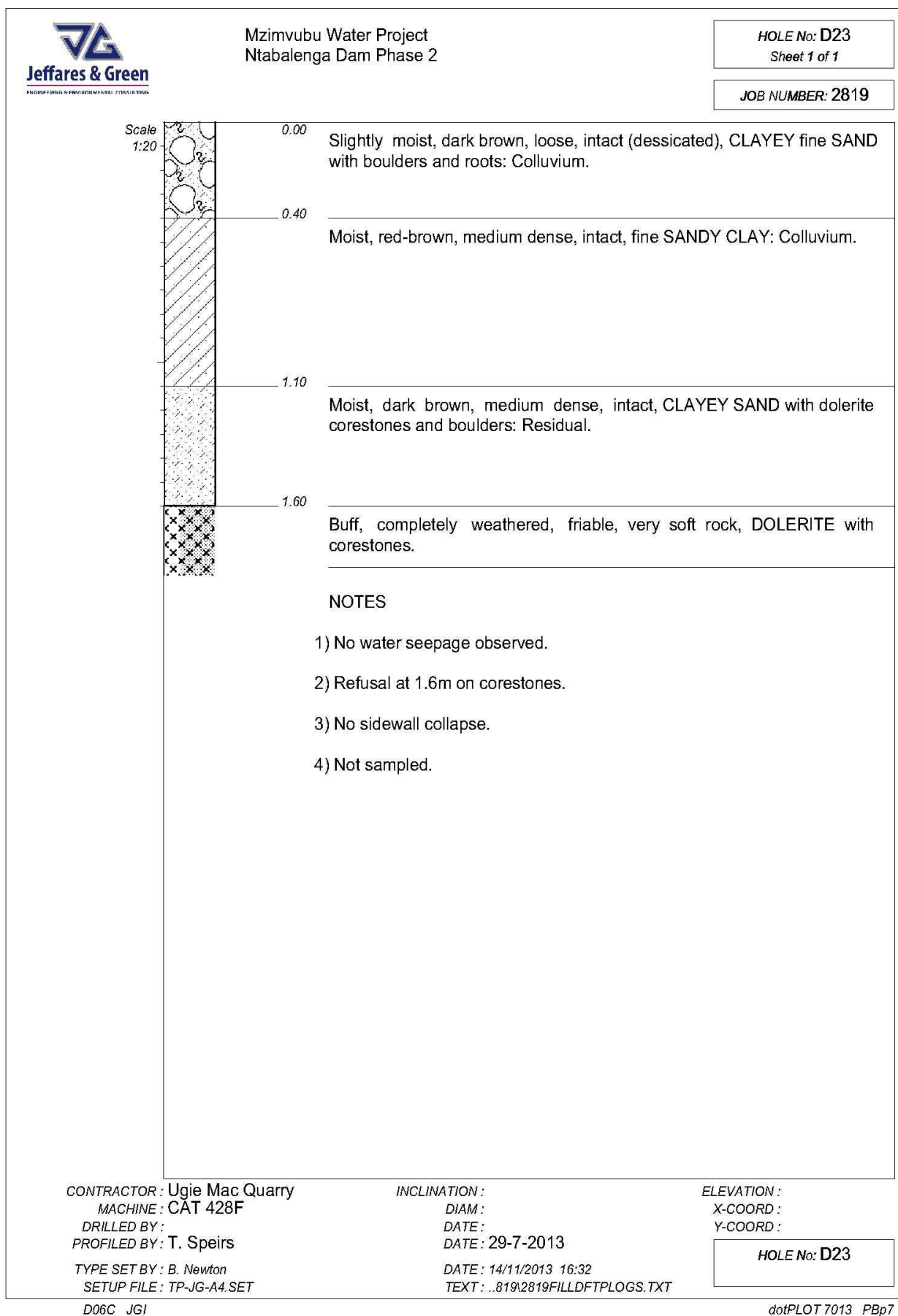


Fig G-2: Dam Trial Pits Hole No: D23

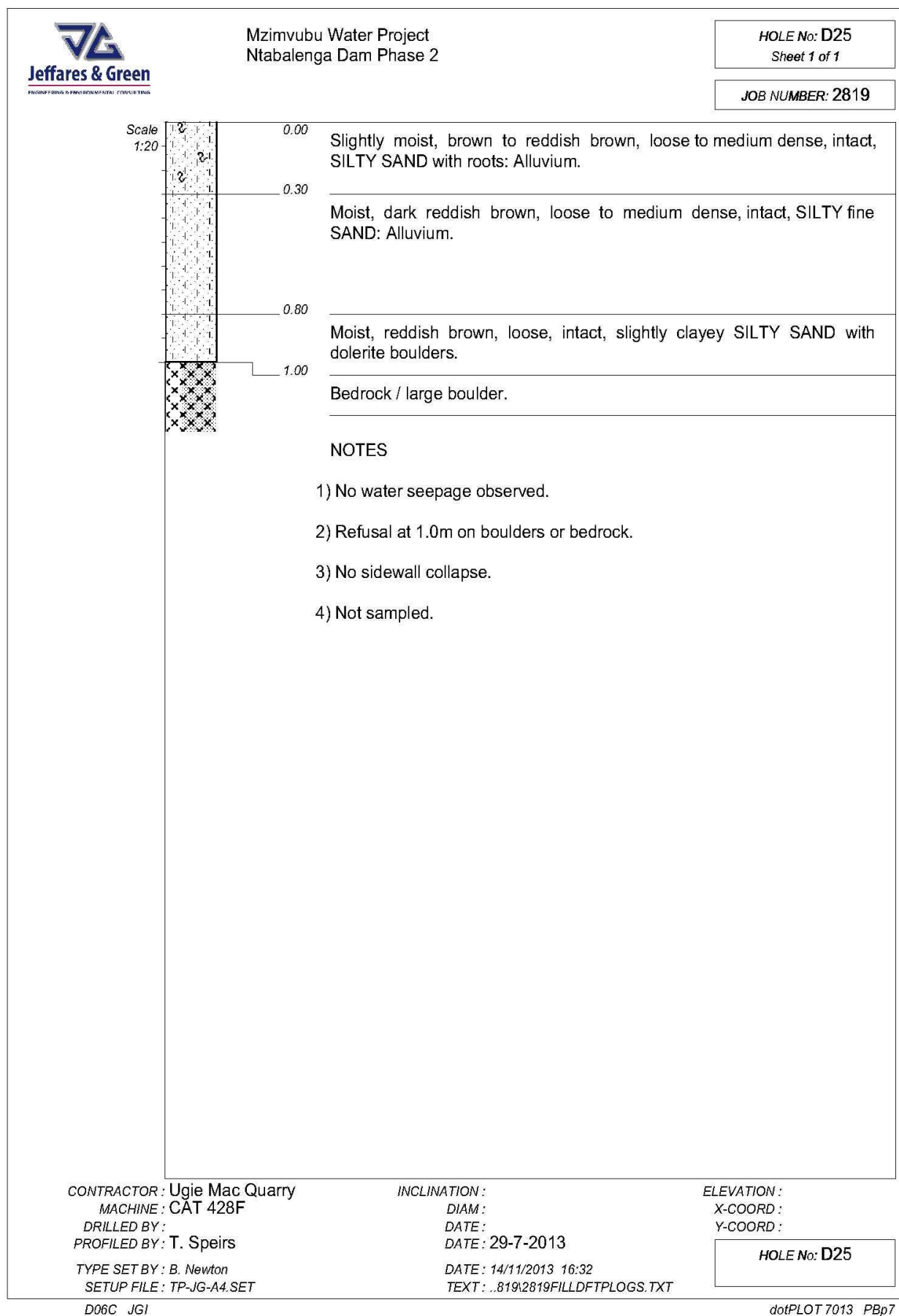


Fig G-3: Dam Trial Pits Hole No: D25

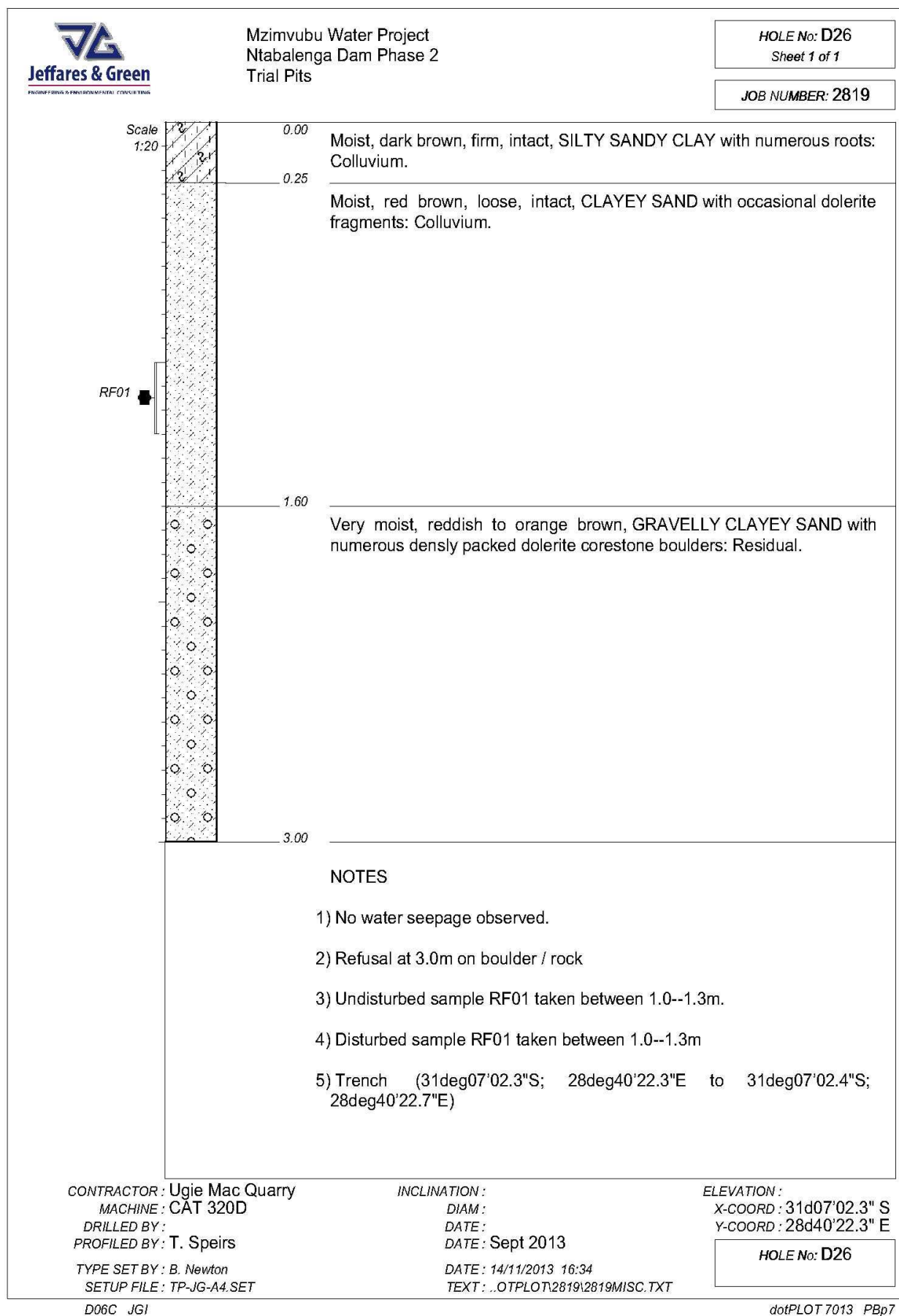


Fig G-4: Dam Trial Pits Hole No: D26

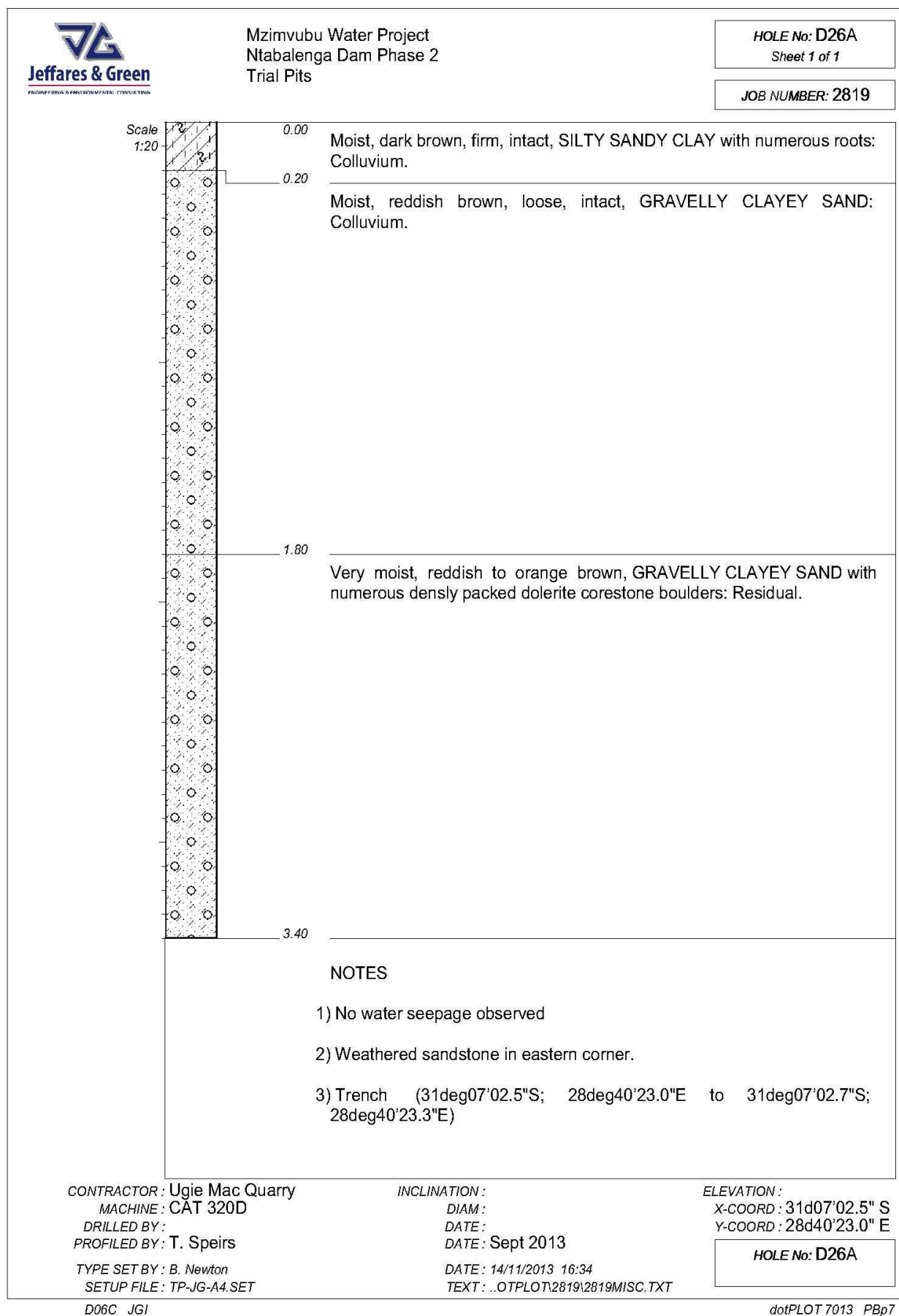


Fig G-5: Dam Trial Pits Hole No: D26A

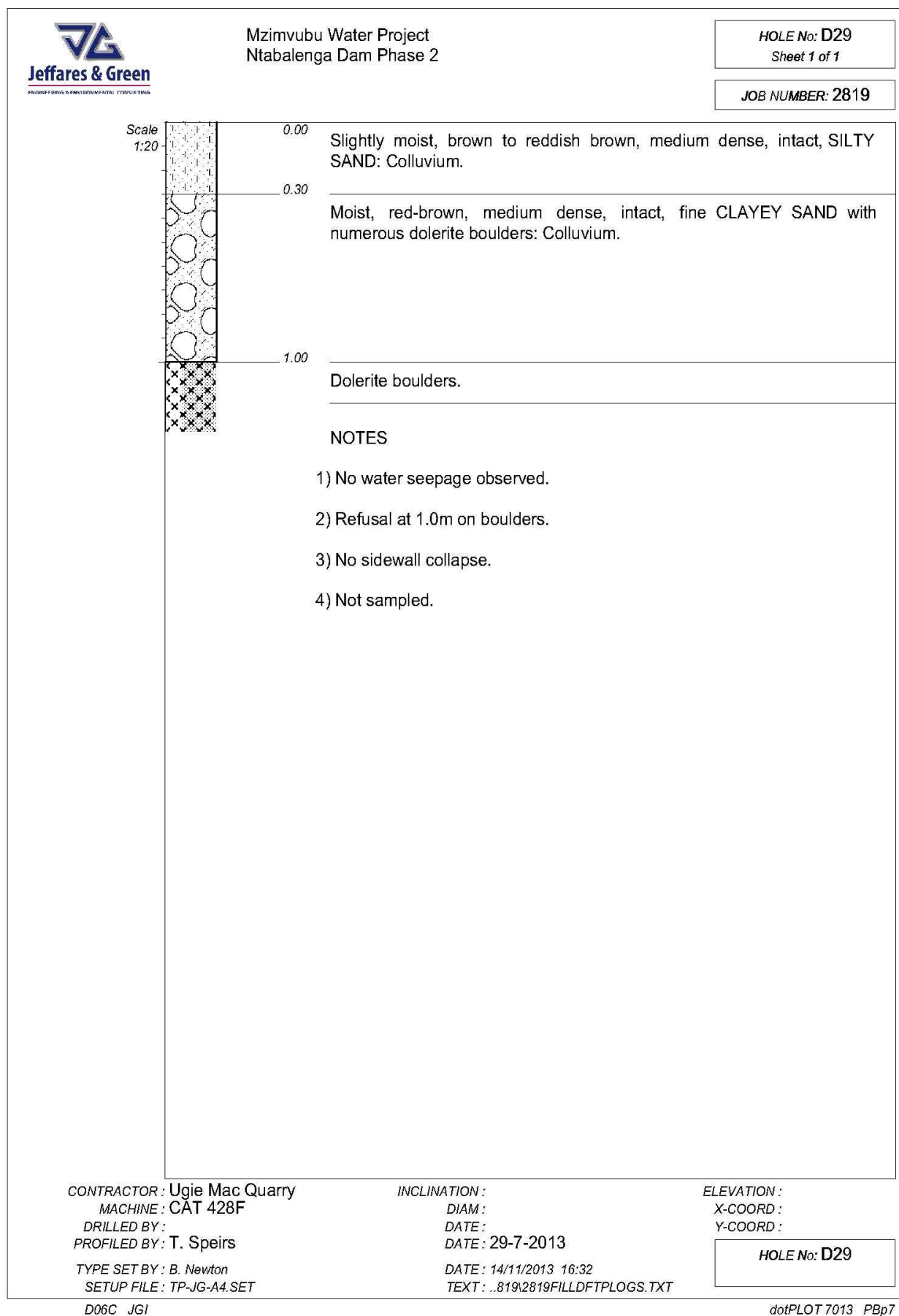


Fig G-6: Dam Trial Pits Hole No: D29

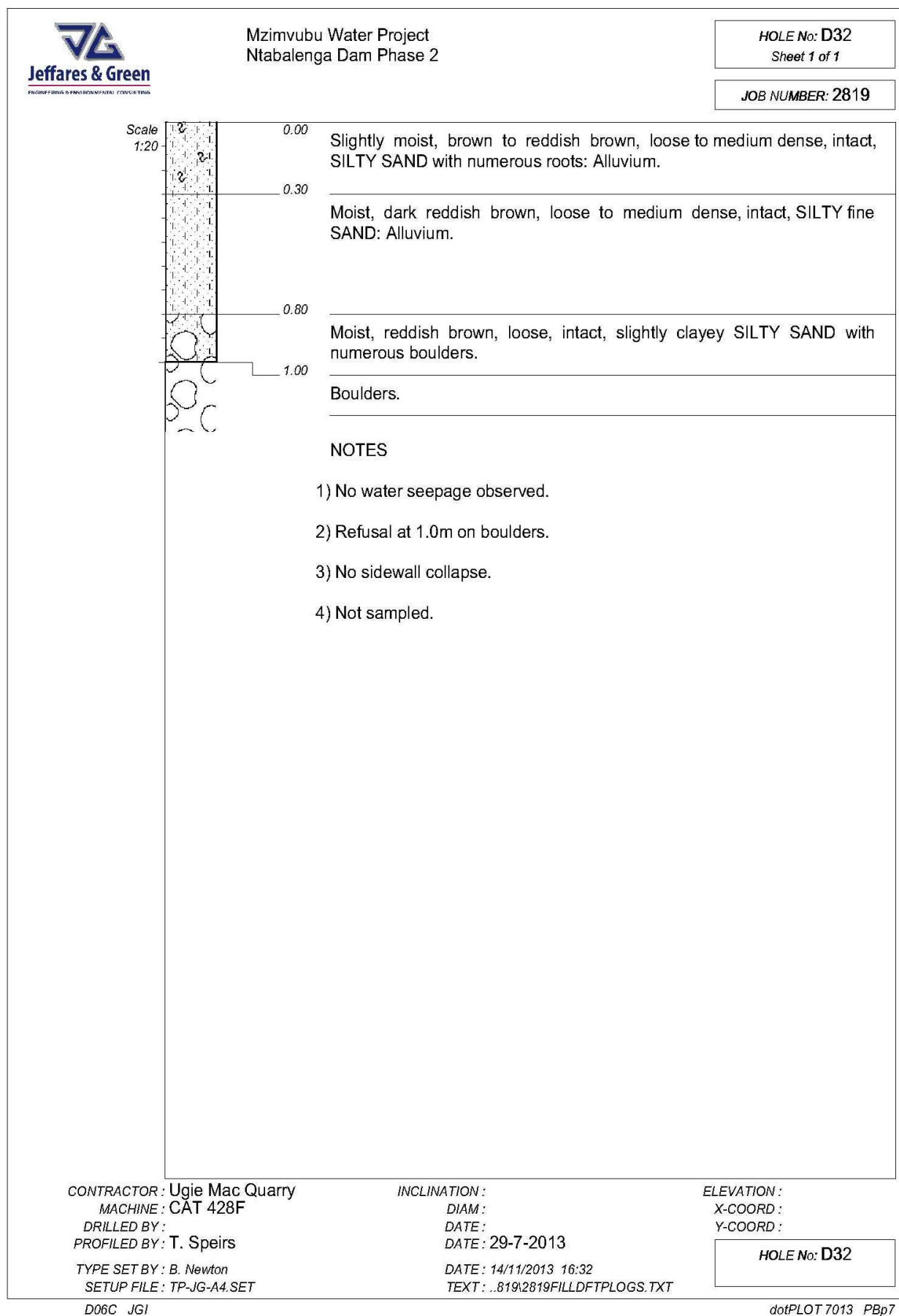


Fig G-7: Dam Trial Pits Hole No: D32

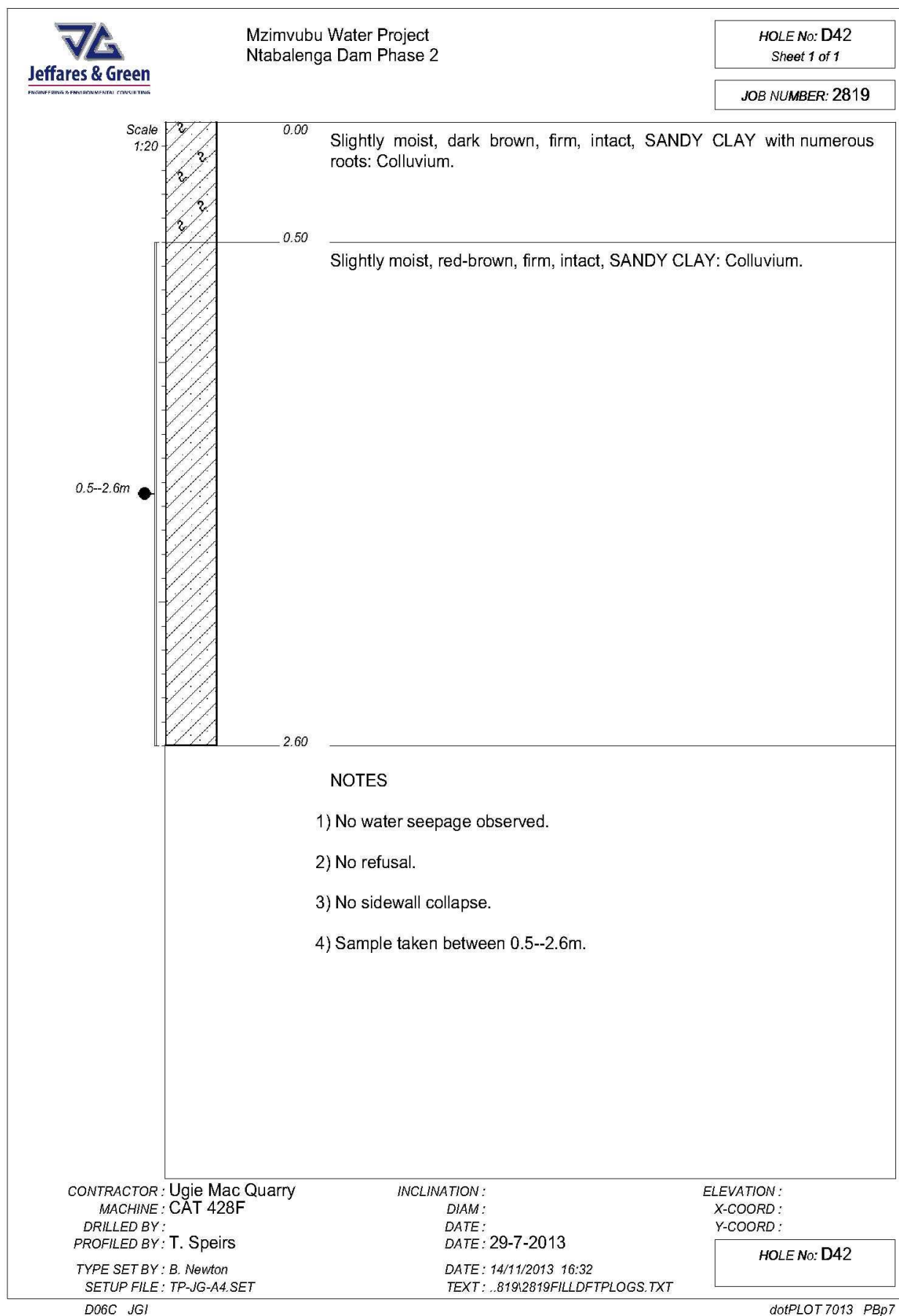


Fig G-8: Dam Trial Pits Hole No: D42

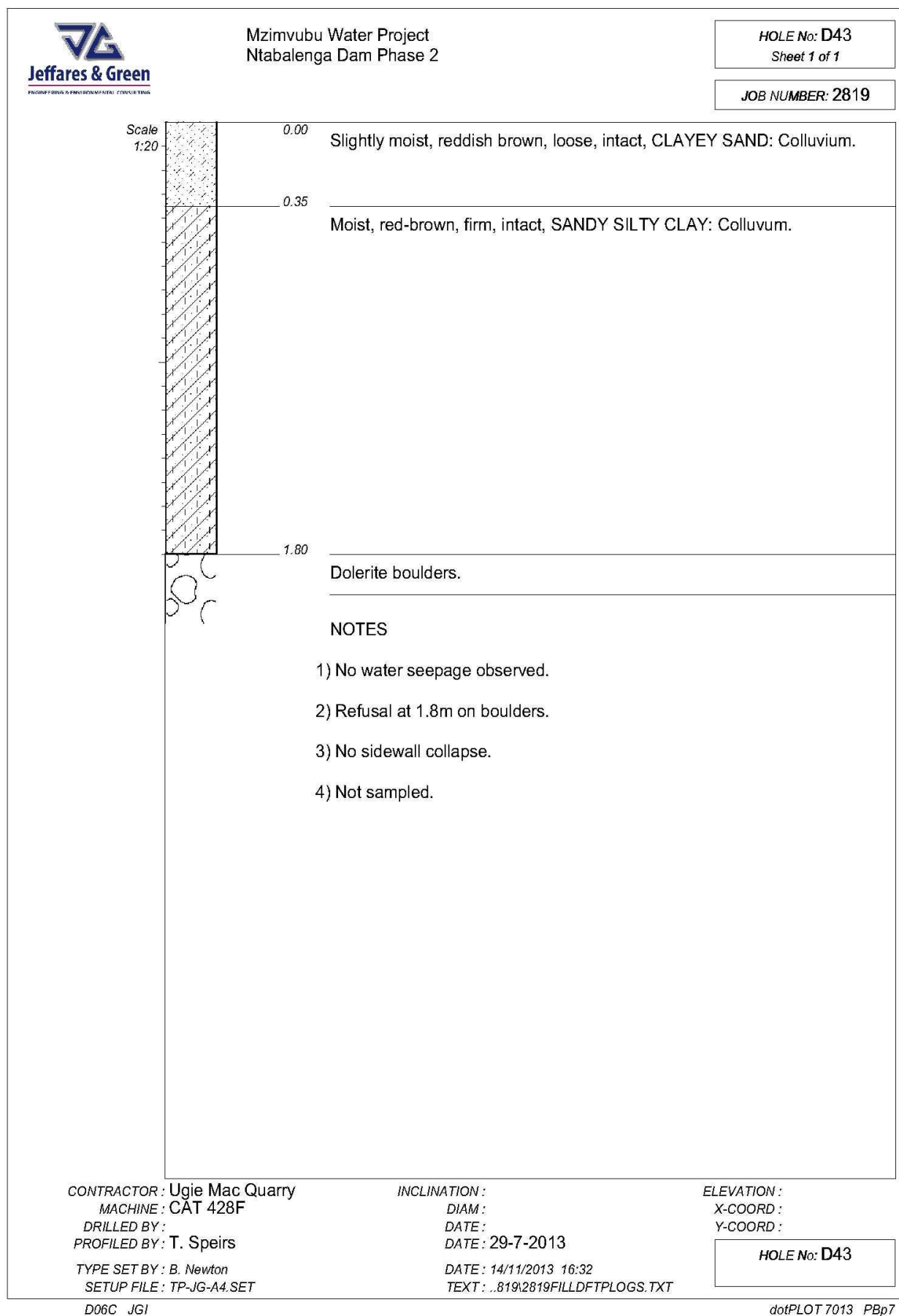


Fig G-9: Dam Trial Pits Hole No: D43

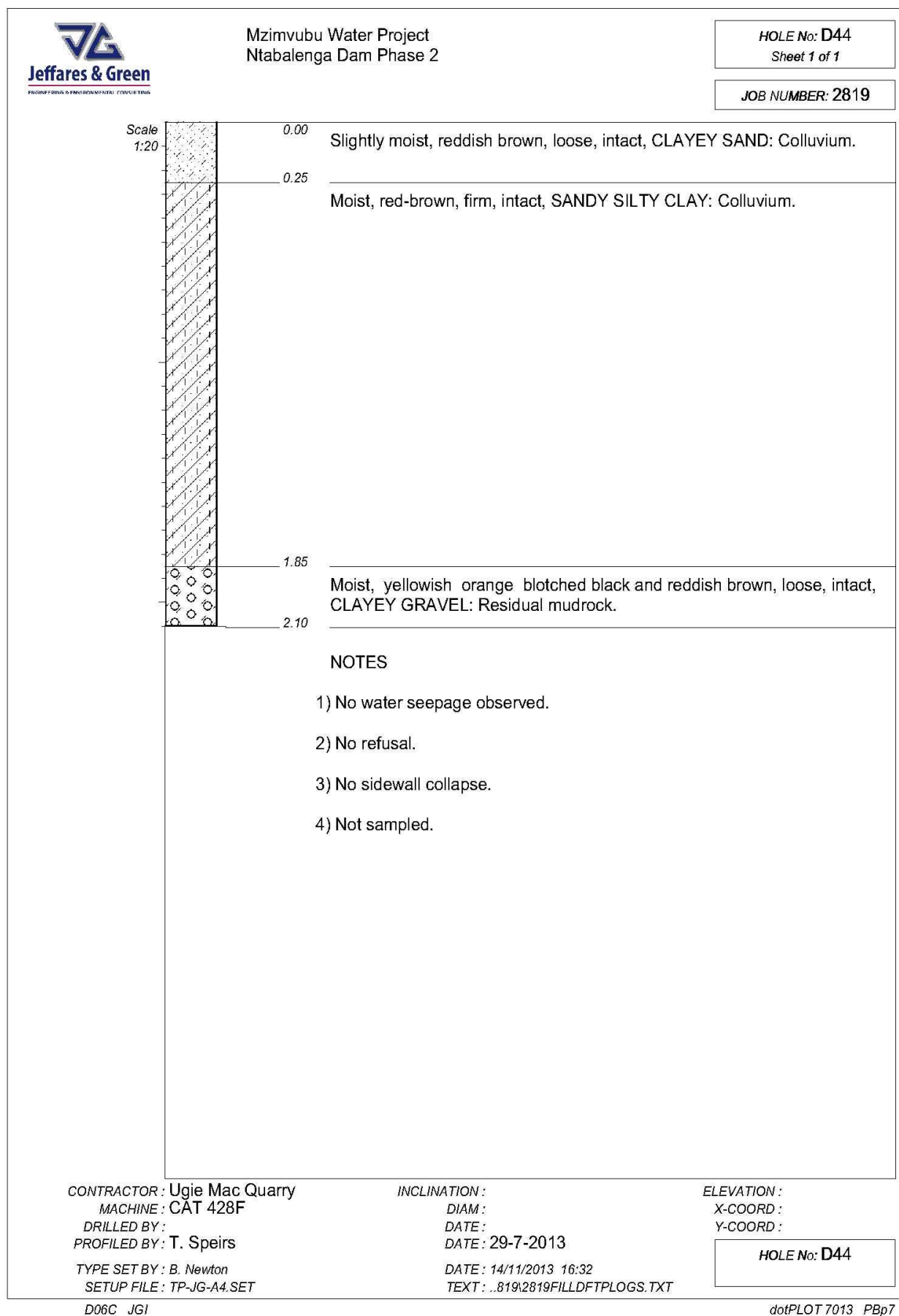


Fig G-10: Dam Trial Pits Hole No: D44

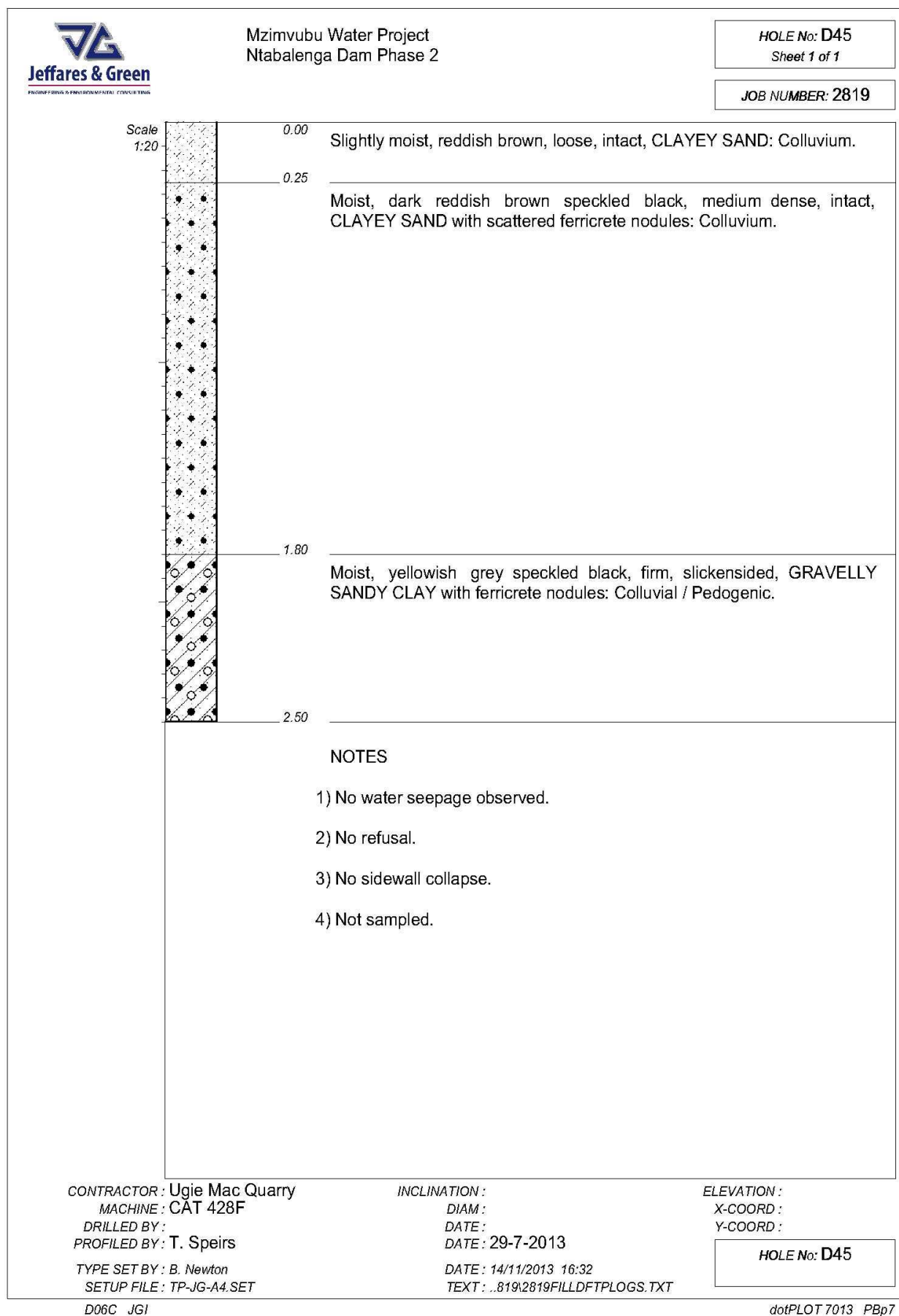


Fig G-11: Dam Trial Pits Hole No: D45

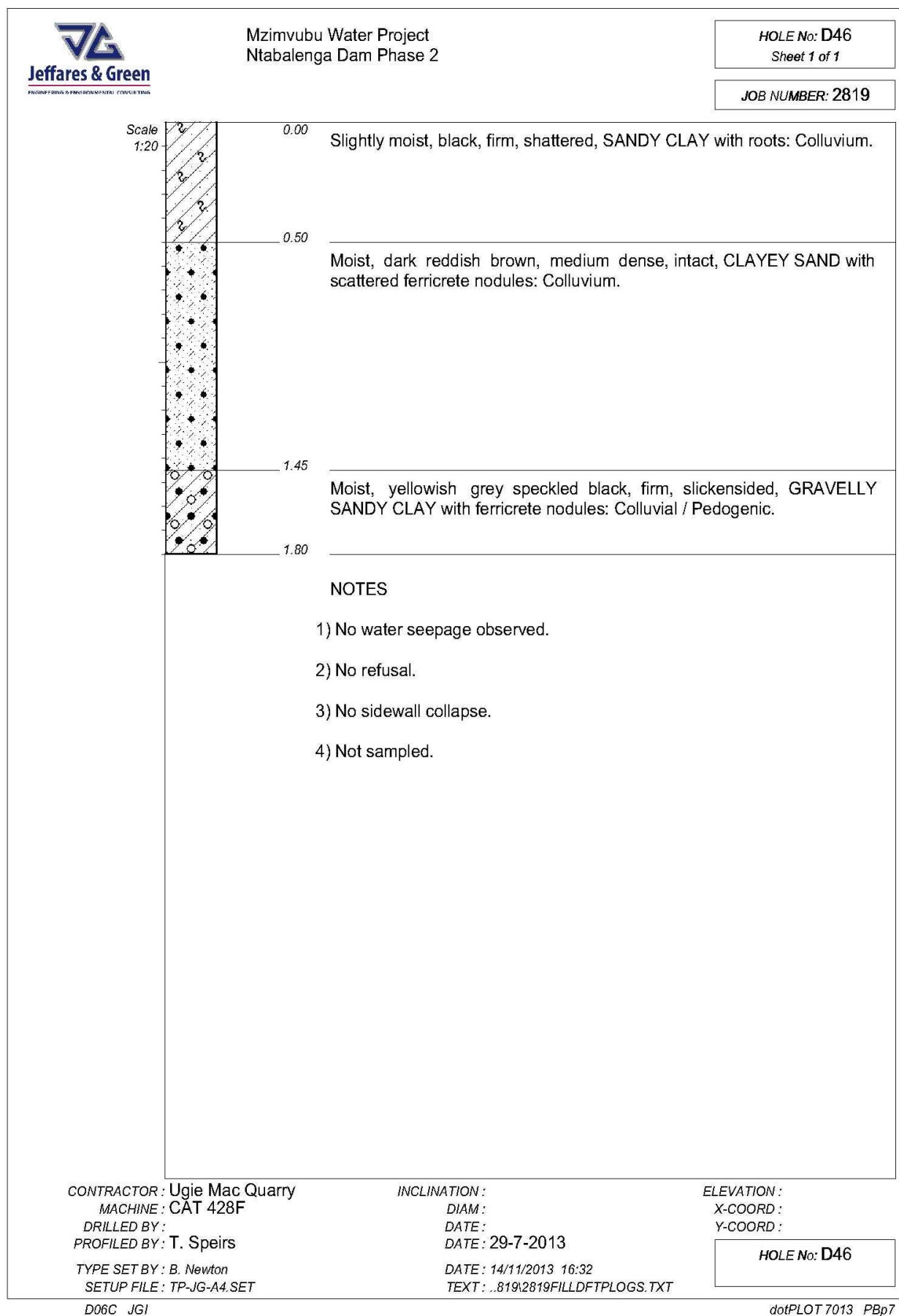


Fig G-12: Dam Trial Pits Hole No: D46

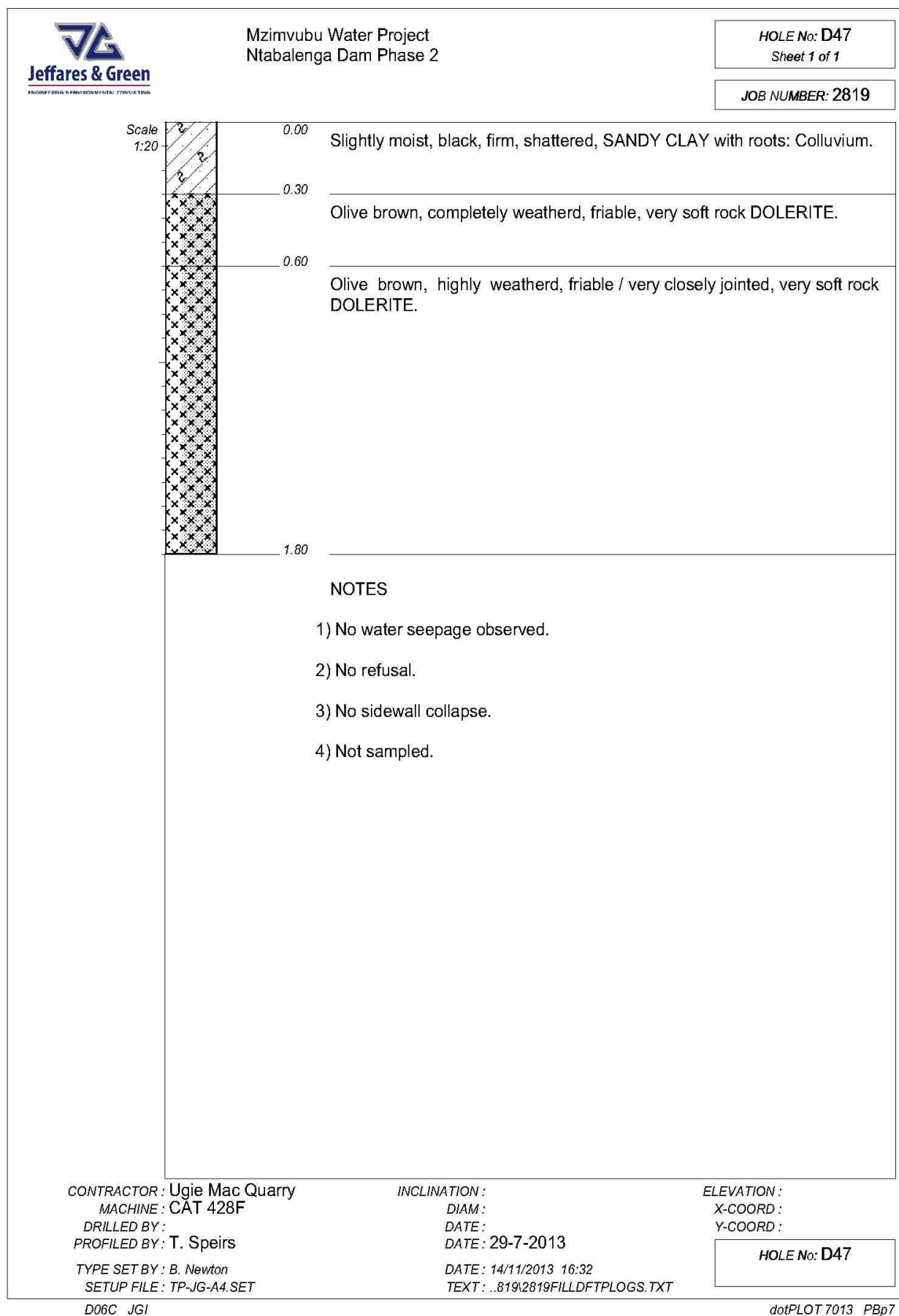


Fig G-13: Dam Trial Pits Hole No: D47

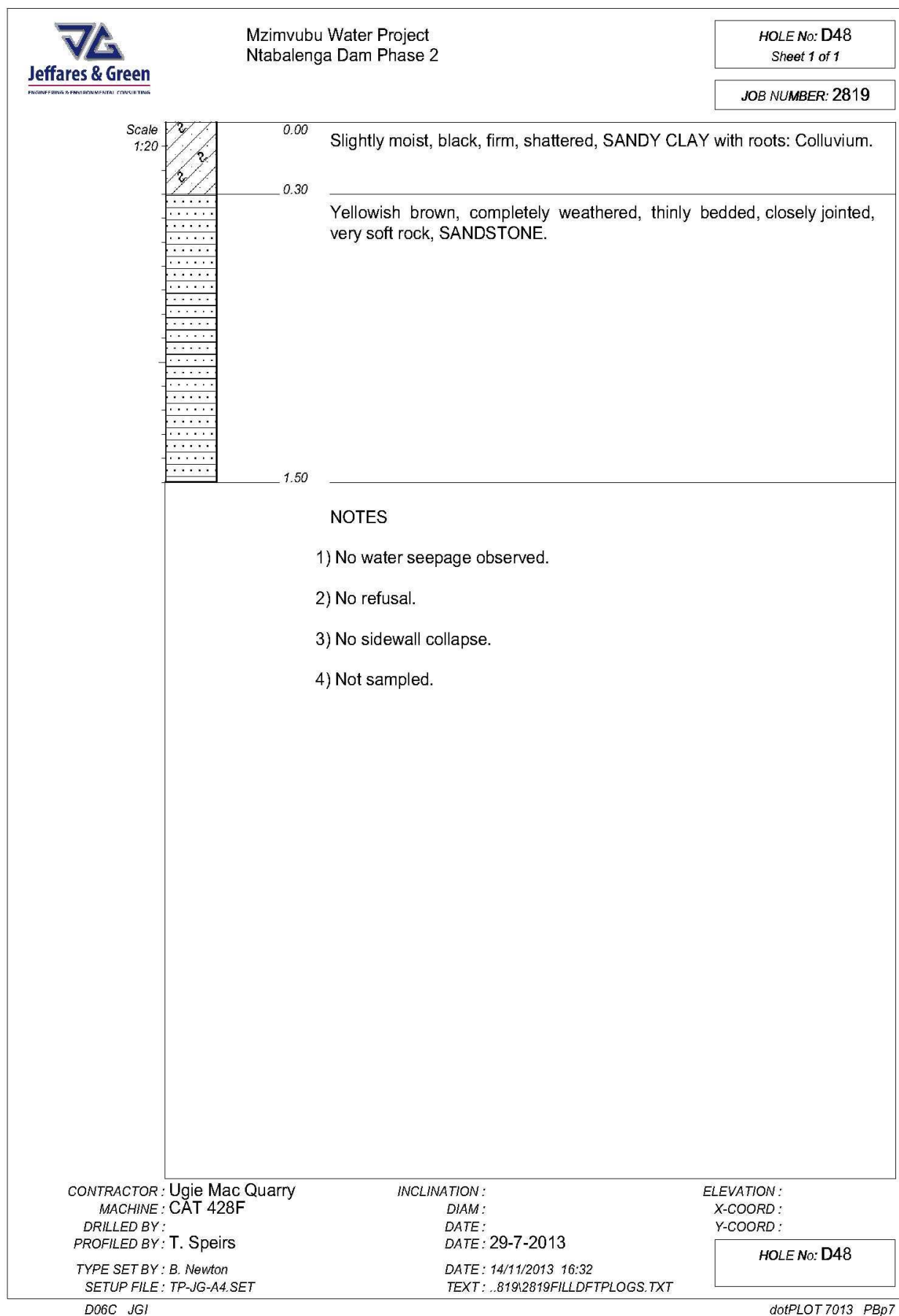


Fig G-14: Dam Trial Pits Hole No: D48

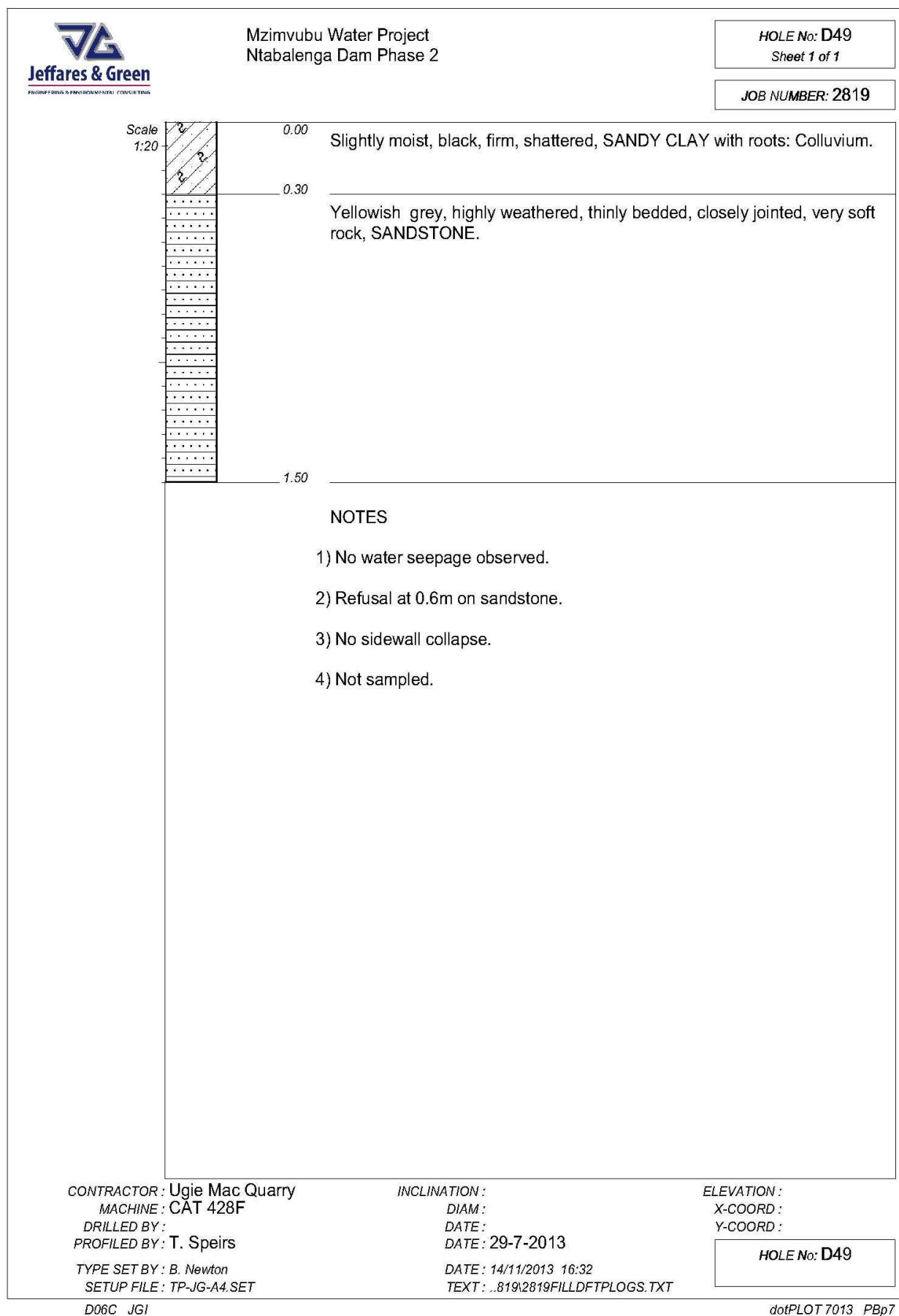


Fig G-15: Dam Trial Pits Hole No: D49

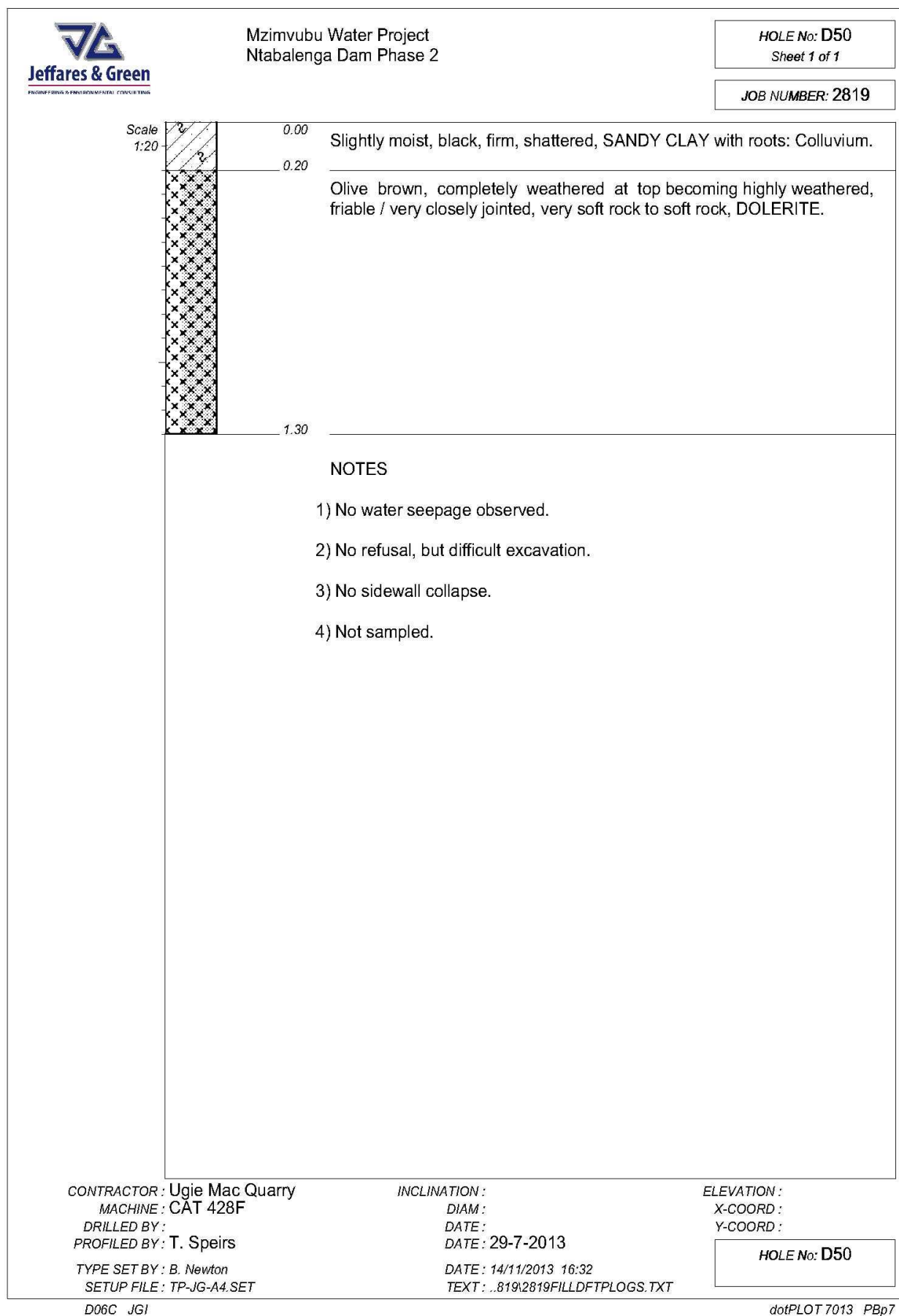


Fig G-16: Dam Trial Pits Hole No: D50

G2:

SPILLWAY TRIAL PITS

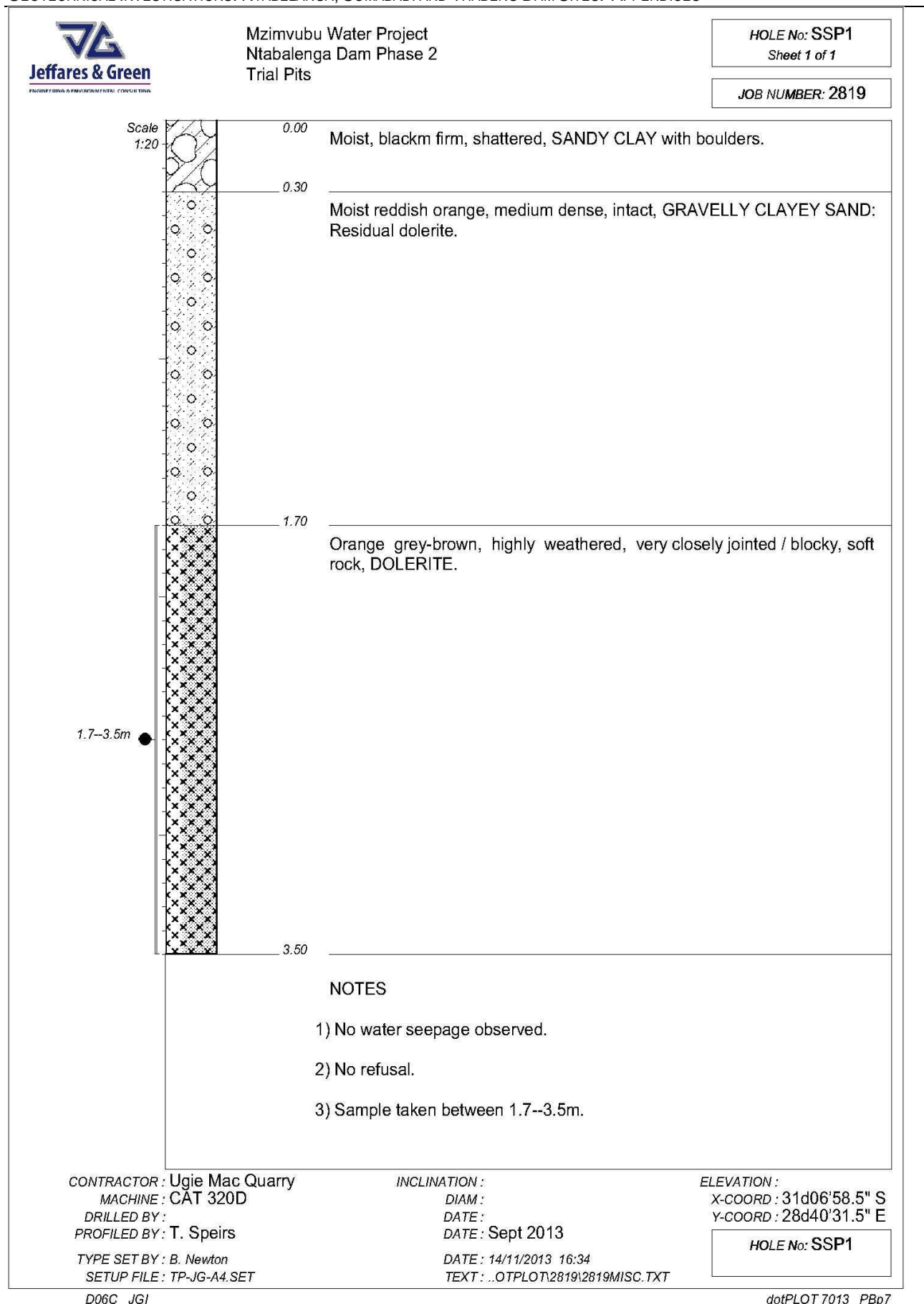


Fig G-17: Spillway Trial Pits Hole No: SP1

HOLE No: SSP2
Sheet 1 of 1

Scale 1:20

The figure is a vertical geological log. On the left, a vertical scale is marked with depth values: 0.00, 0.15, 2.20, 3.20, and 3.90. The log is divided into sections by horizontal lines. The top section (0.00 to 0.15) is filled with a pattern of small circles and dots. The middle section (0.15 to 2.20) is filled with a pattern of small horizontal dashes. The bottom section (2.20 to 3.90) is filled with a pattern of small crosses. To the right of the log, text descriptions are provided for each section.

0.00 Slightly moist, dark brown speckled yellow, firm, shattered, SANDY GRAVELLY CLAY with mudrock fragments and dolerite boulders.

0.15 Khaki, highly weathered, thinly bedded, closely jointed, very soft rock, MUDROCK.

2.20 Olive grey blotched orange speckled black, completely weathered, friable, very soft rock, DOLERITE.

3.20 Grey, highly weathered, very closely jointed / blocky, soft rock DOLERITE.

3.90

NOTES

1) No water seepage observed.

2) No refusal.

HOLE No: SSP2

dotPLOT7013 PBp7

OCTOBER 2014

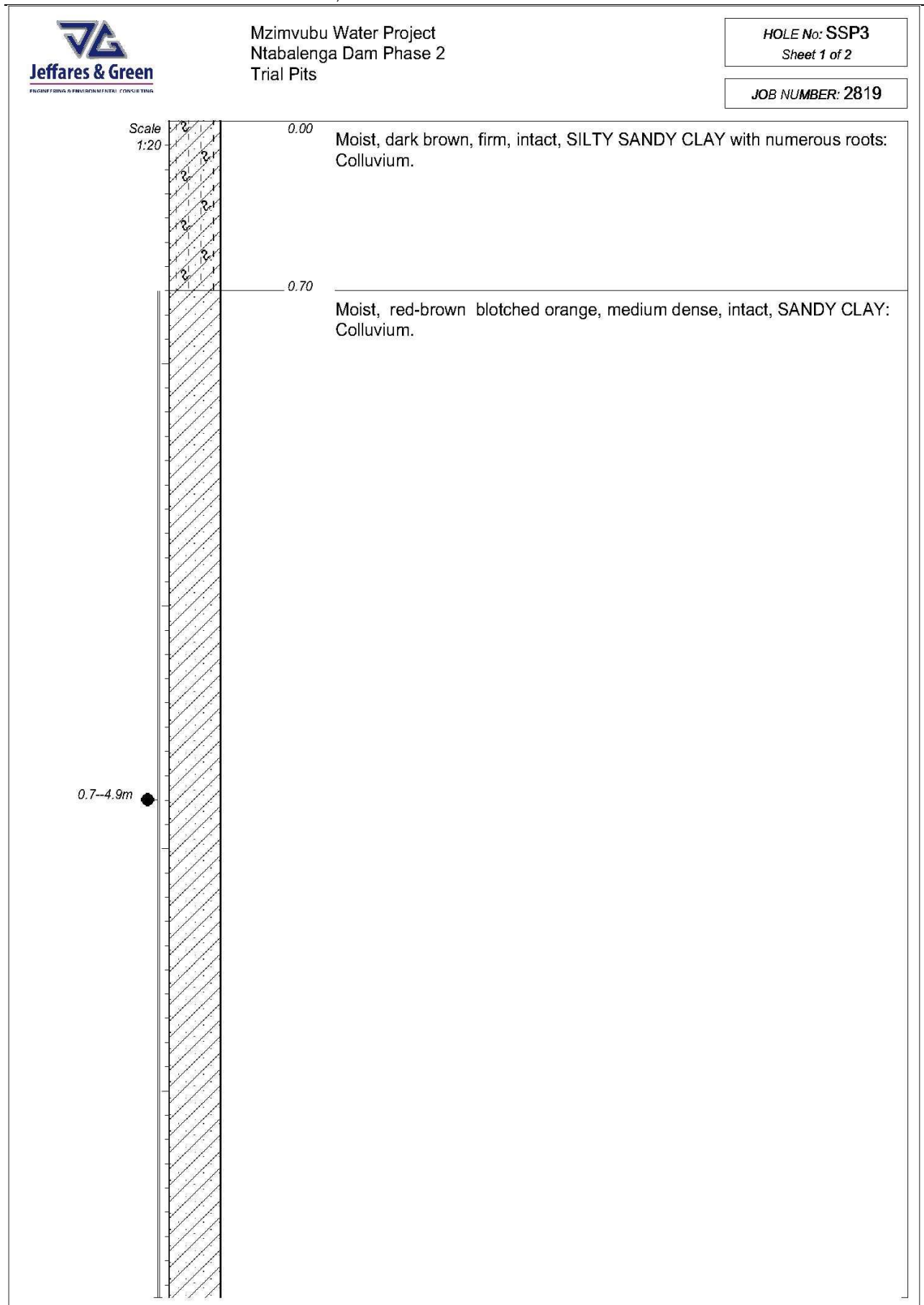


Fig G-19-1: Spillway Trial Pits Hole No: SP3

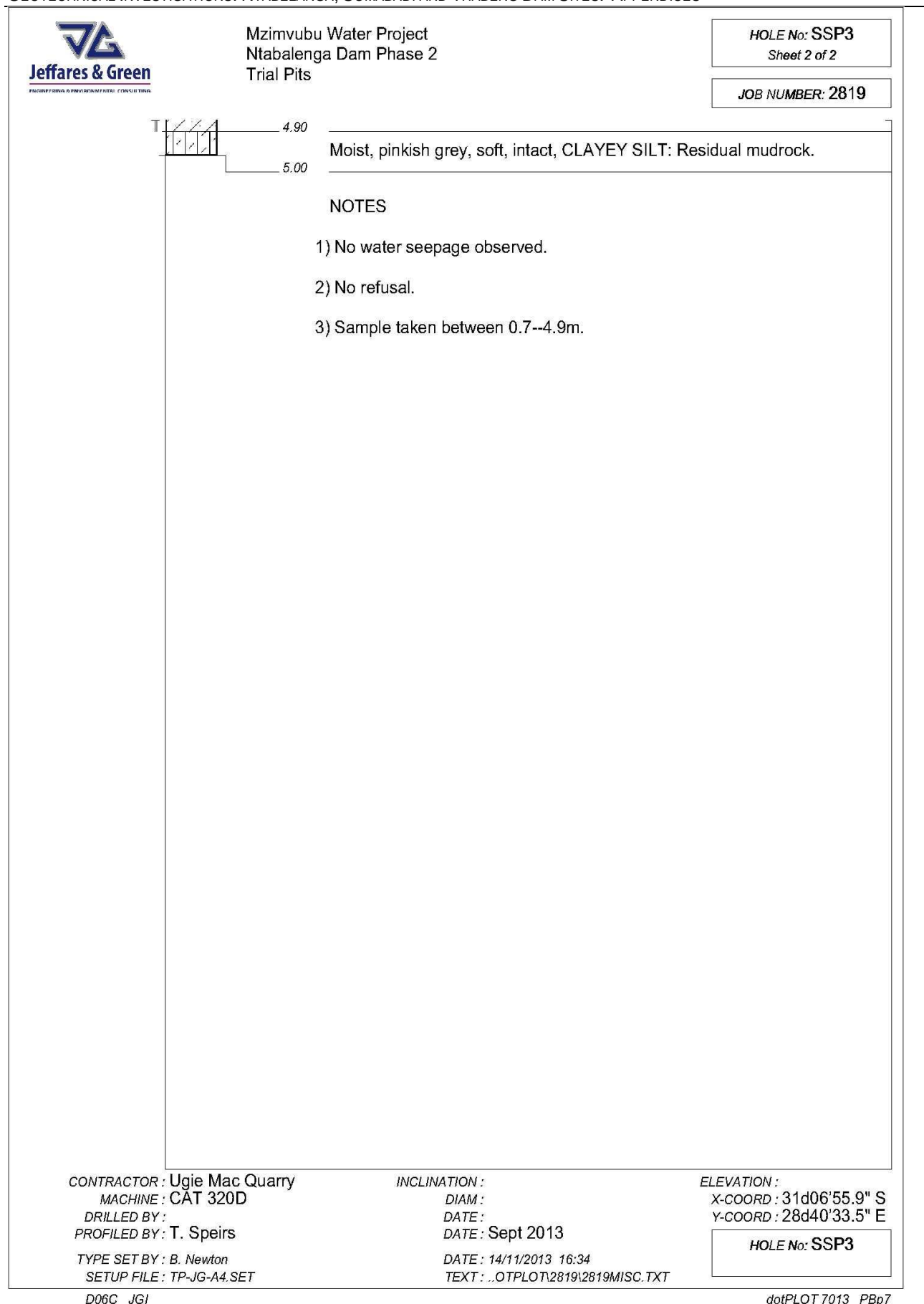


Fig G-19-2: Spillway Trial Pits Hole No: SP3

HOLE No: SP4
Sheet 1 of 1

Scale 1:20

0.00 Slightly moist, black, firm, shattered, GRAVELLY SANDY CLAY: Colluvium.

0.40

1.20

1.70

Light olive / brownish grey, medium to slightly weathered, thinly bedded, medium jointed, medium hard rock, SANDSTONE. Excavation facilitated by break out along open joints and bedding planes.

Yellowish grey-brown, highly to medium weathered, thinly bedded, closely jointed, soft rock, MUDROCK.

- 1) No water seepage observed.
- 2) No refusal.

HOLE No: **SP4**

dotPLOT7013 PBp7

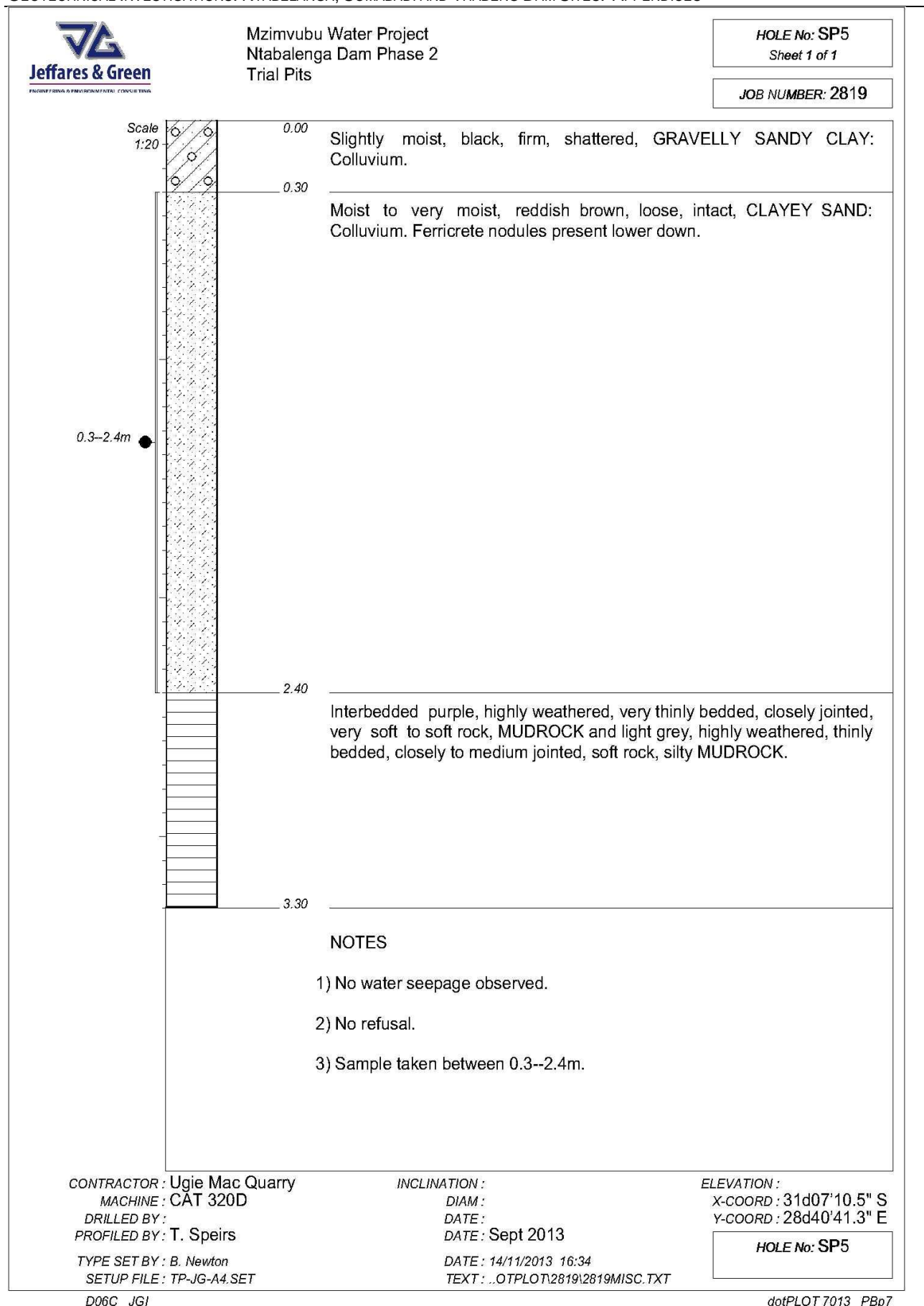


Fig G- 21: Spillway Trial Pits Hole No: SP5

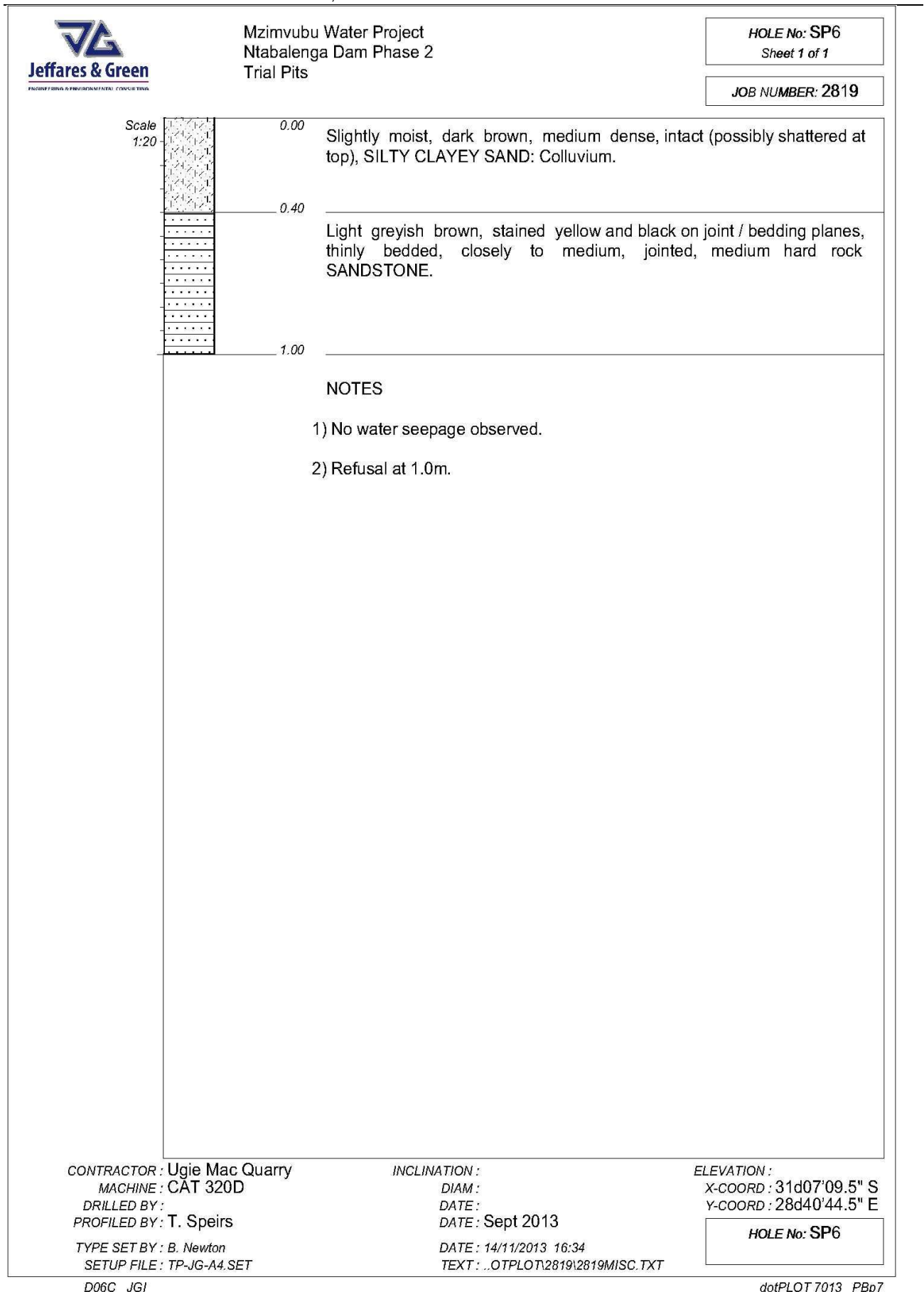


Fig G- 22: Spillway Trial Pits Hole No: SP6

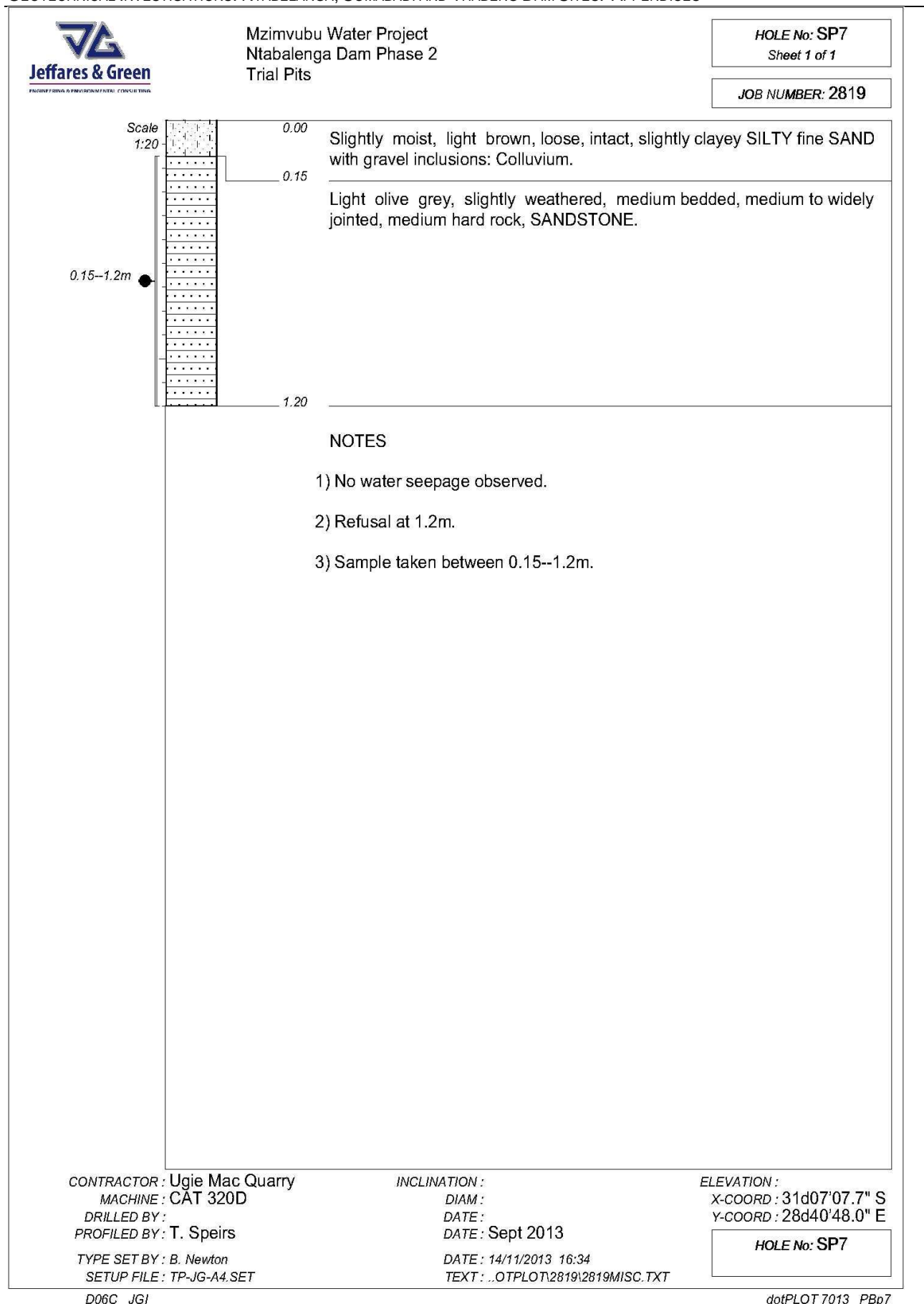


Fig G- 23: Spillway Trial Pits Hole No: SP7

G3:

SADDLE DAM TRIAL PITS

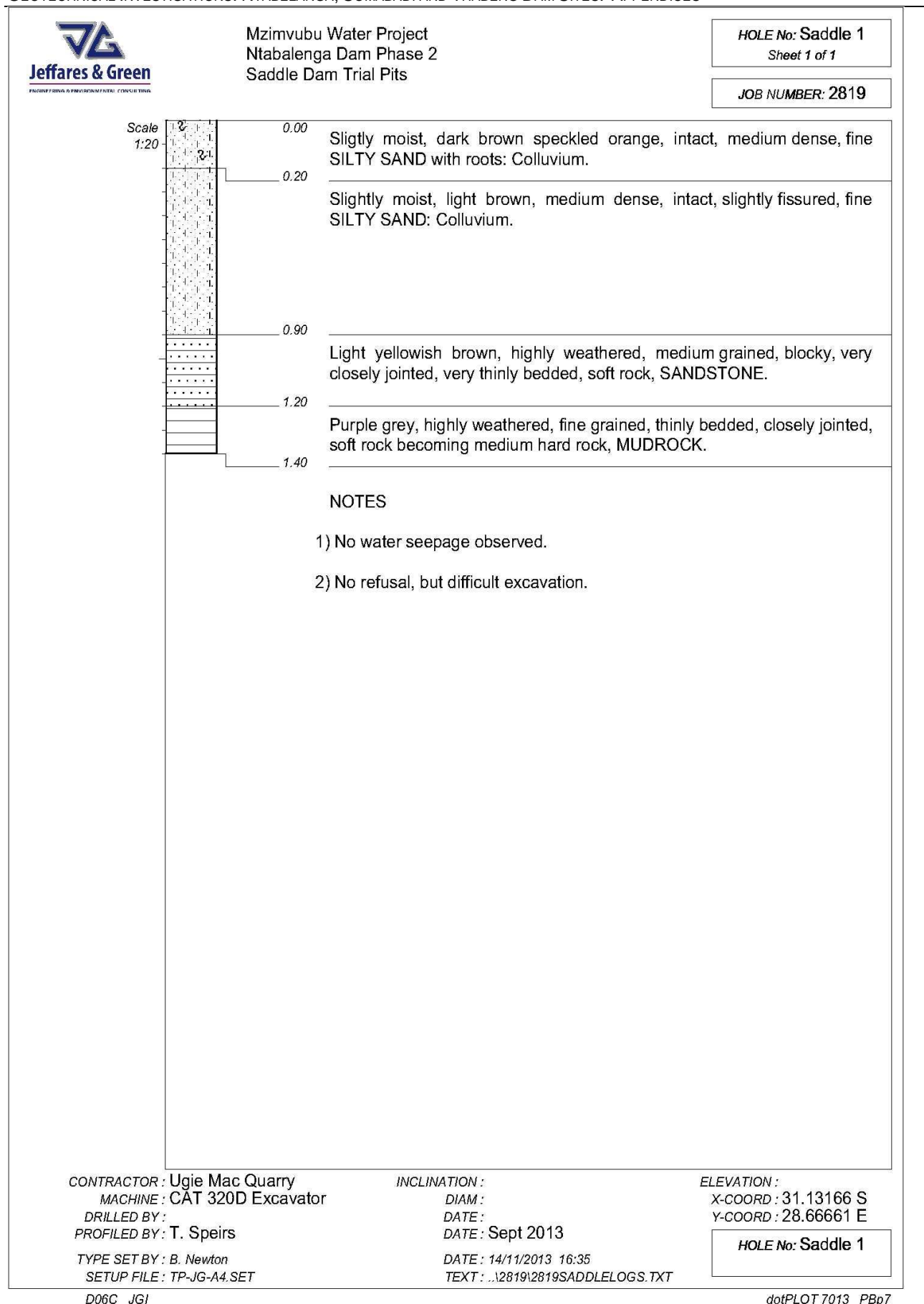


Fig G- 24: Saddle Dam Trial Pits Hole No: Saddle 1

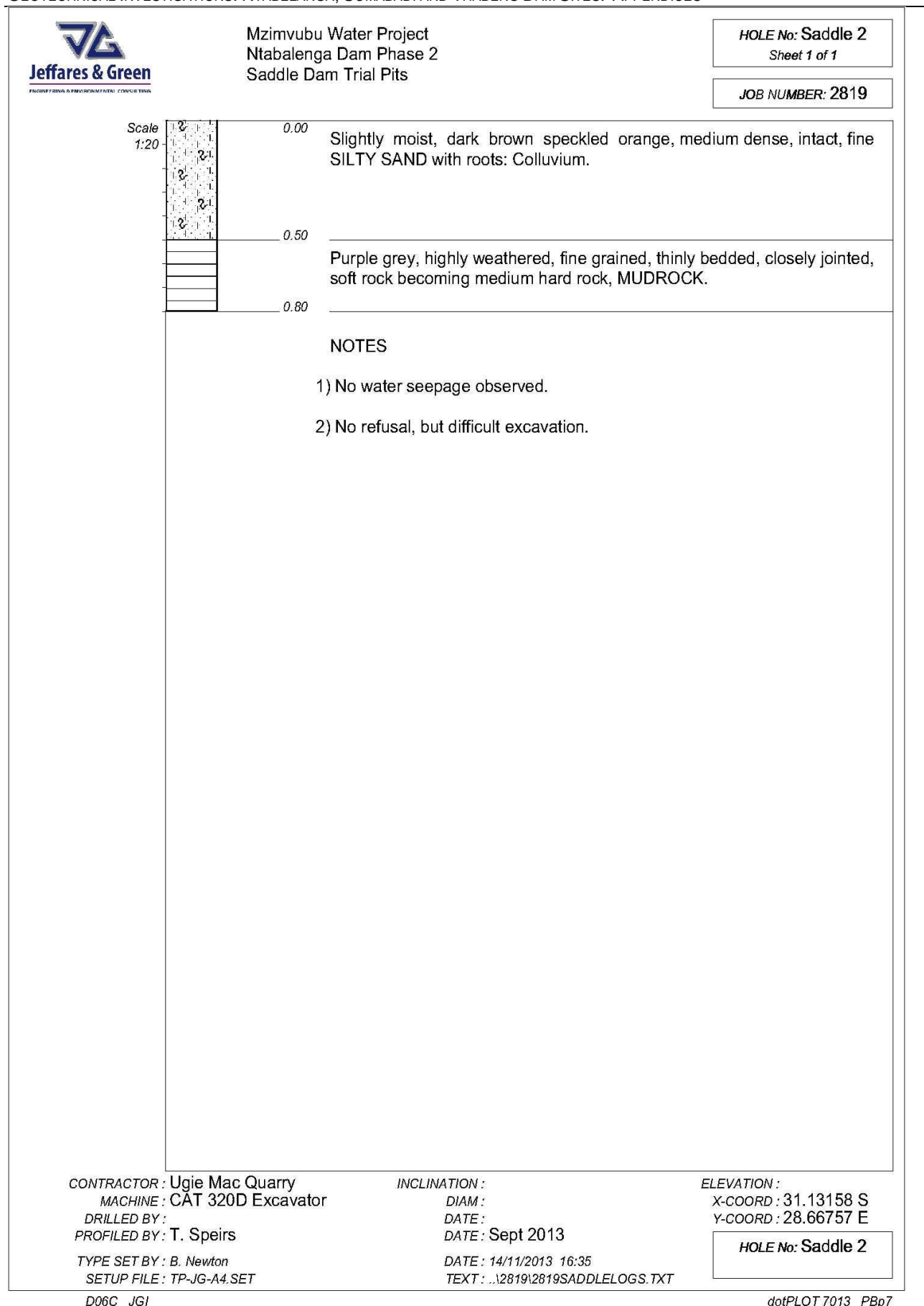


Fig G- 25: Saddle Dam Trial Pits Hole No: Saddle 2

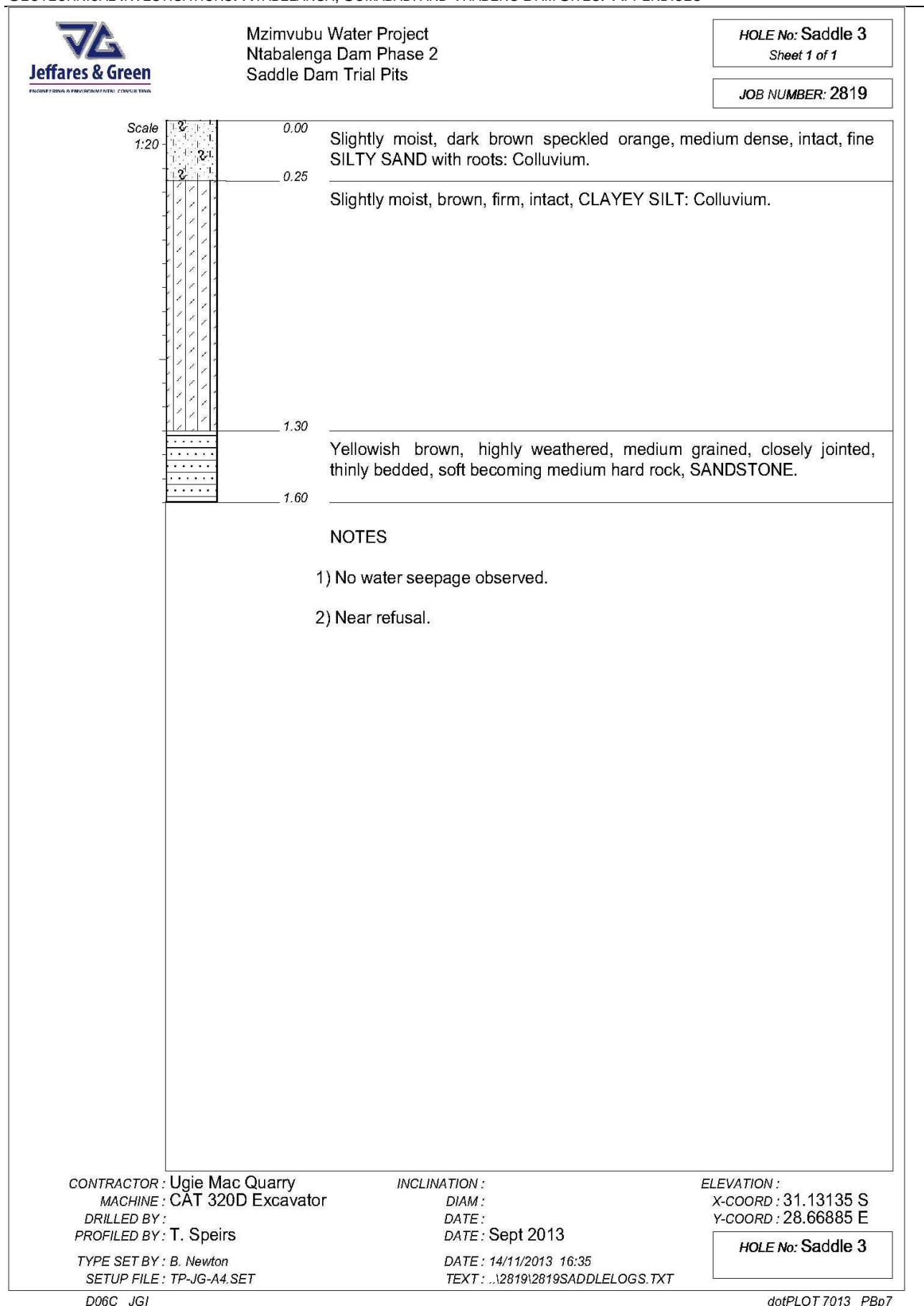


Fig G- 26: Saddle Dam Trial Pits Hole No: Saddle 3

G4:

CORE BORROW PIT TRIAL PITS

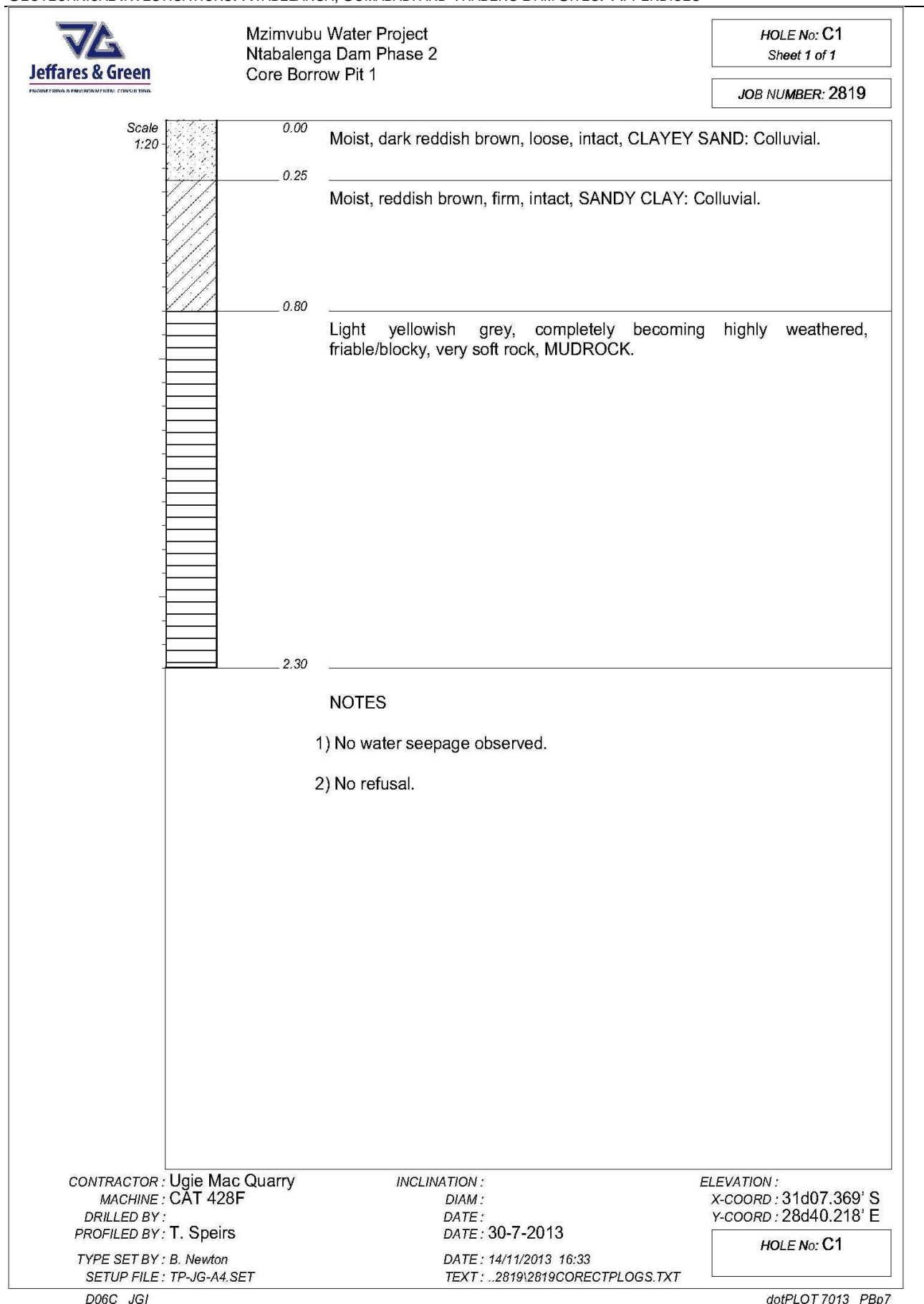


Fig G- 27-1: Core Borrow Pit 1 - Hole No: C1

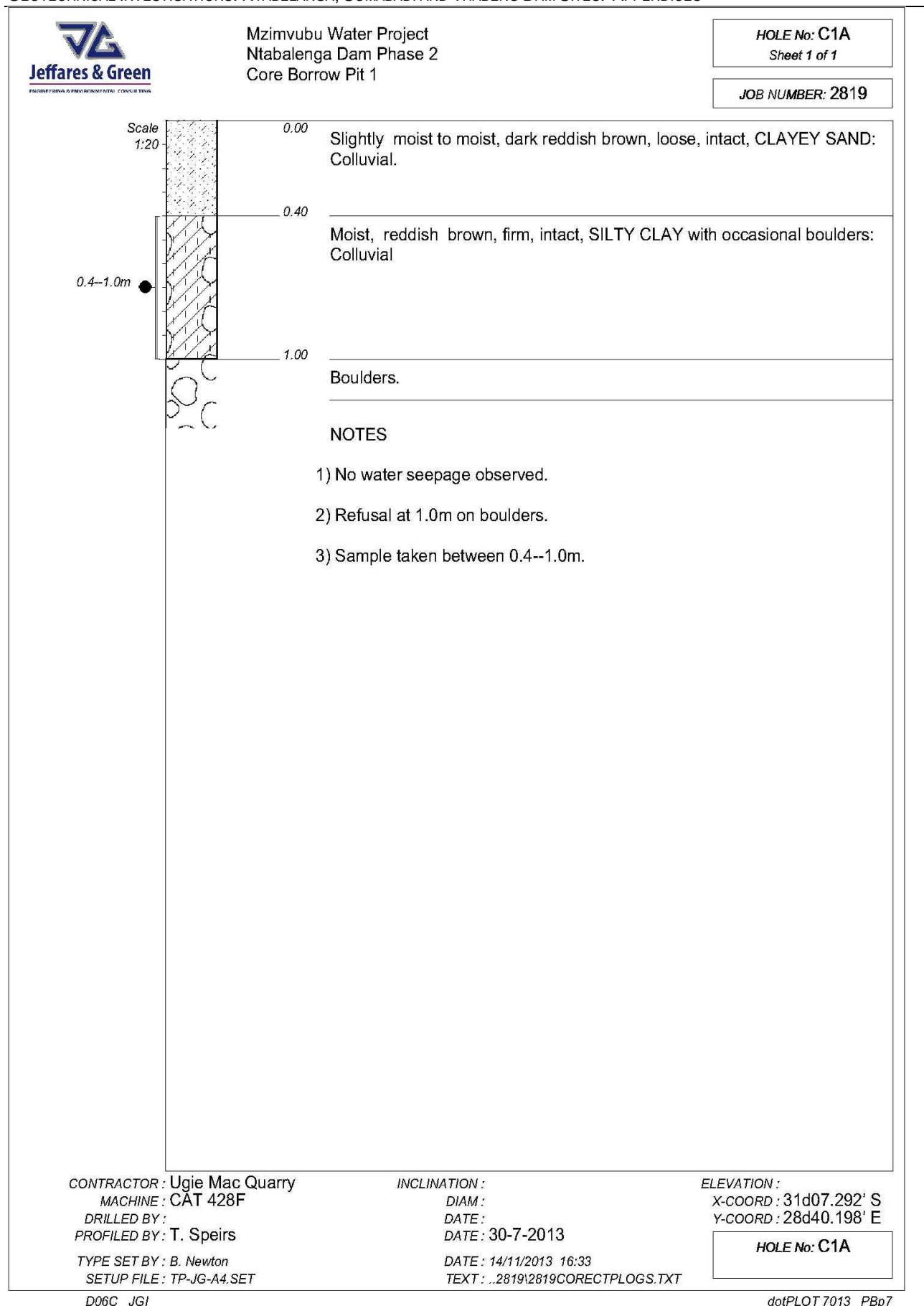


Fig G- 27-2: Core Borrow Pit 1 - Hole No: C1A

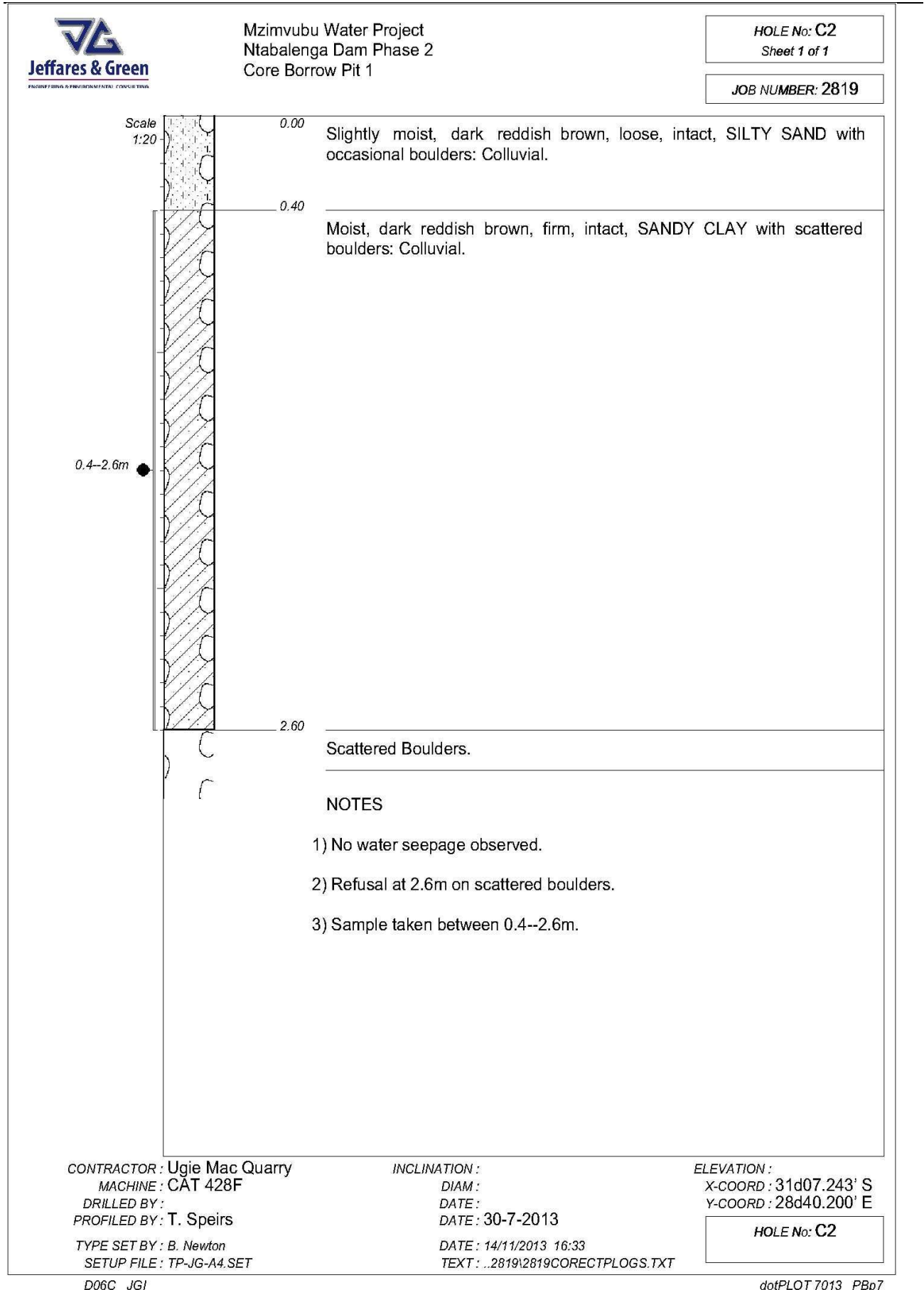


Fig G- 28-1: Core Borrow Pit 1 - Hole No: C2

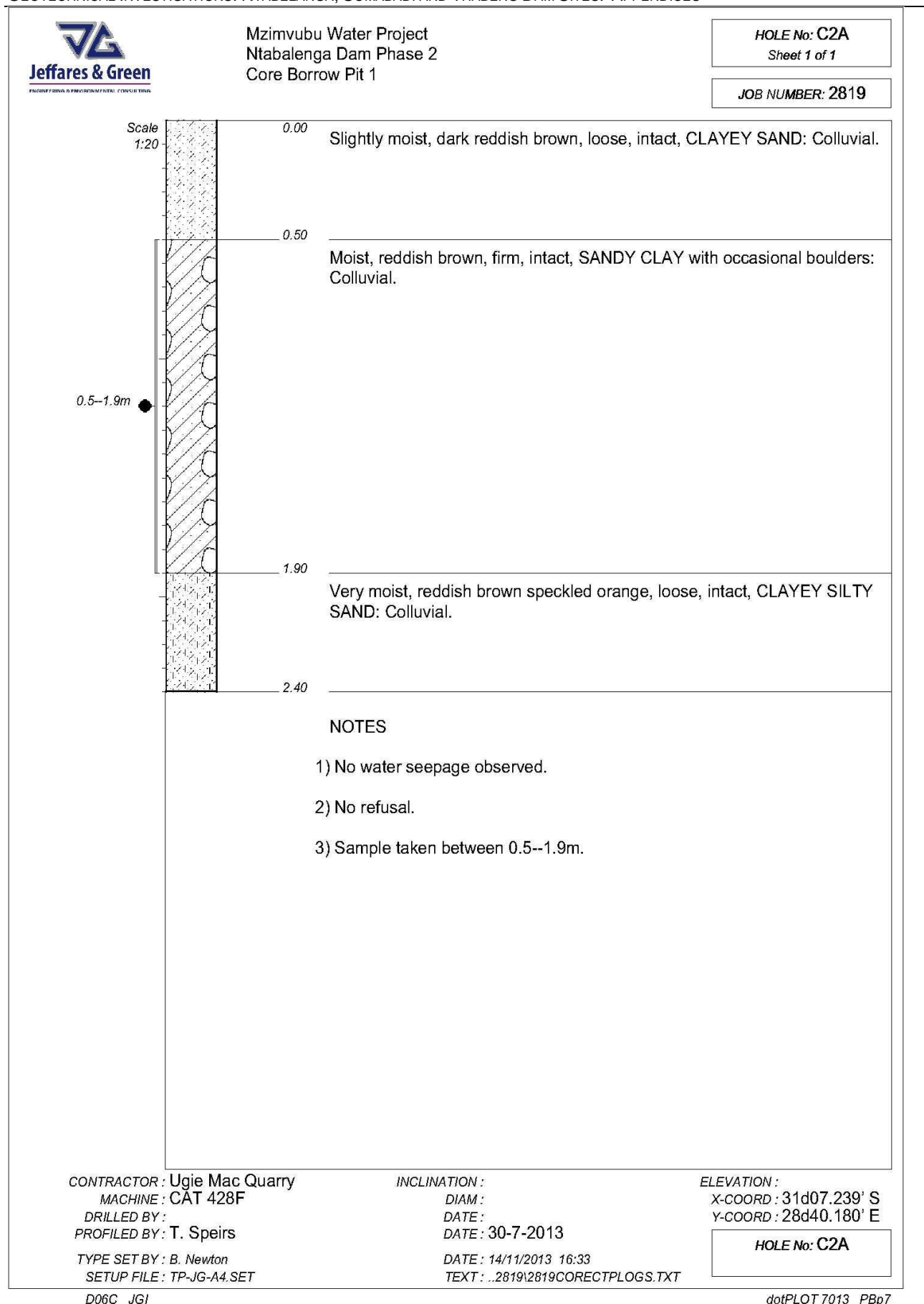


Fig G- 28-2: Core Borrow Pit 1 - Hole No: C2A

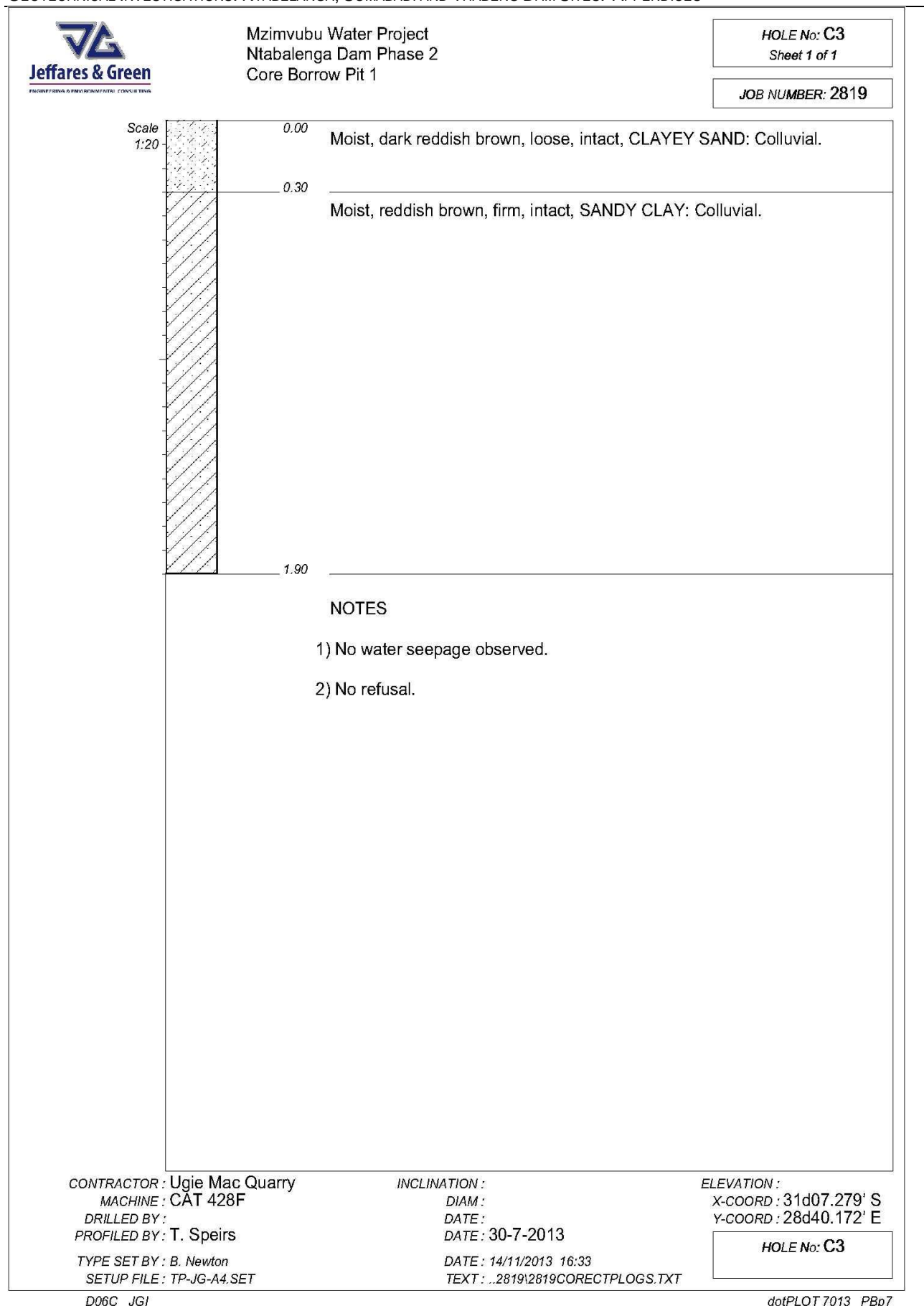


Fig G- 29: Core Borrow Pit 1 - Hole No: C3

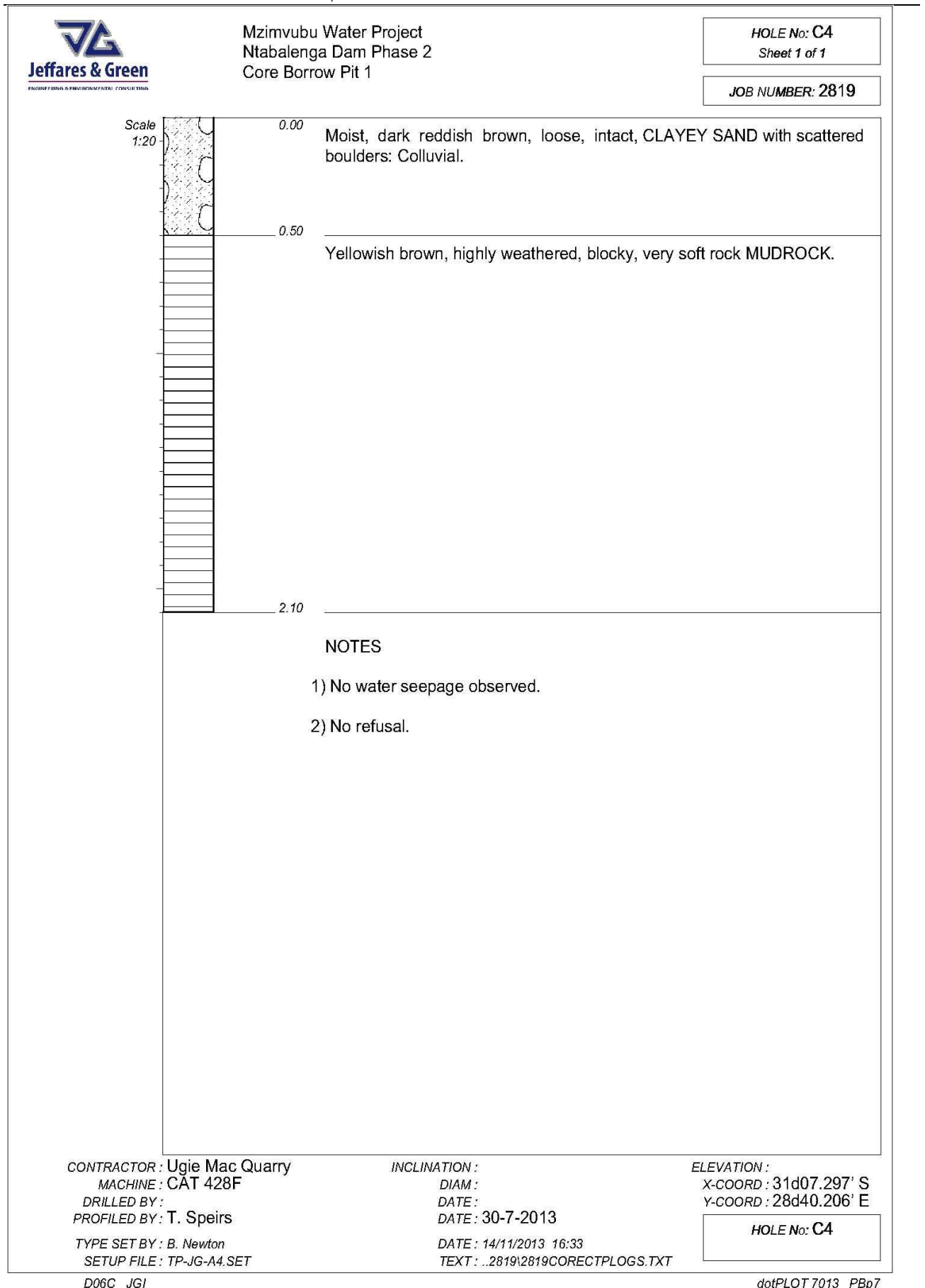


Fig G- 30-1: Core Borrow Pit 1 - Hole No: C4

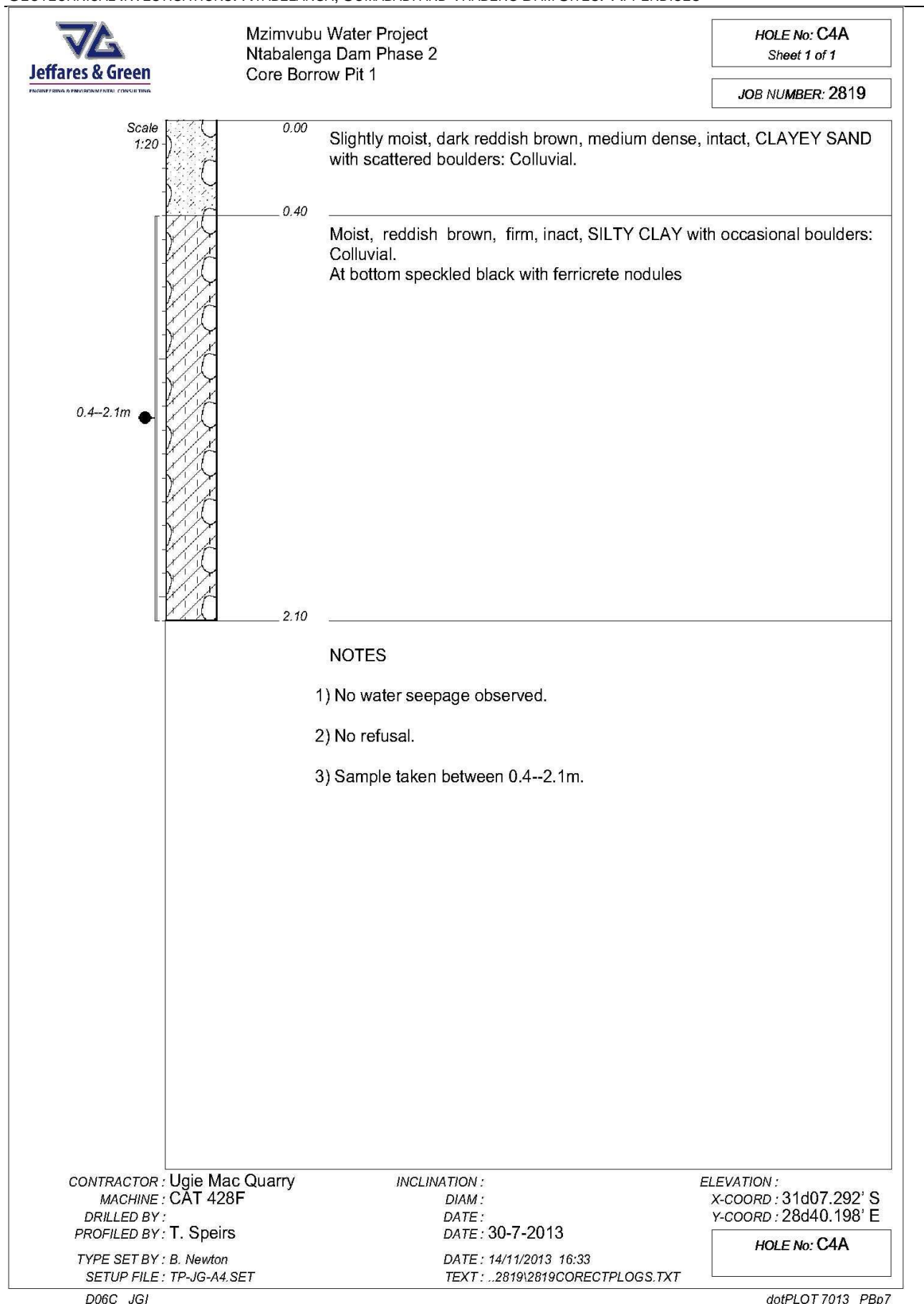


Fig G- 30-2: Core Borrow Pit 1 - Hole No: C4A

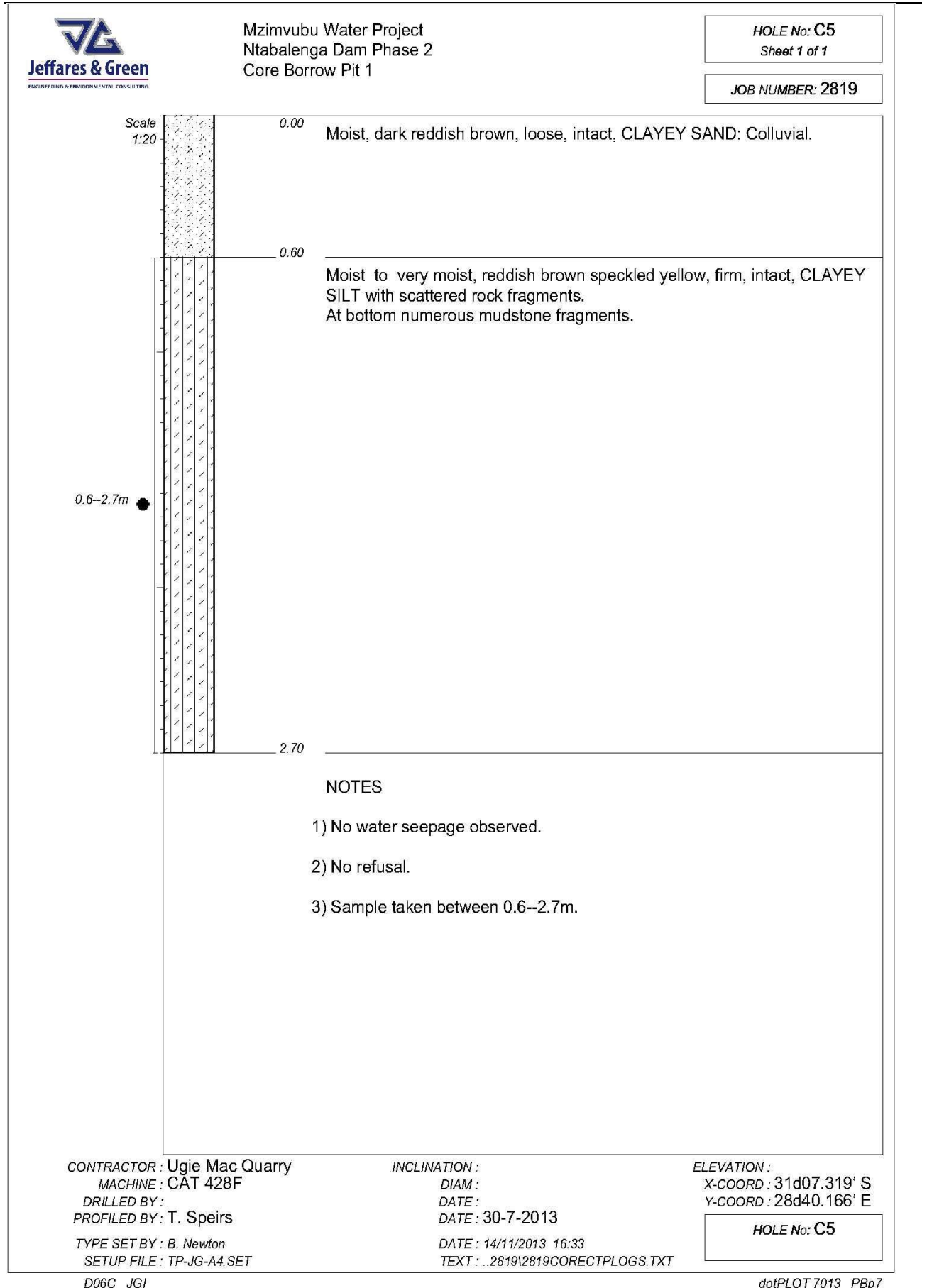


Fig G- 31: Core Borrow Pit 1 - Hole No: C5

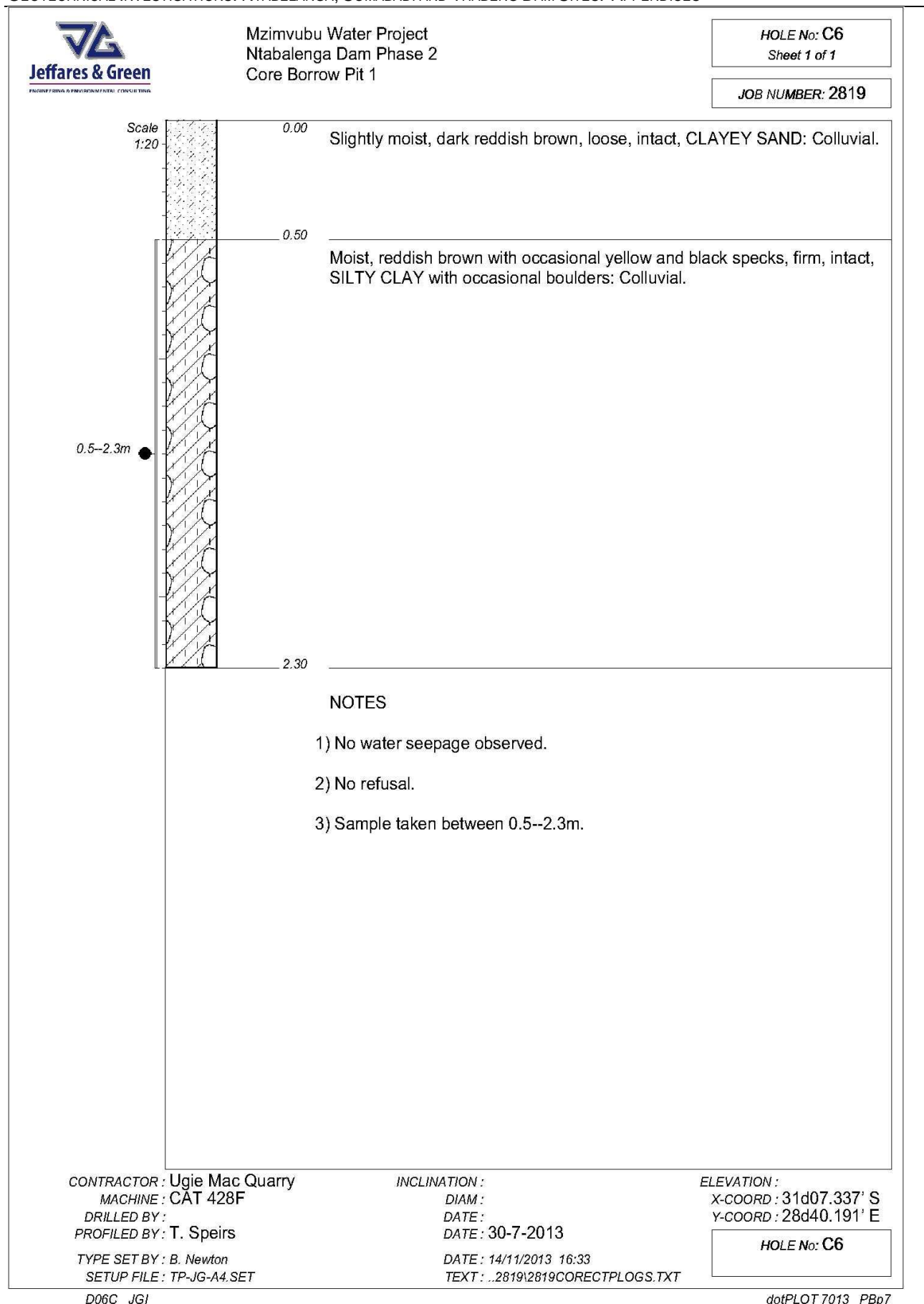


Fig G- 32: Core Borrow Pit 1 - Hole No: C6

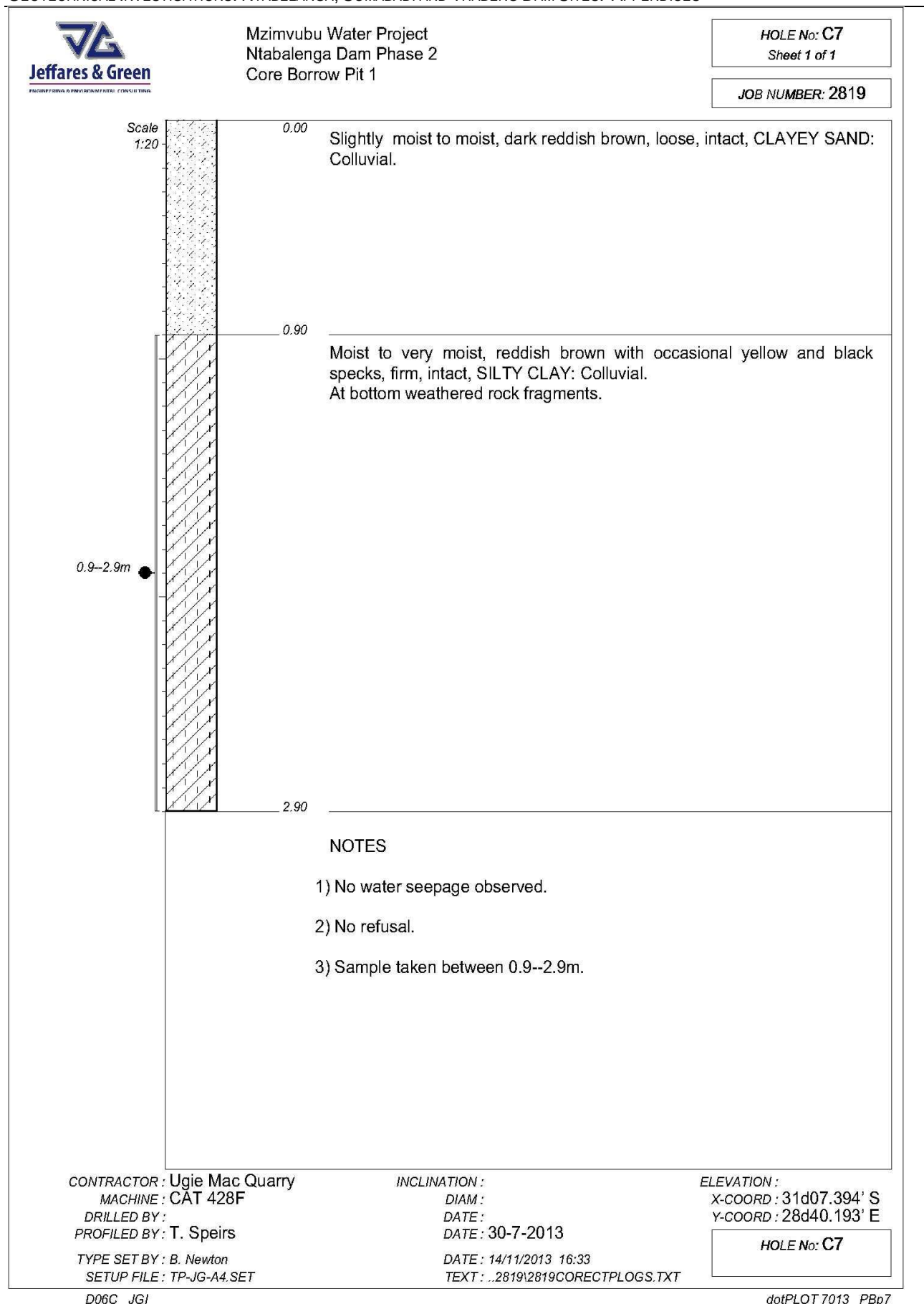


Fig G- 33: Core Borrow Pit 1 - Hole No: C7

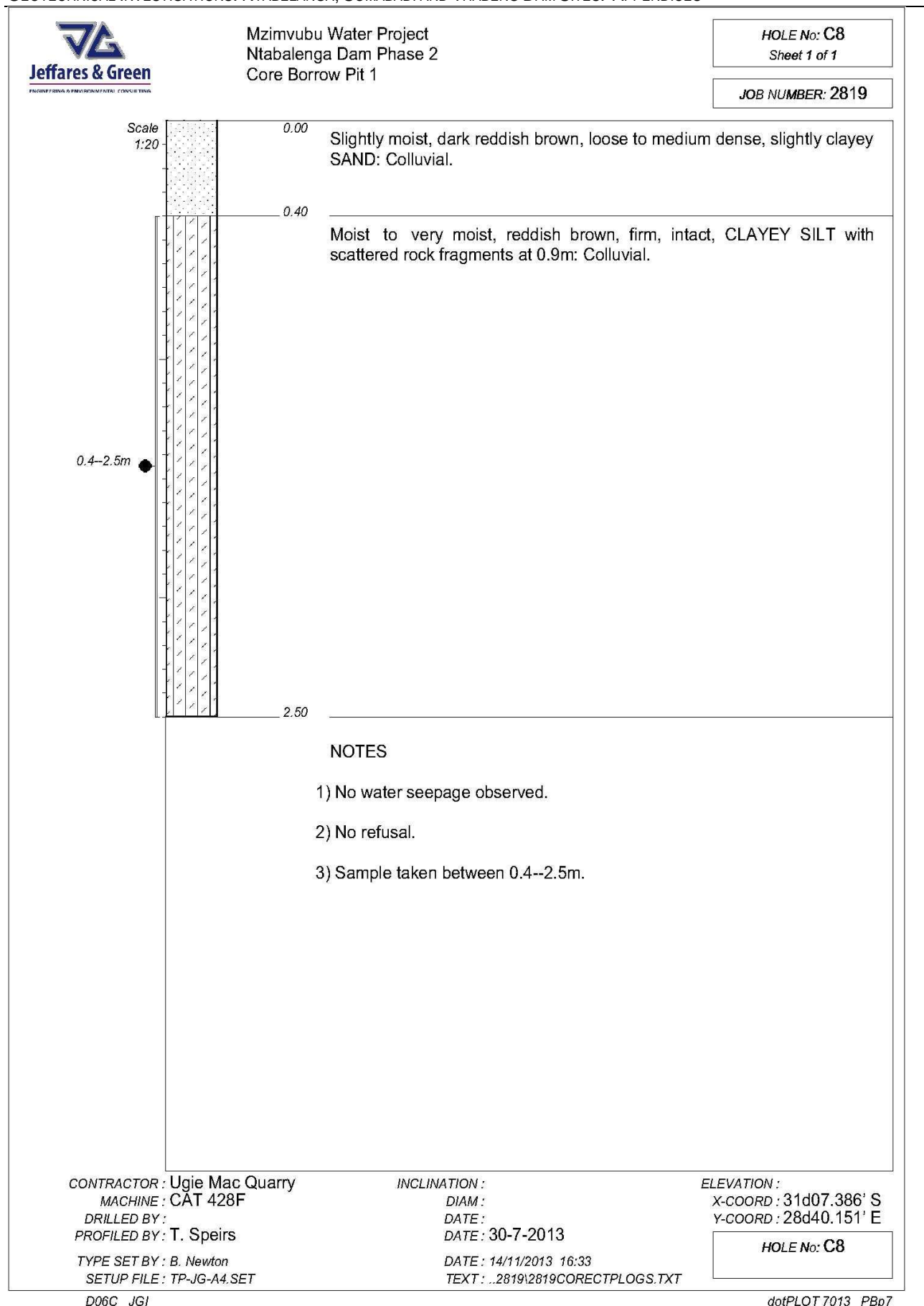


Fig G- 34: Core Borrow Pit 1 - Hole No: C8

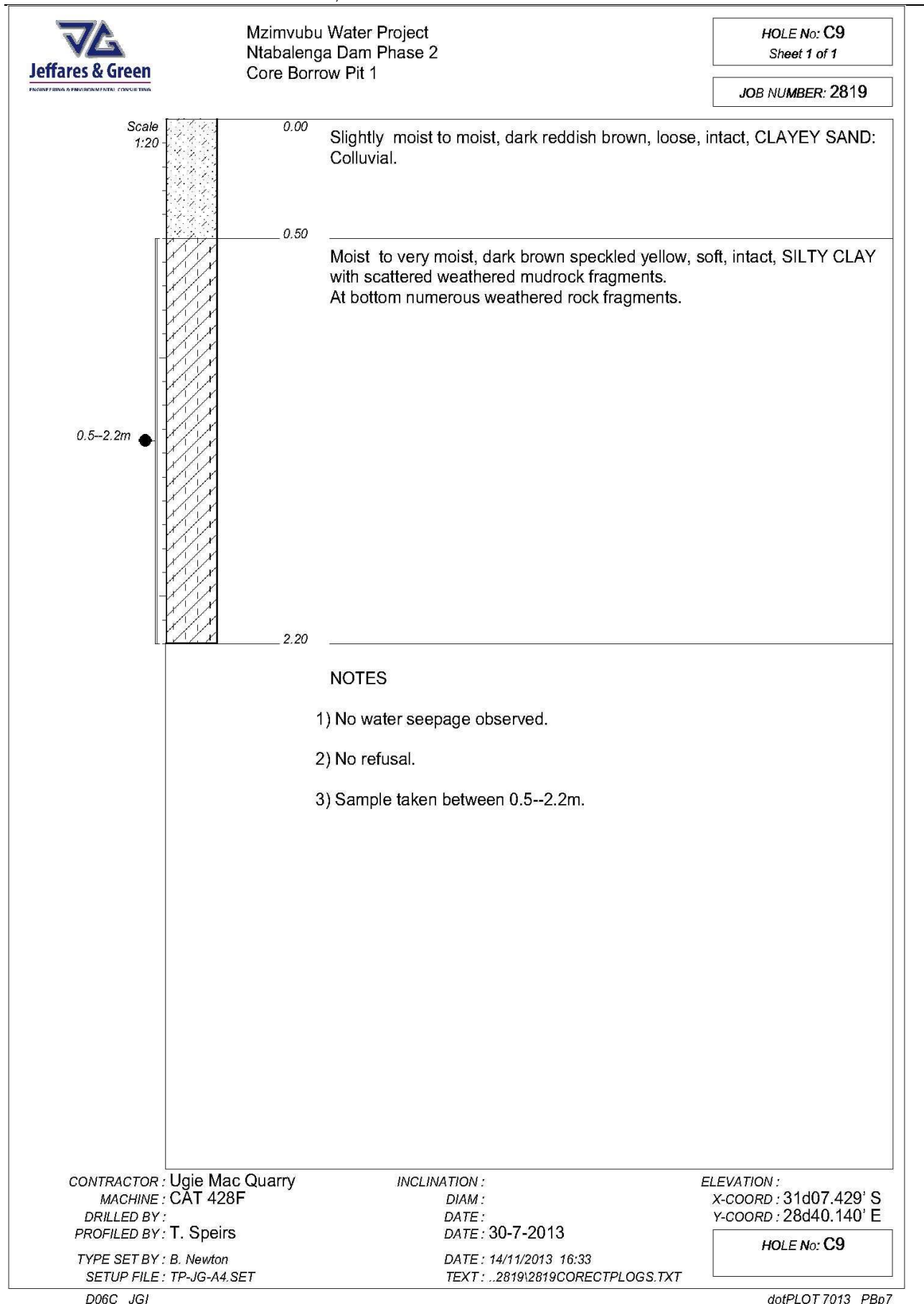


Fig G- 35: Core Borrow Pit 1 - Hole No: C9

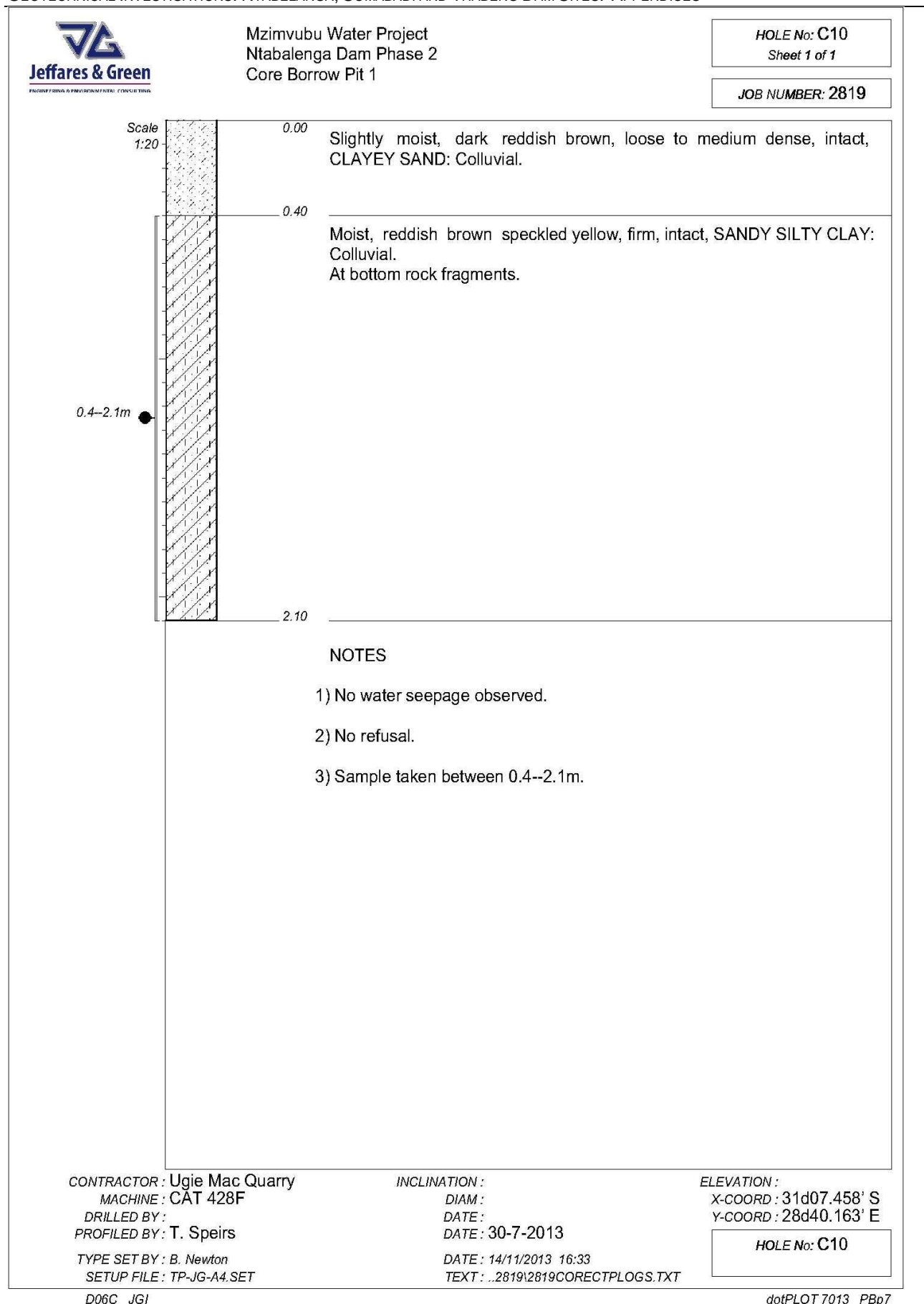


Fig G- 36: Core Borrow Pit 1 - Hole No: C10

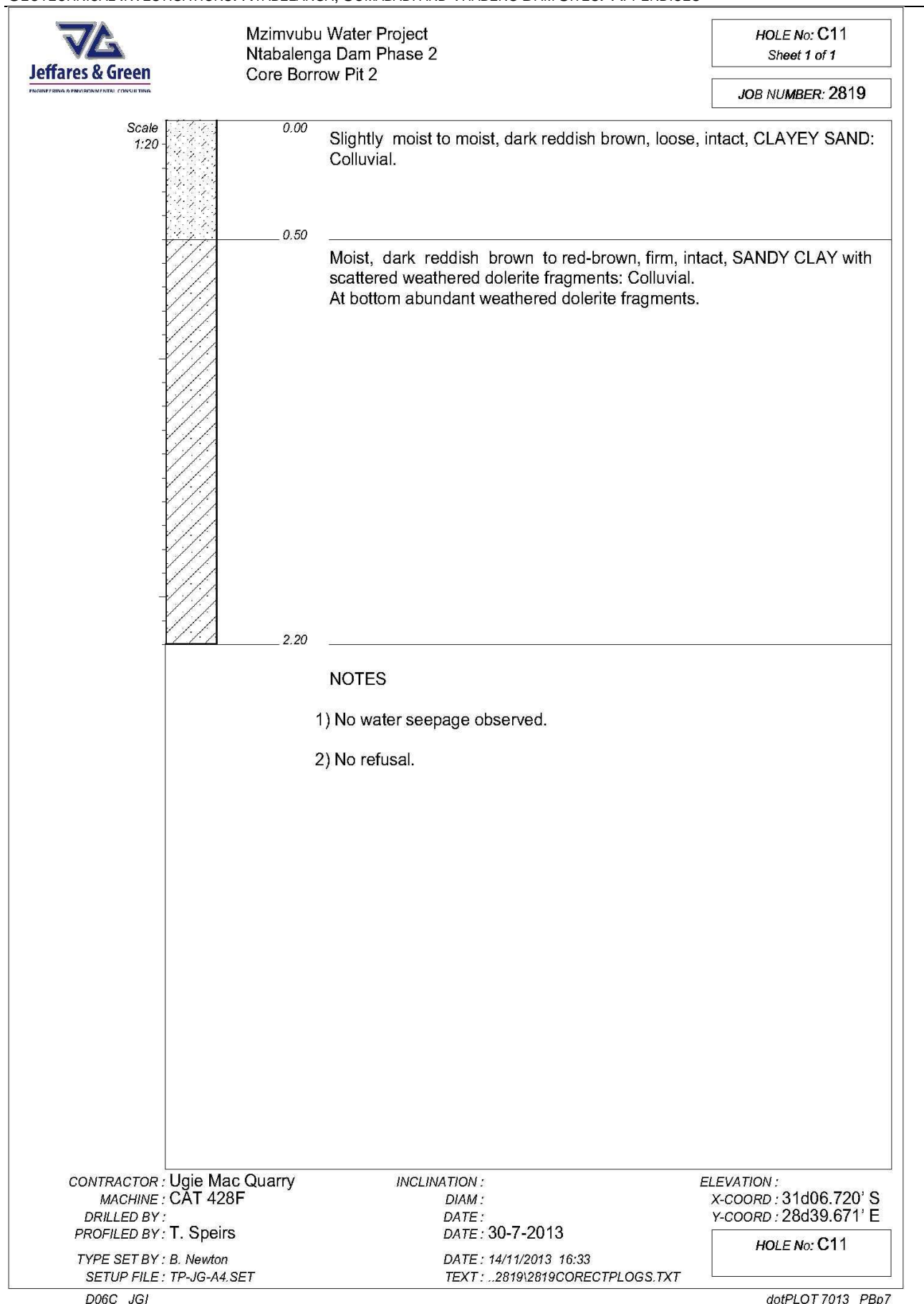


Fig G- 37: Core Borrow Pit 2 - Hole No: C11

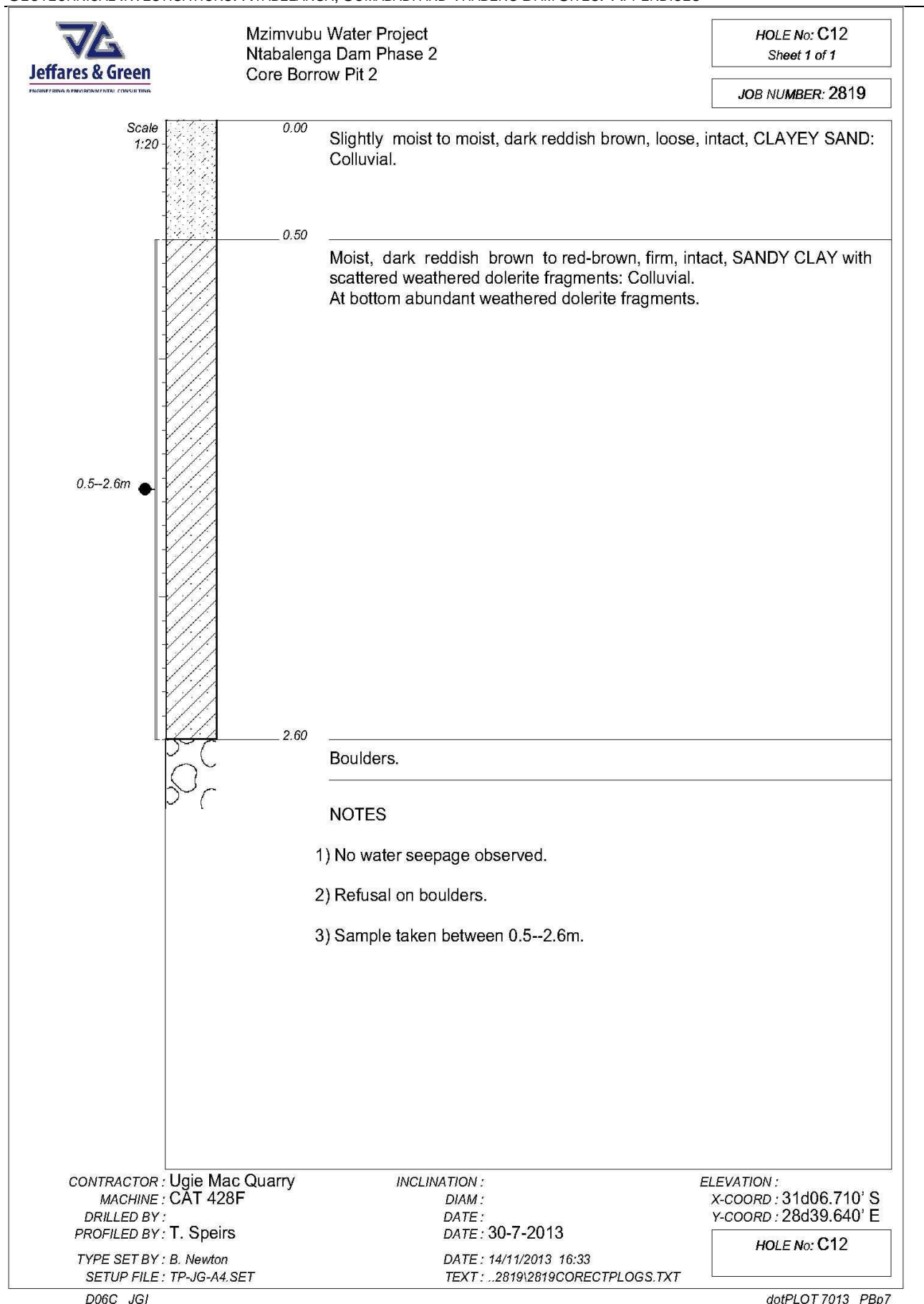


Fig G- 37: Core Borrow Pit 2 - Hole No: C12

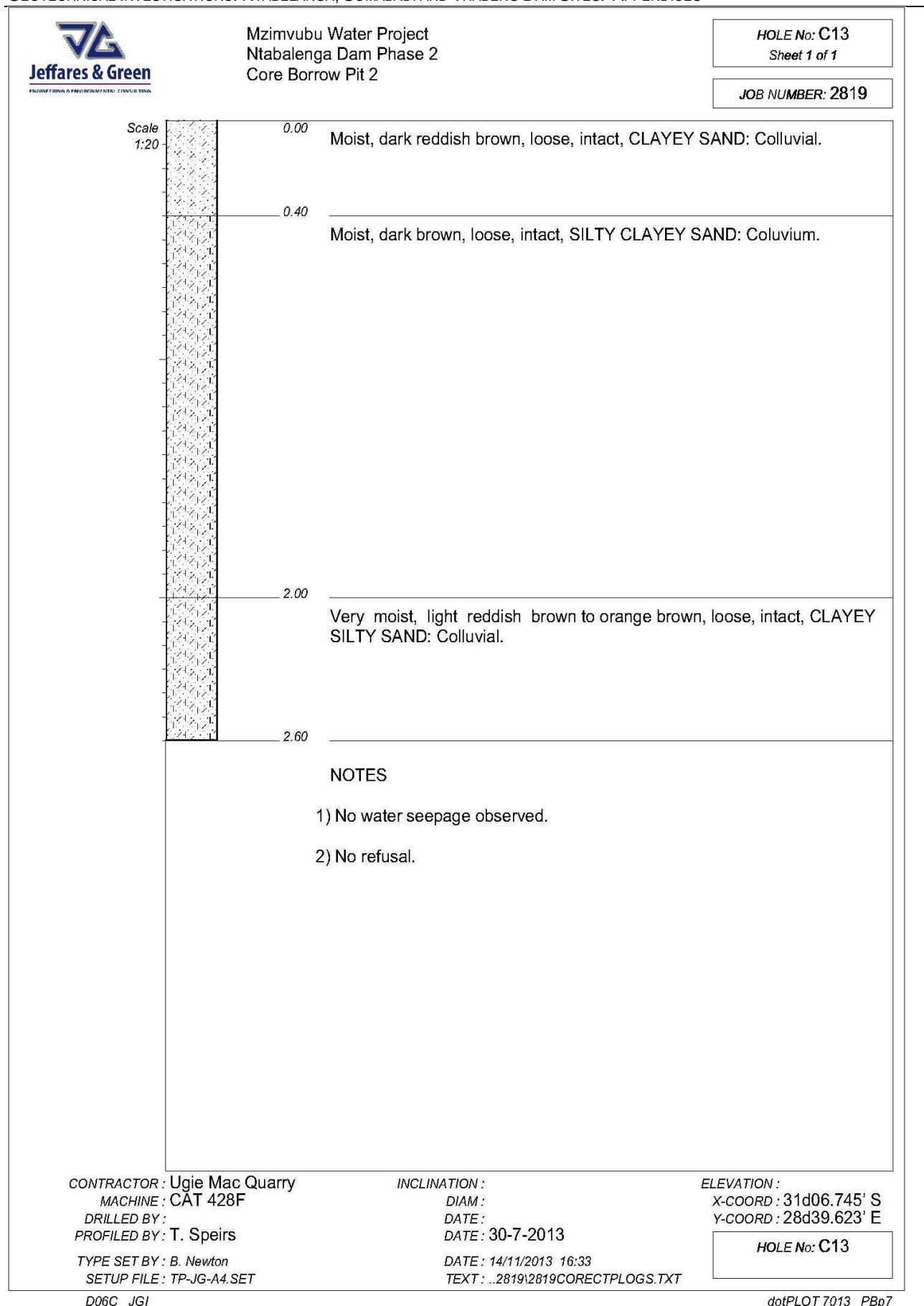


Fig G- 38: Core Borrow Pit 2 - Hole No: C13

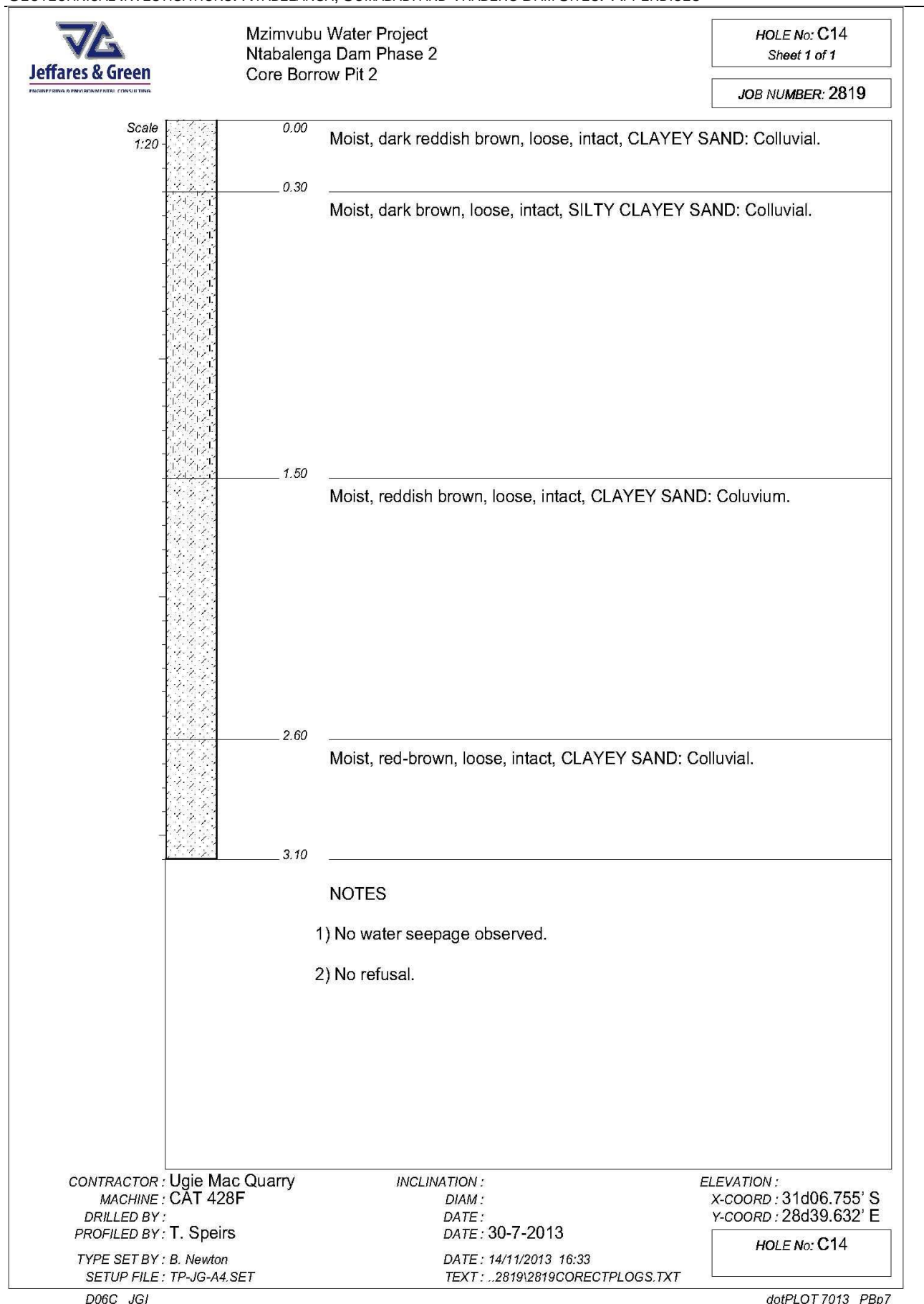


Fig G- 39: Core Borrow Pit 2 - Hole No: C14

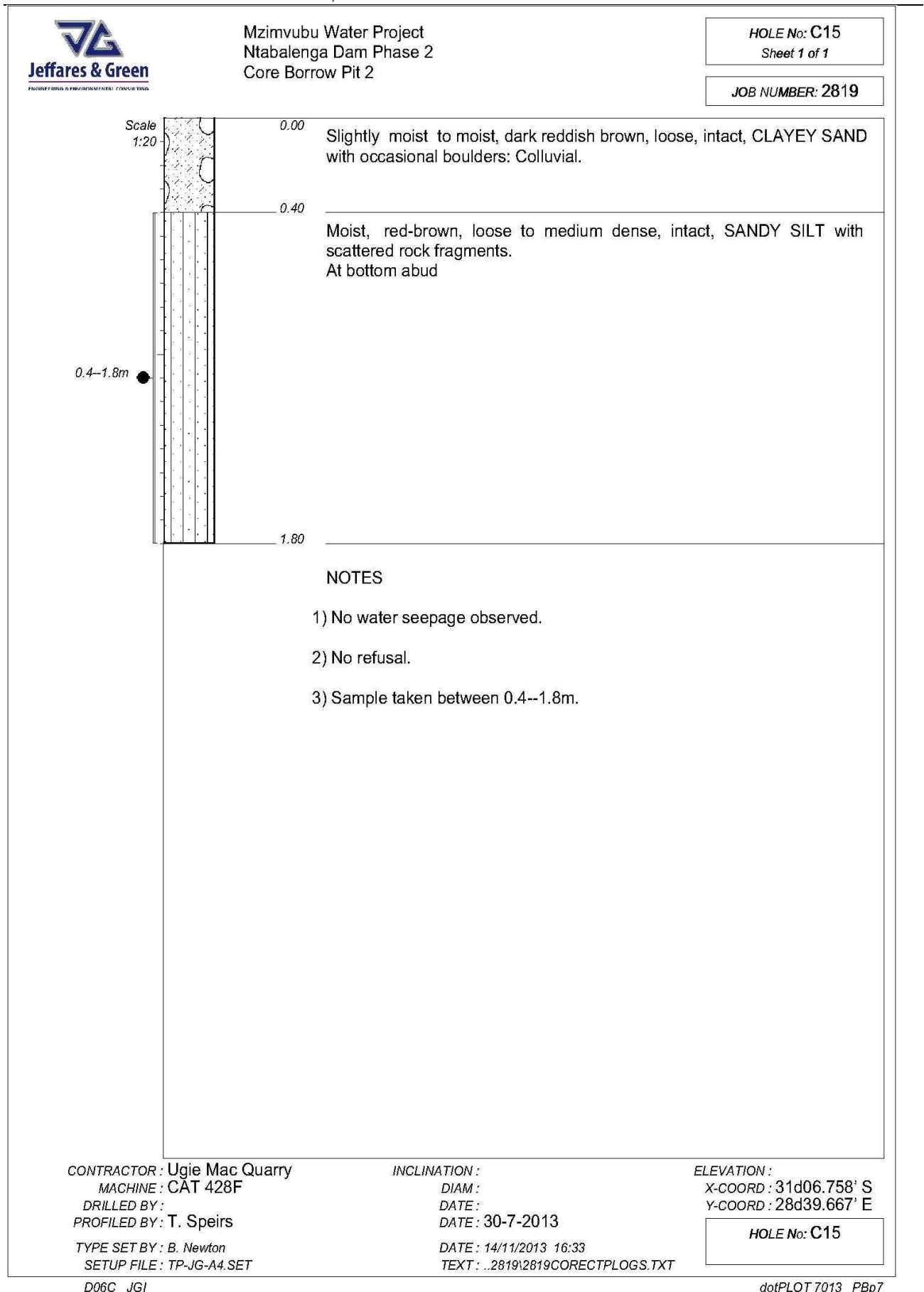


Fig G- 40: Core Borrow Pit 2 - Hole No: C15

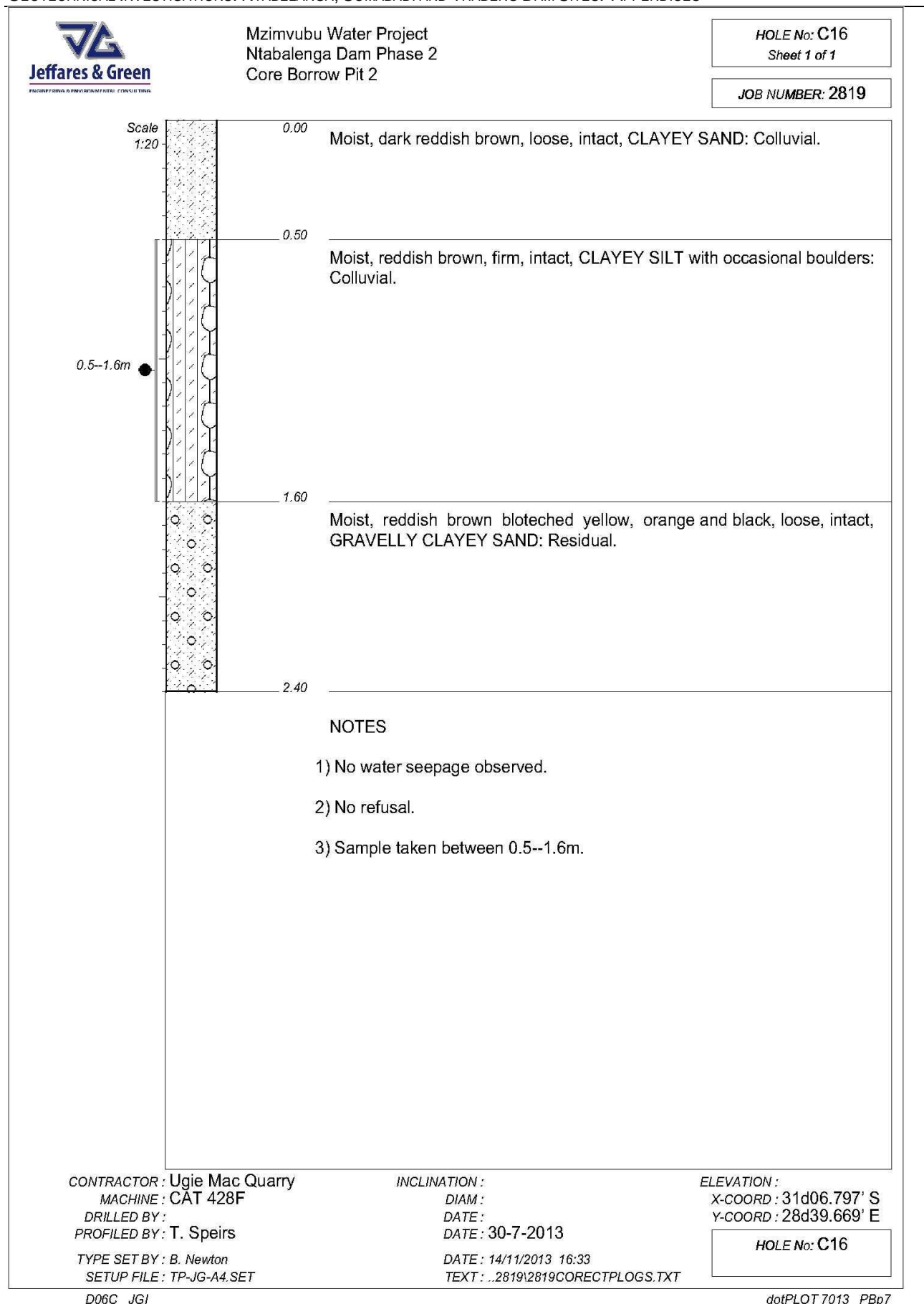


Fig G- 41: Core Borrow Pit 2 - Hole No: C16

HOLE No: C18
Sheet 1 of 1

Scale 1:20

0.00 Slightly moist, dark reddish brown, loose, intact, CLAYEY SAND: Colluvial.

0.30 Moist, dark brown, loose to medium dense, intact, CLAYEY SAND: Colluvial.

1.40 Moist, reddish brown, loose to medium dense, intact, CLAYEY SAND: Colluvial.

1.90 Moist to very moist, red-brown, loose, intact, CLAYEY SAND: Colluvial.

2.90

0.3—2.9m

- 1) No water seepage observed.
- 2) No refusal.
- 3) Sample taken between 0.3--2.9m.

HOLE No: C18

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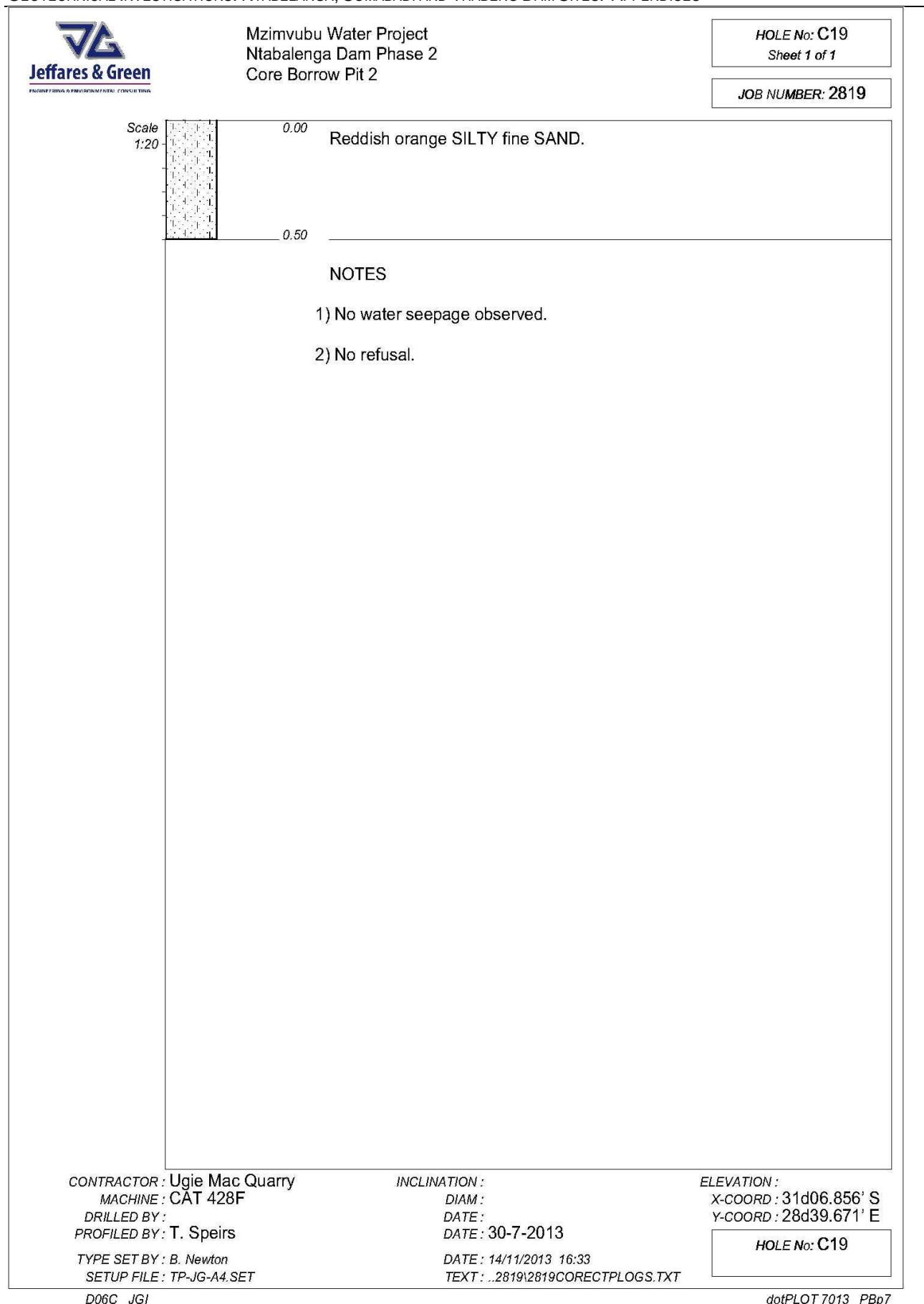


Fig G- 44: Core Borrow Pit 2 - Hole No: C19

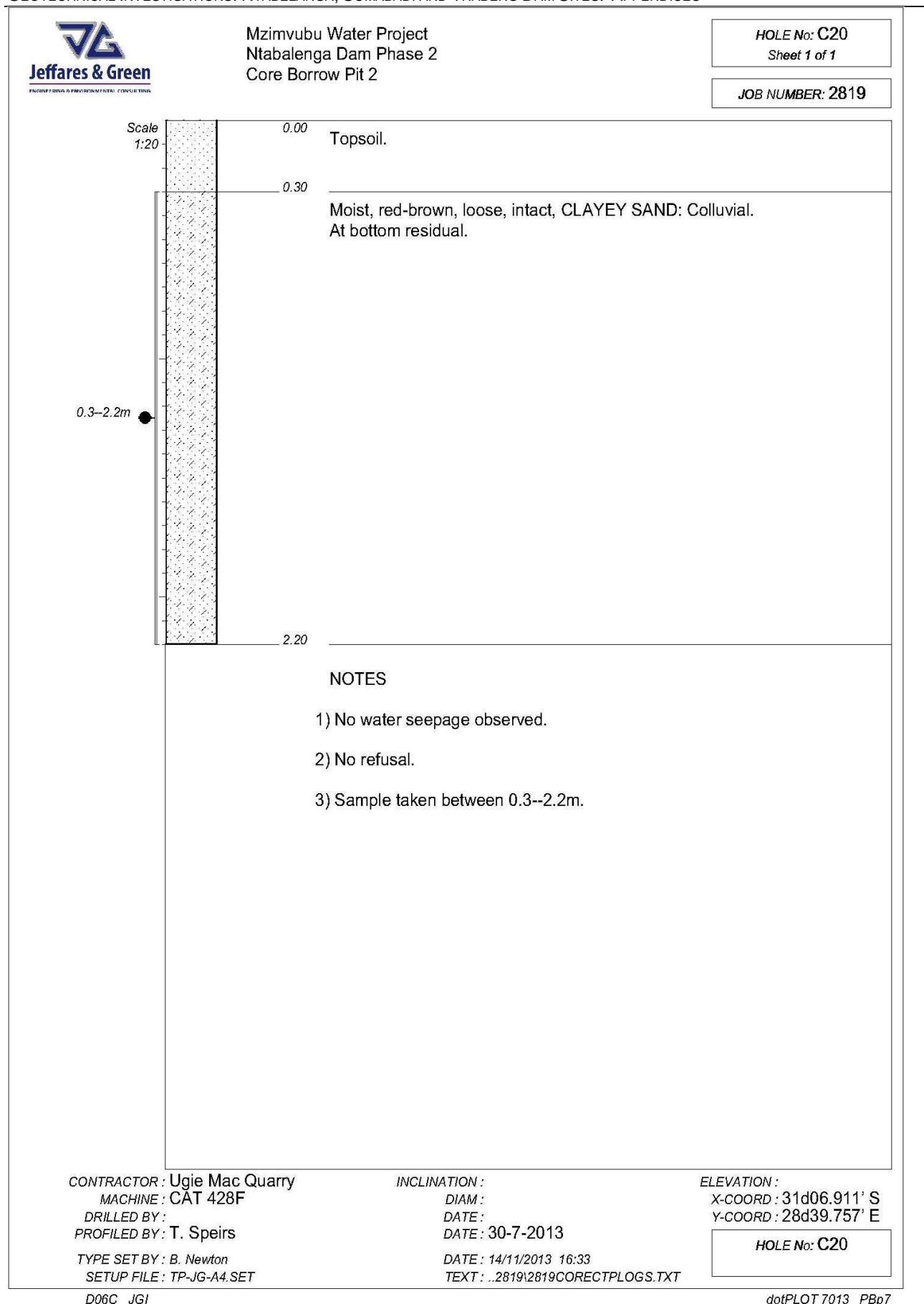


Fig G- 45: Core Borrow Pit 2 - Hole No: C20

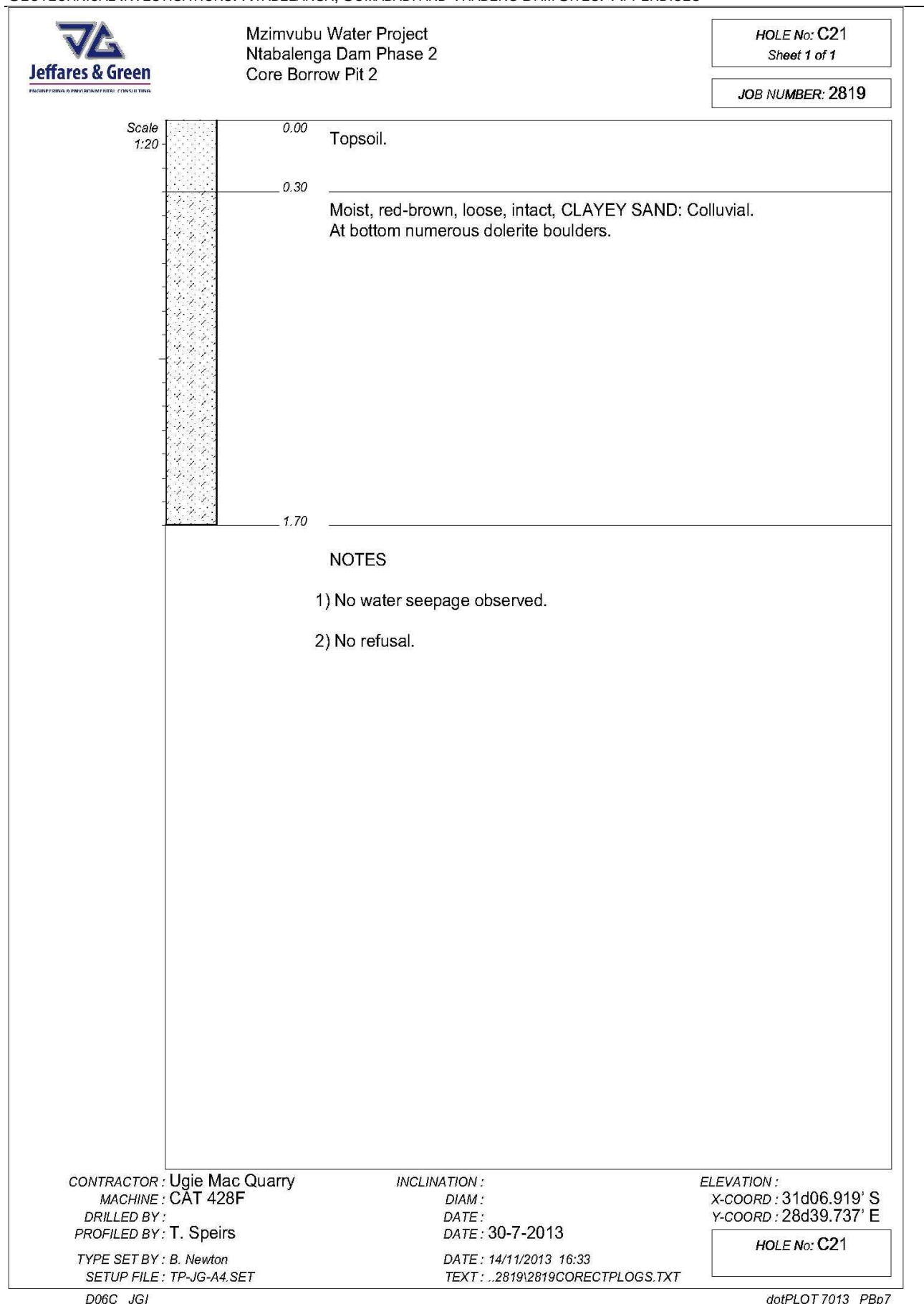


Fig G- 46: Core Borrow Pit 2 - Hole No: C21

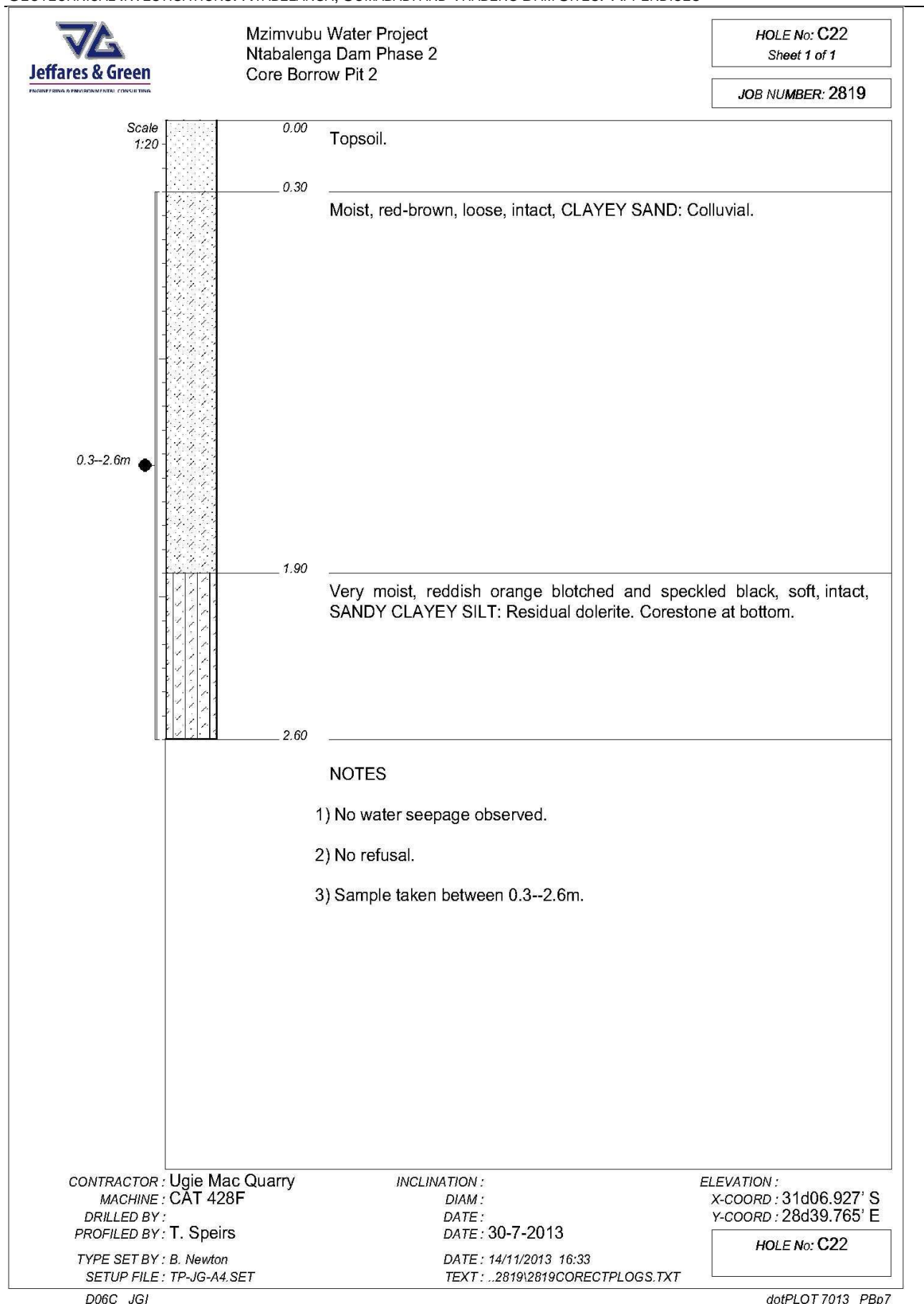


Fig G- 47: Core Borrow Pit 2 - Hole No: C22

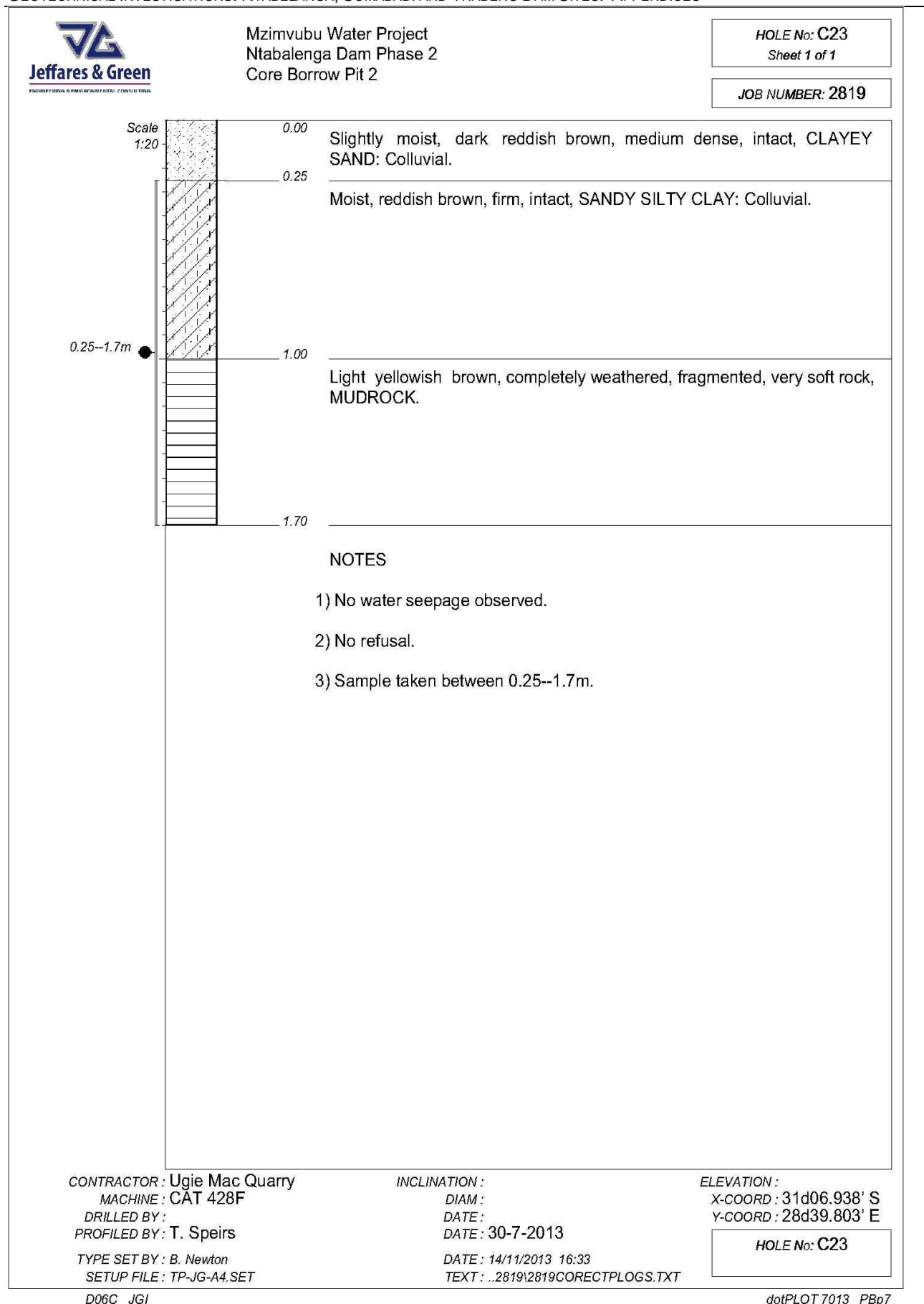


Fig G- 48: Core Borrow Pit 2 - Hole No: C23

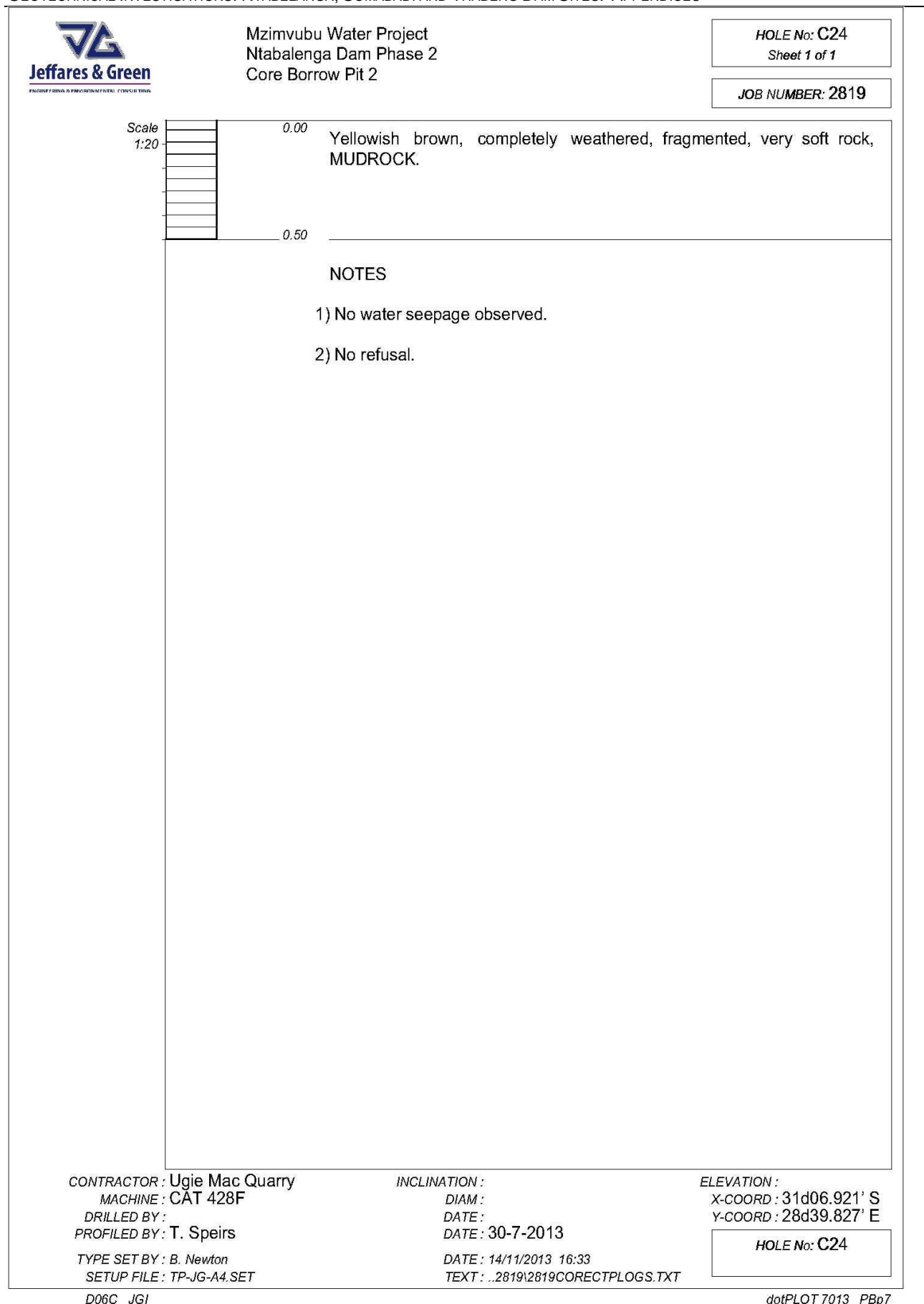


Fig G- 49: Core Borrow Pit 2 - Hole No: C24

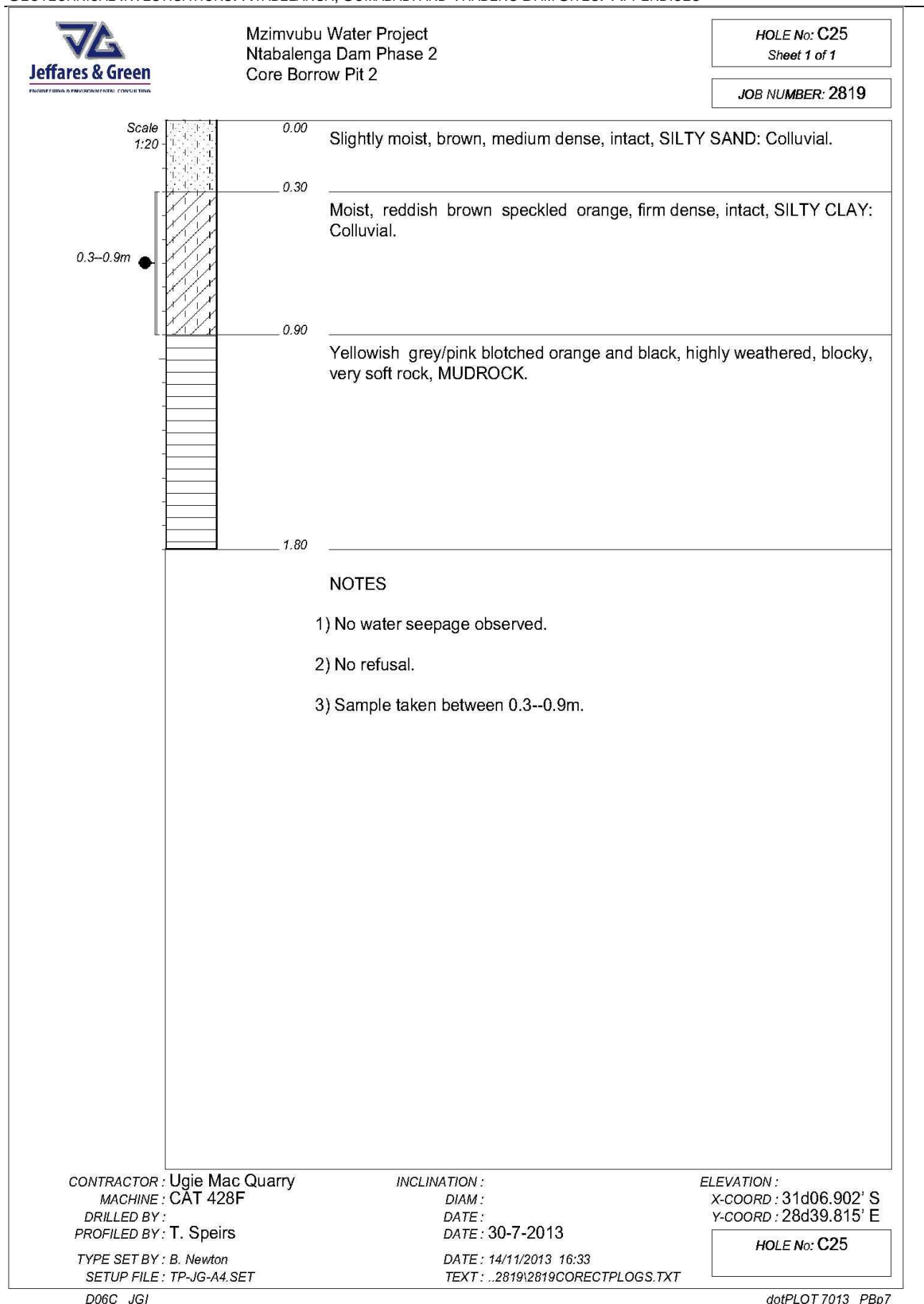


Fig G- 50: Core Borrow Pit 2 - Hole No: C25

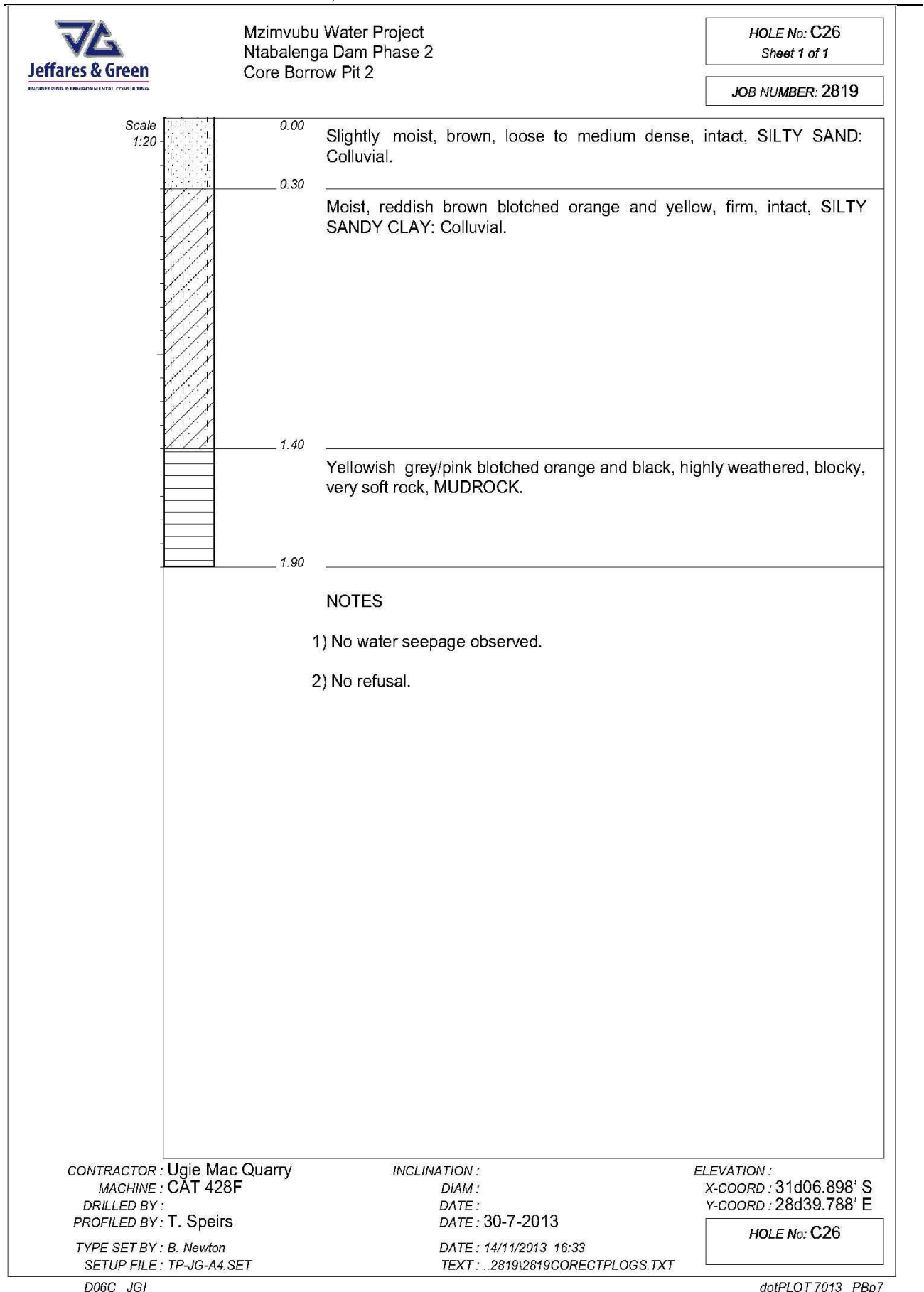


Fig G- 51: Core Borrow Pit 2 - Hole No: C26

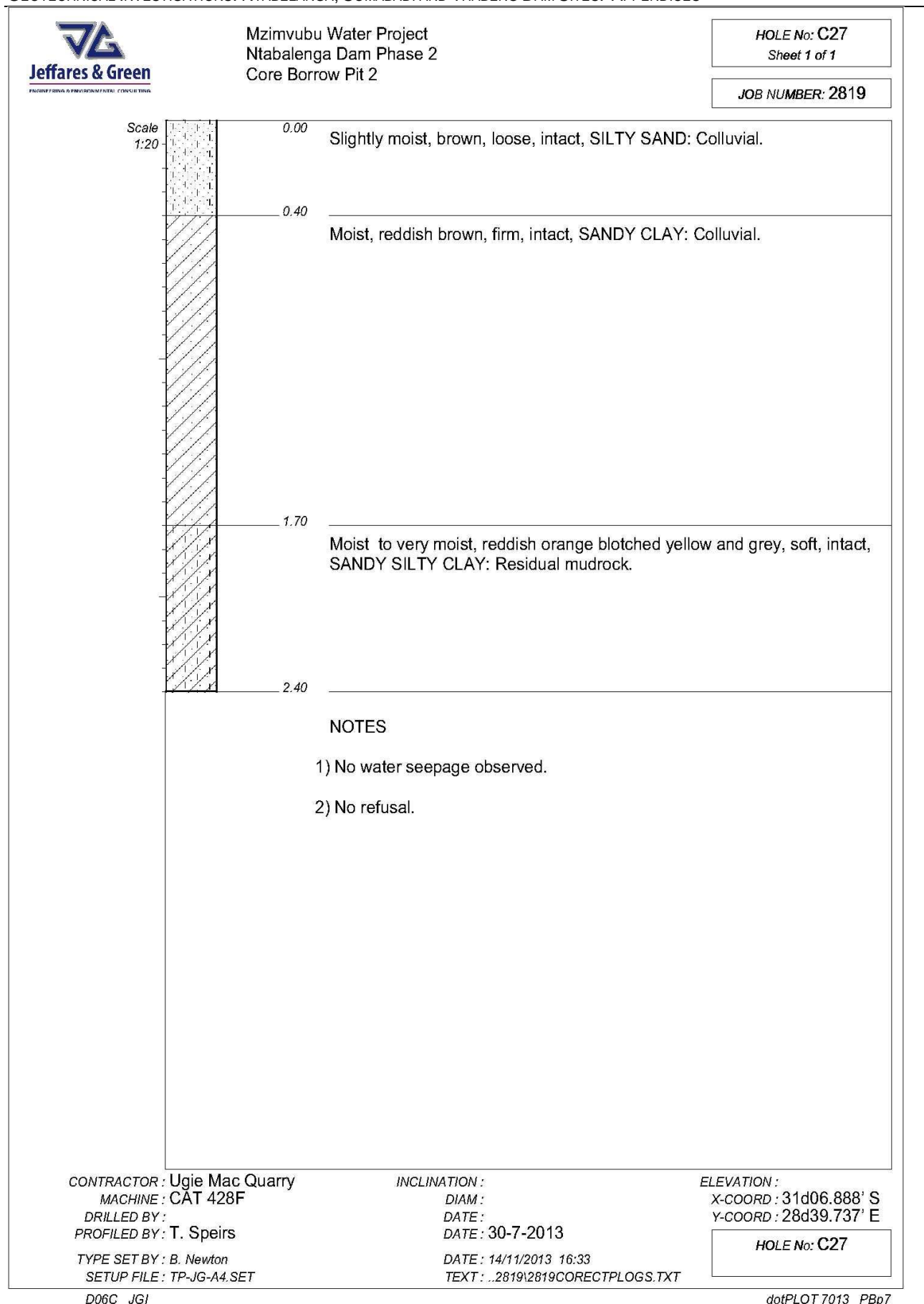


Fig G- 52: Core Borrow Pit 2 - Hole No: C27

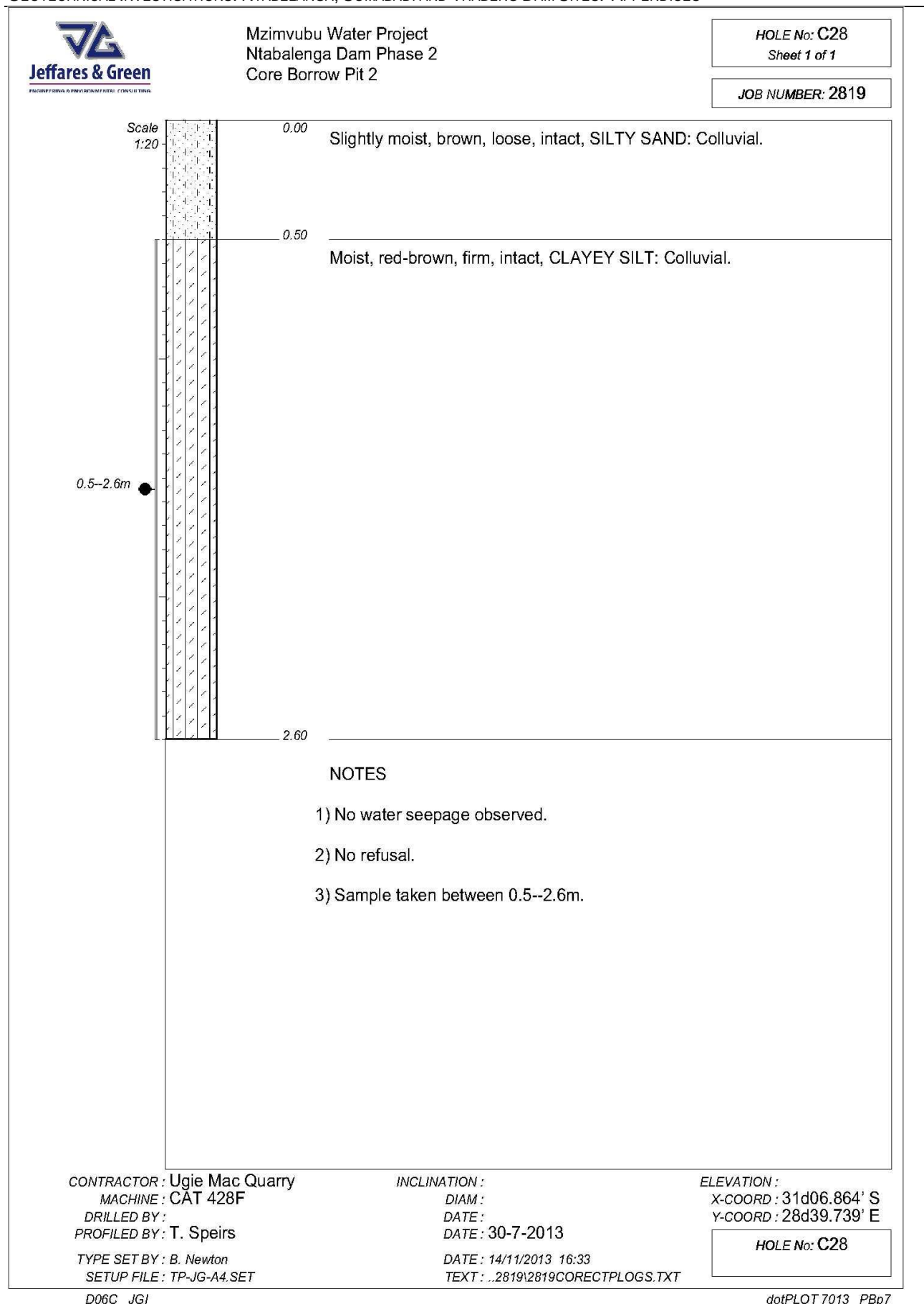


Fig G- 53: Core Borrow Pit 2 - Hole No: C28

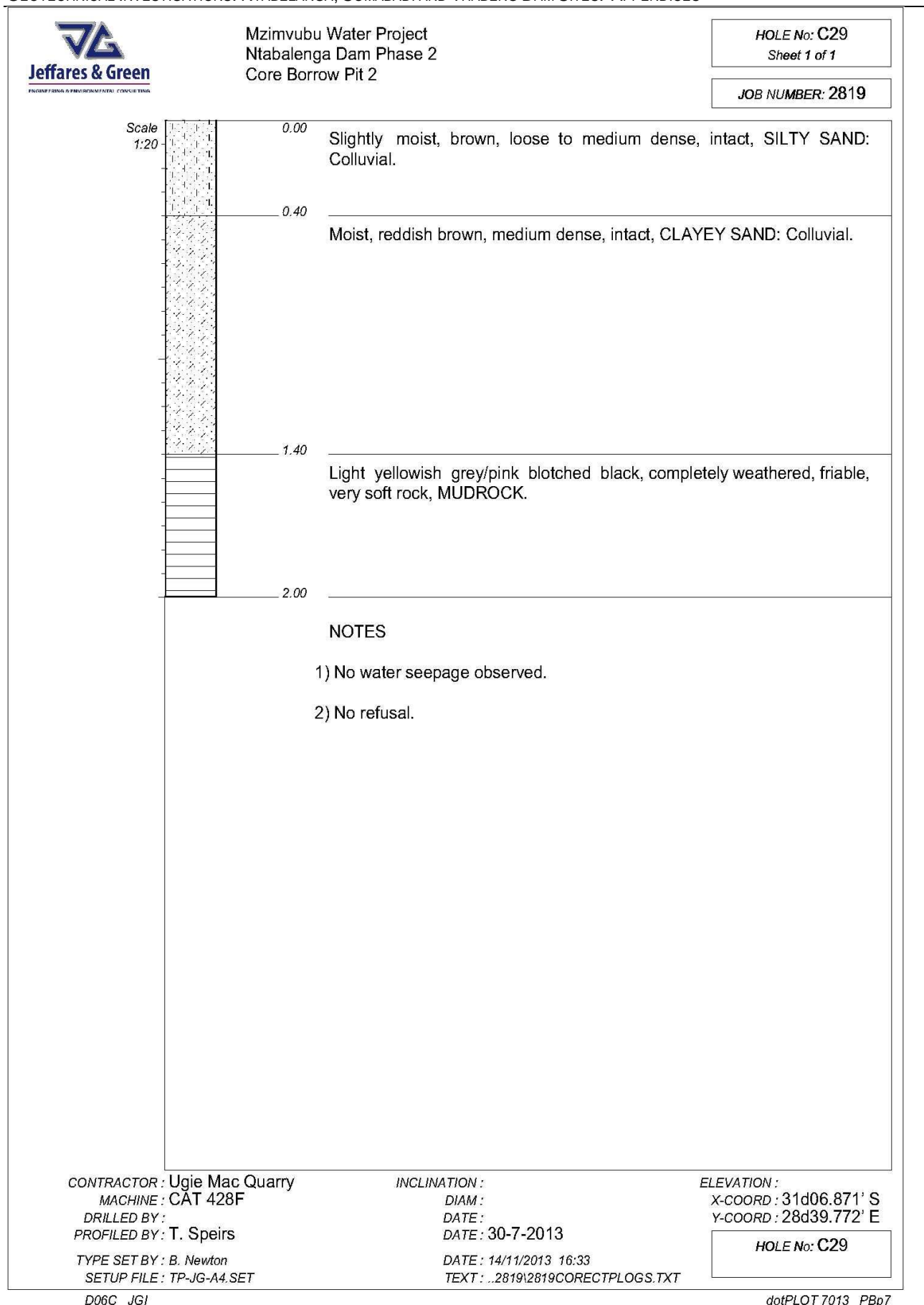


Fig G- 54: Core Borrow Pit 2 - Hole No: C29

G5:

SHELL BORROW PIT TRIAL PITS

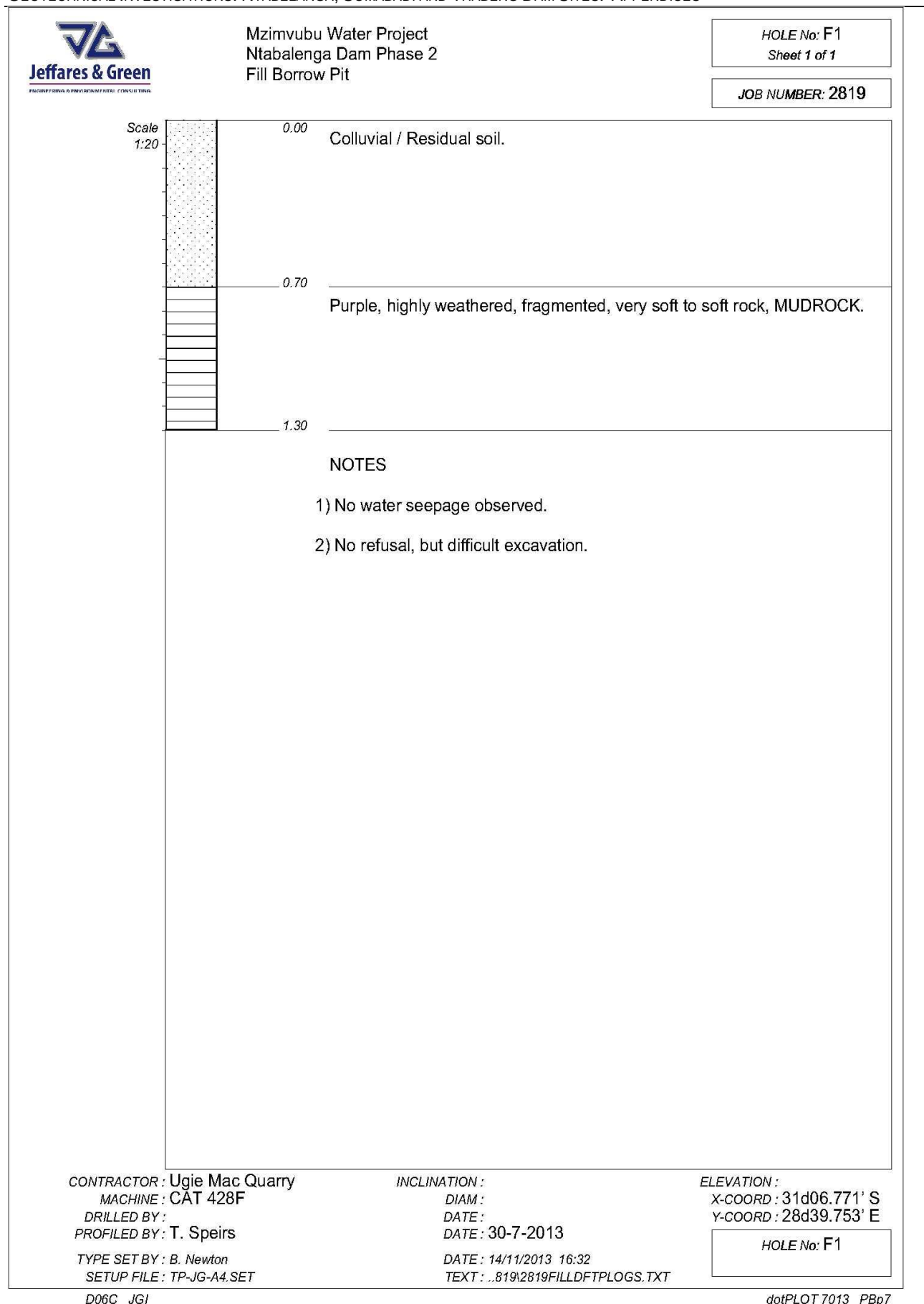


Fig G- 55: Fill Borrow Pit - Hole No: F1

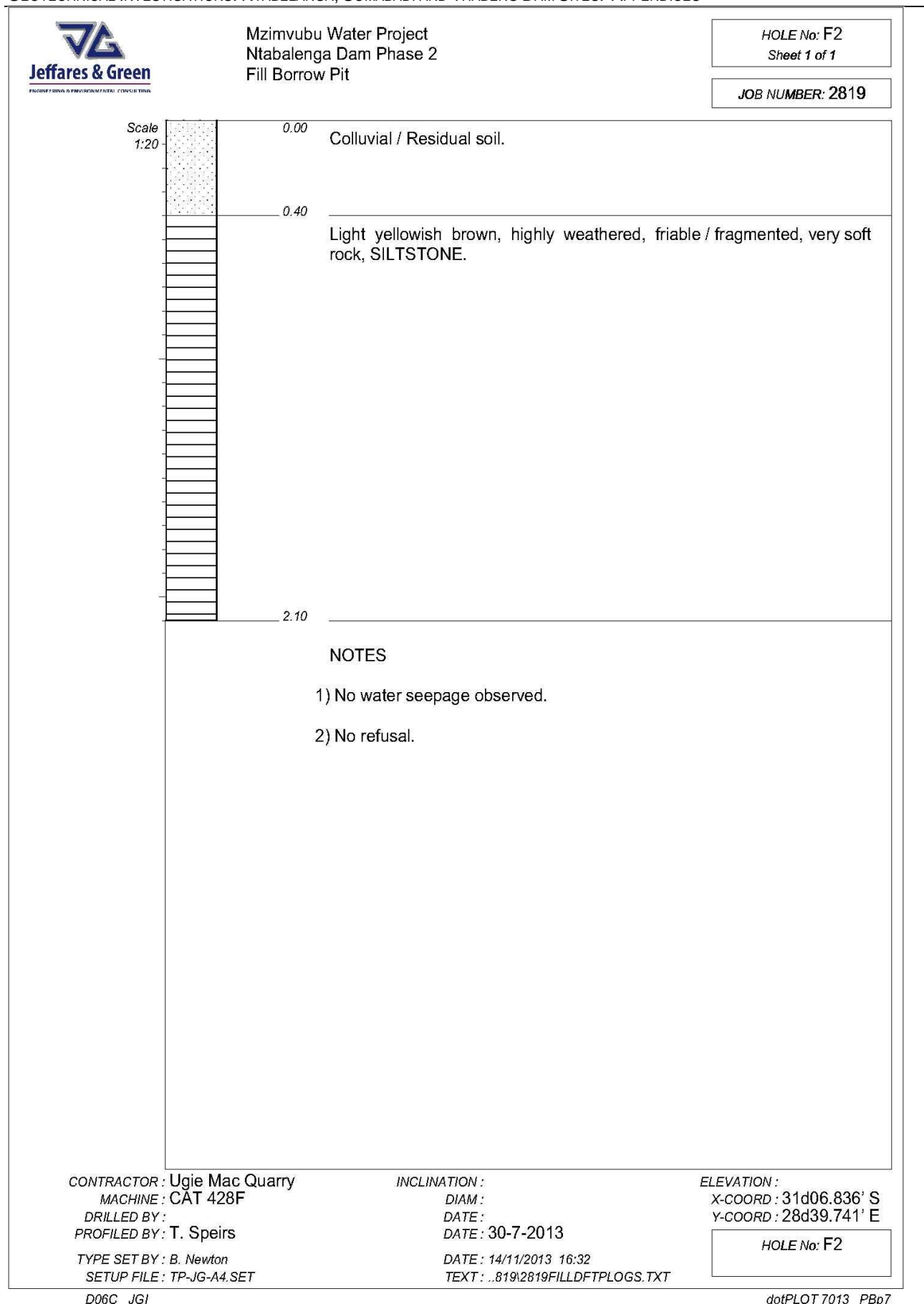


Fig G- 56: Fill Borrow Pit - Hole No: F2

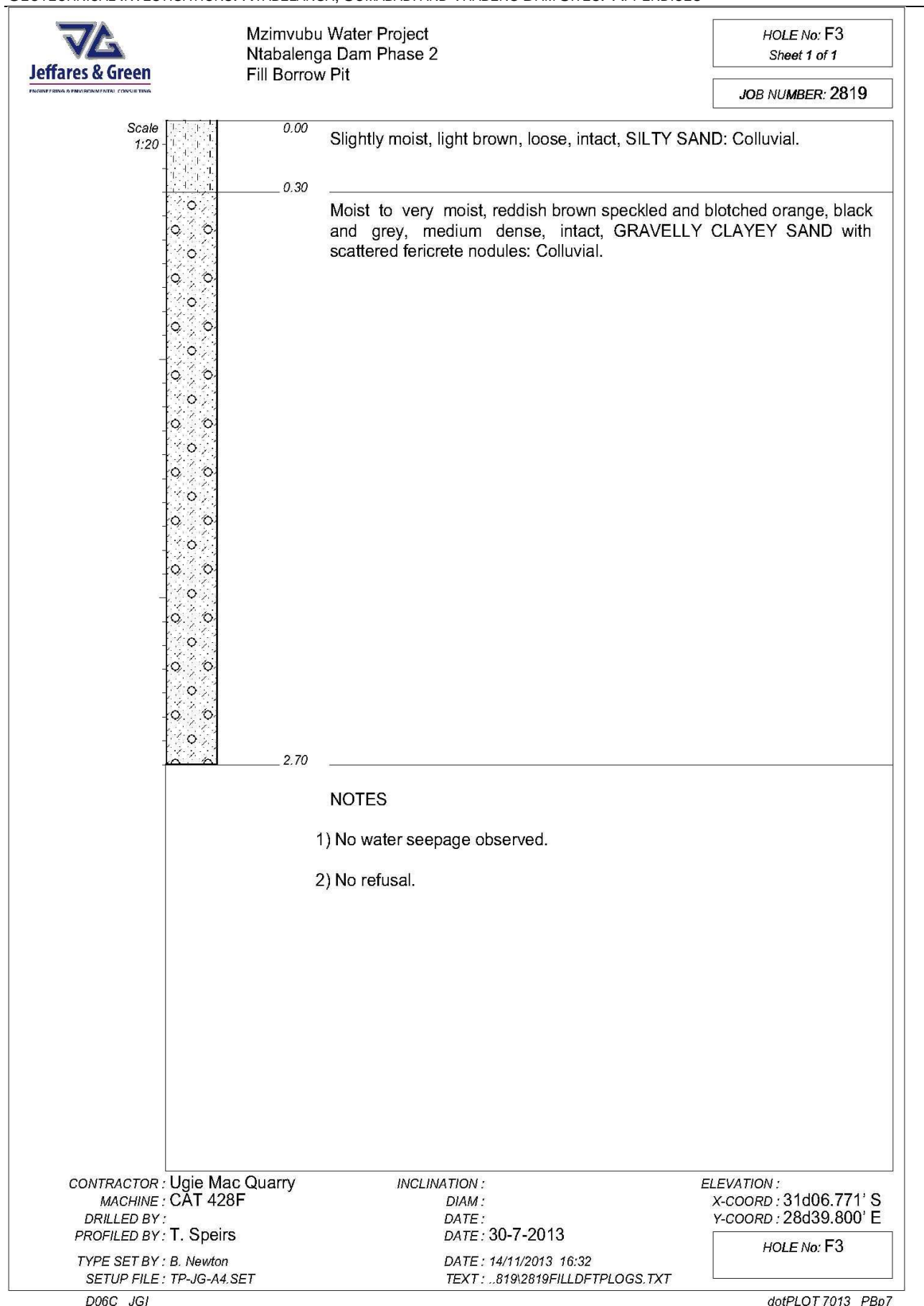


Fig G- 57: Fill Borrow Pit - Hole No: F3

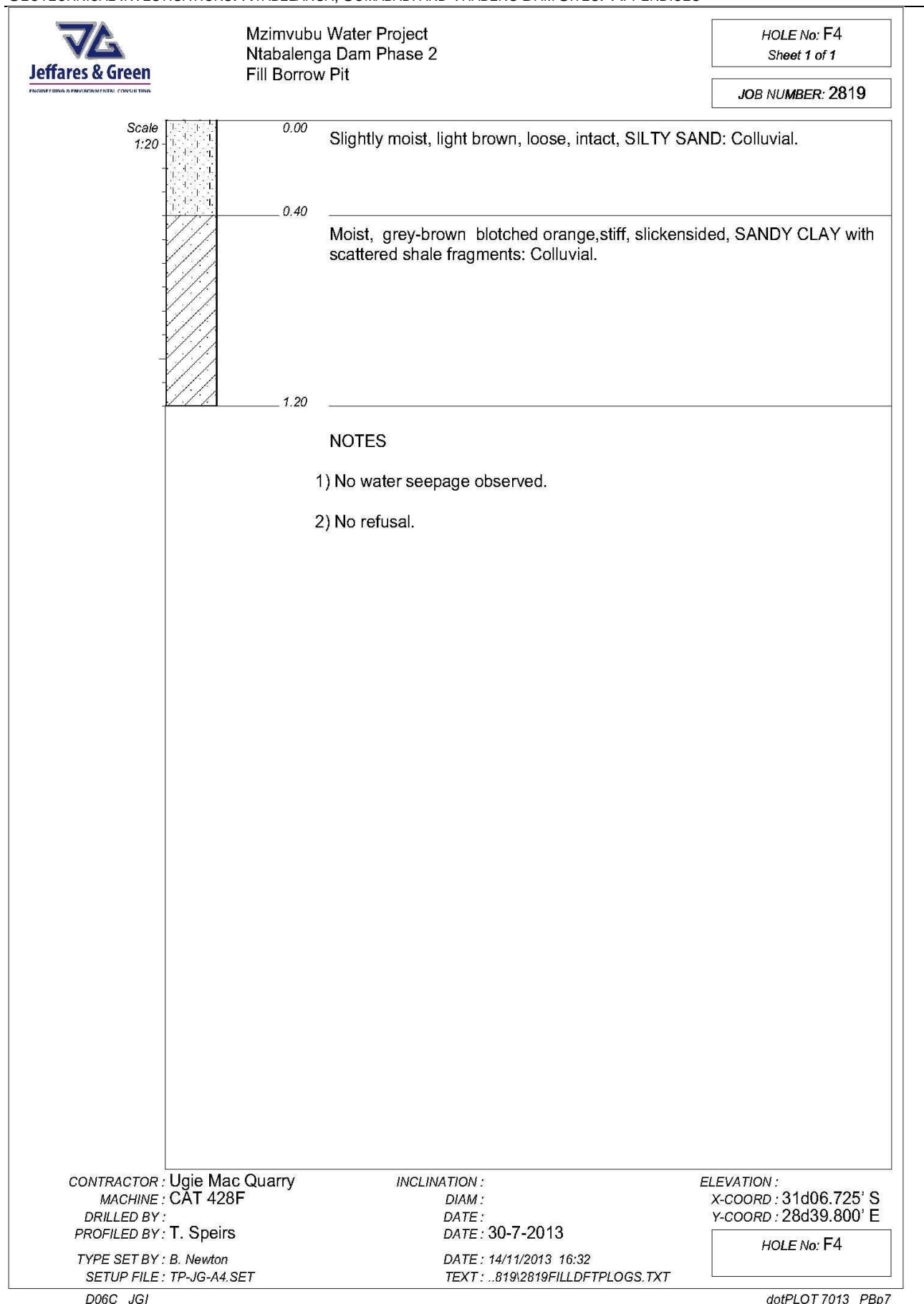


Fig G- 58: Fill Borrow Pit - Hole No: F4

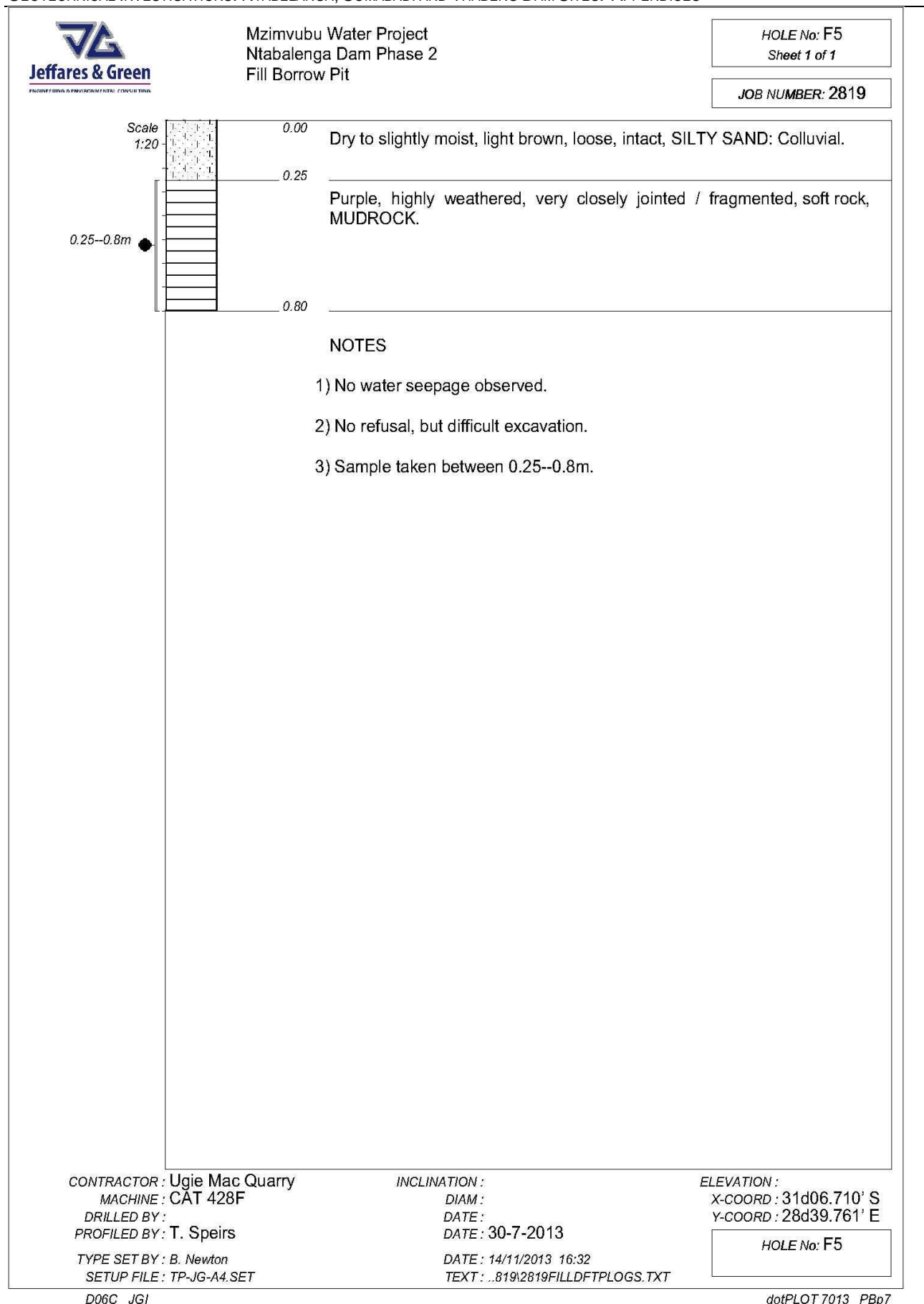


Fig G- 59: Fill Borrow Pit - Hole No: F5

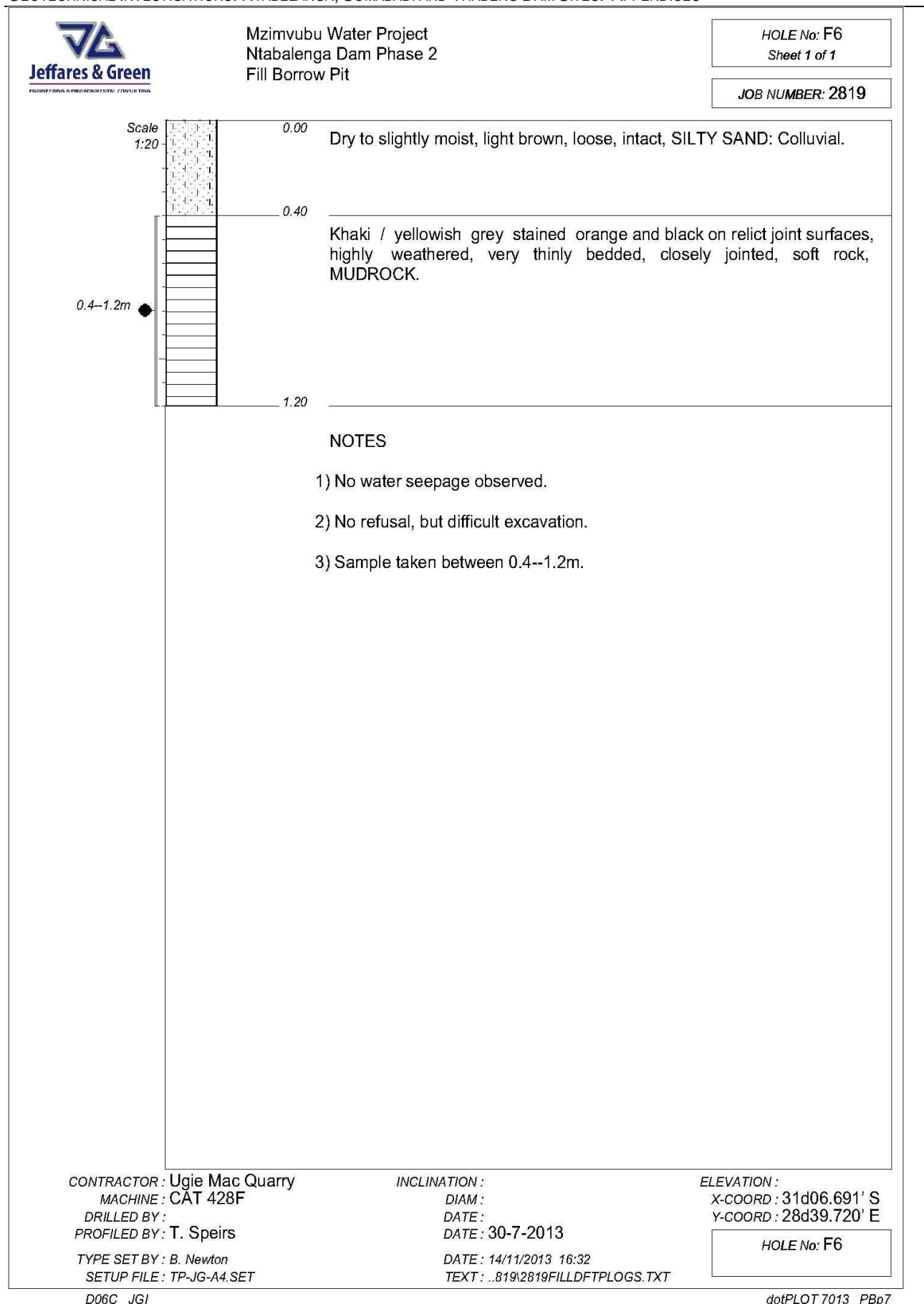


Fig G- 60: Fill Borrow Pit - Hole No: F6

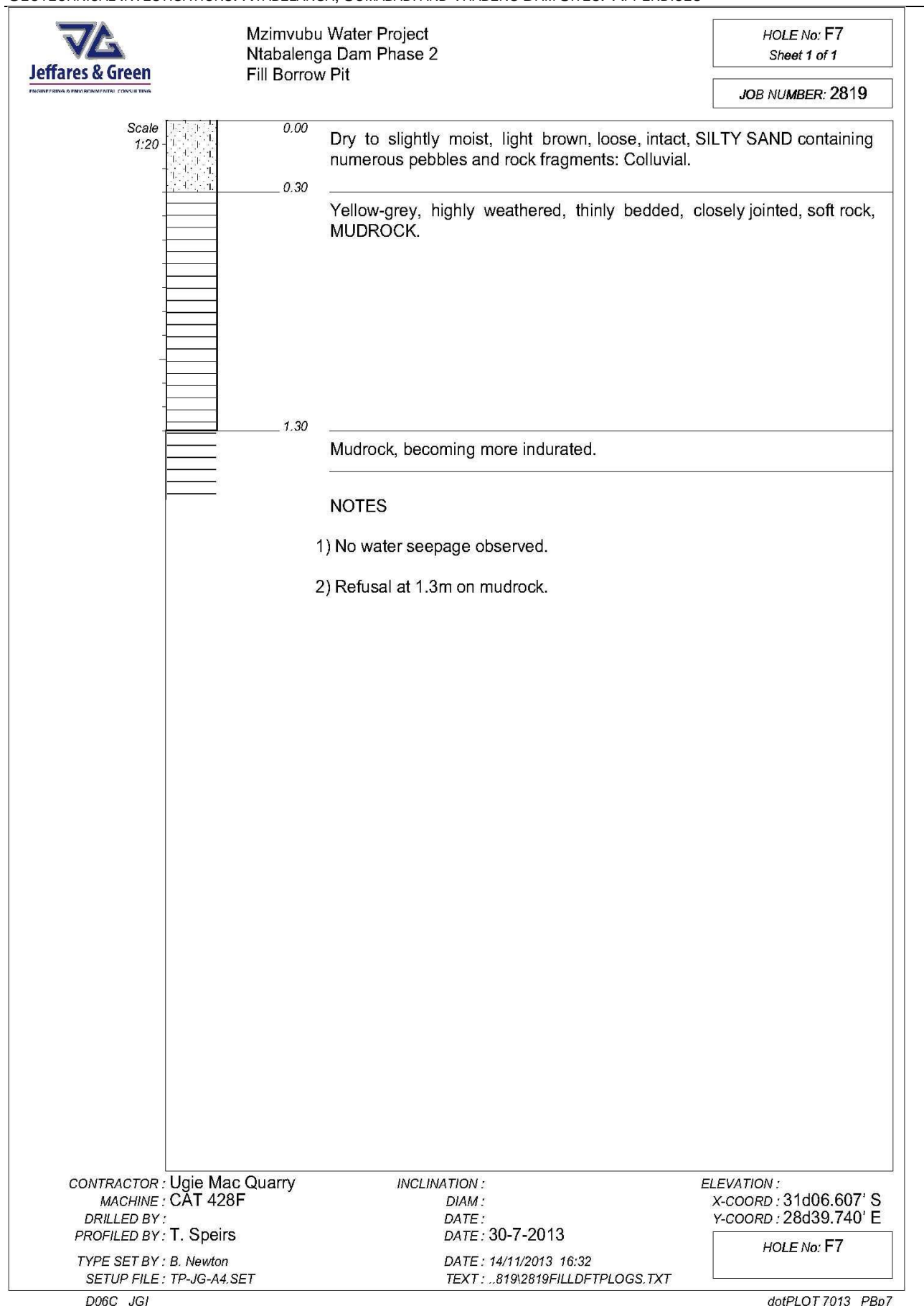


Fig G- 61: Fill Borrow Pit - Hole No: F7

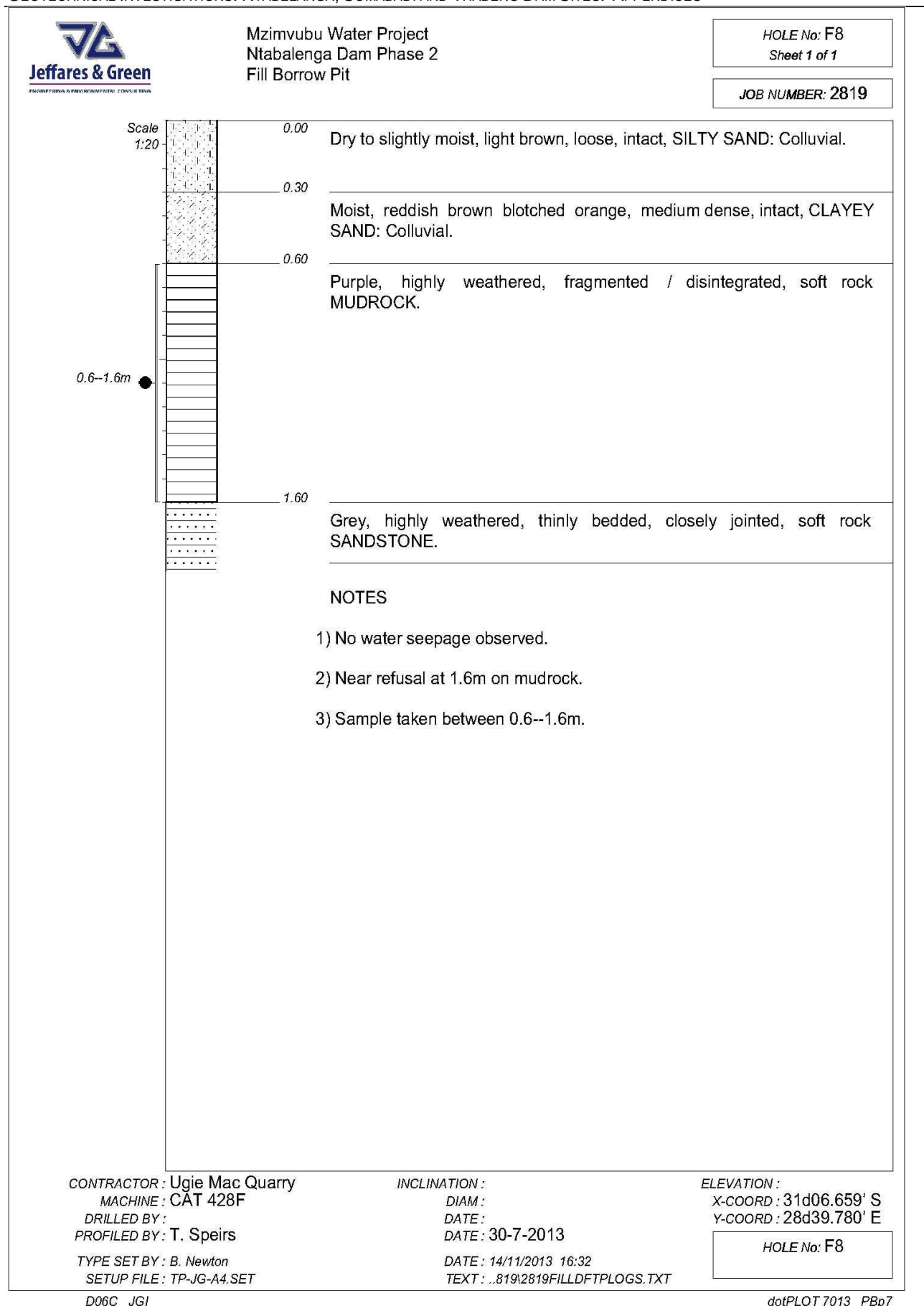


Fig G- 62: Fill Borrow Pit - Hole No: F8

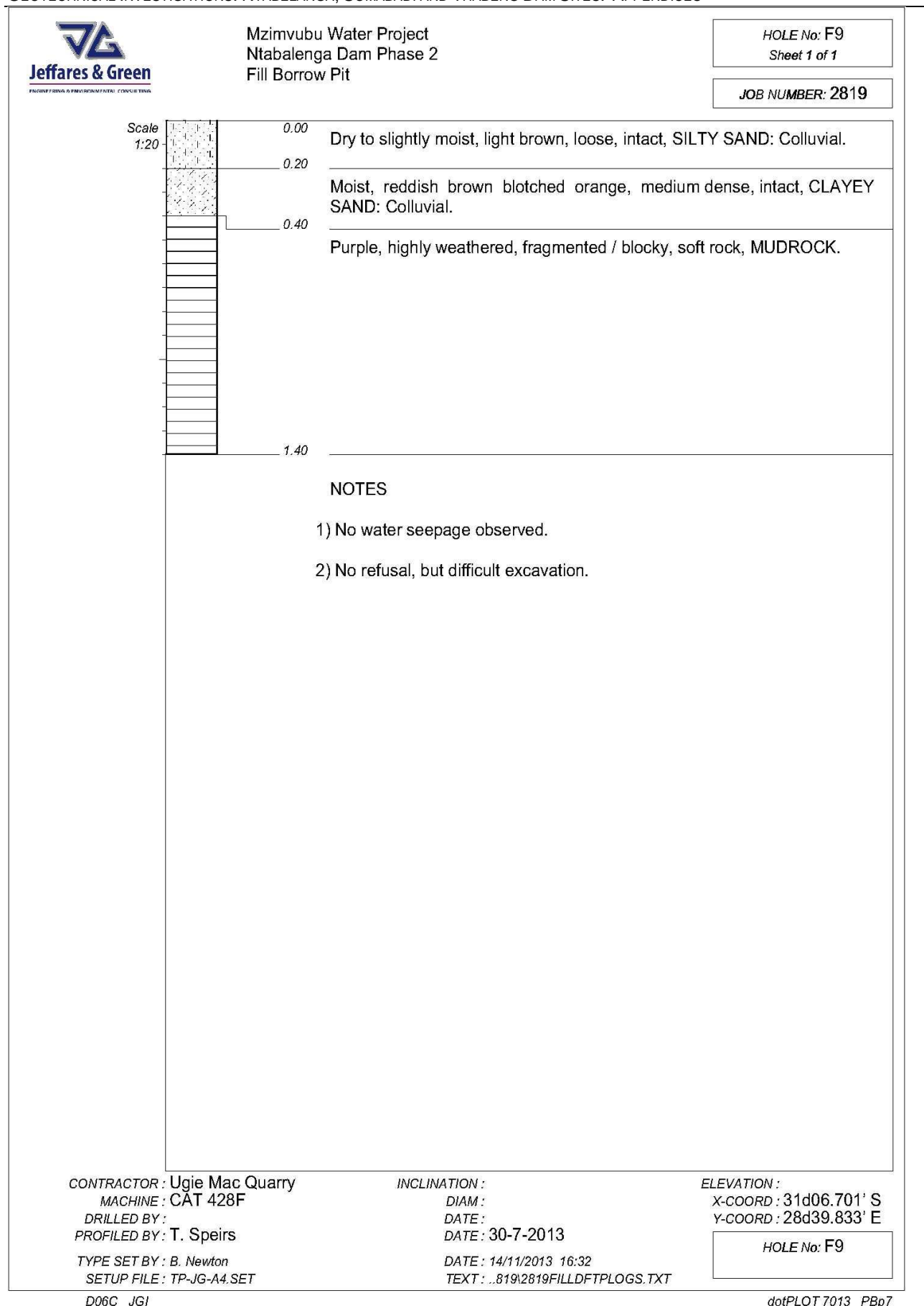


Fig G- 63: Fill Borrow Pit - Hole No: F9

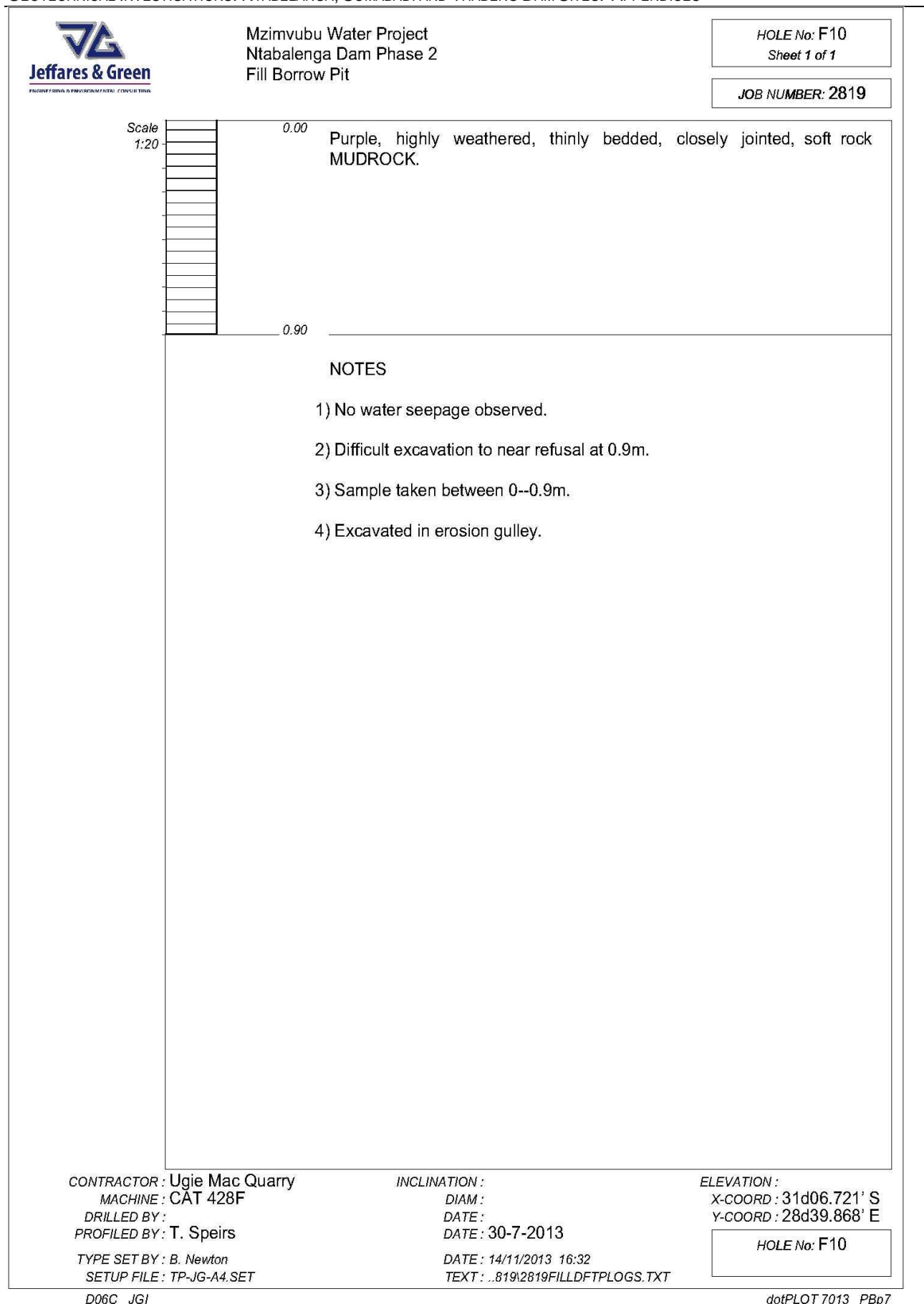


Fig G- 64: Fill Borrow Pit - Hole No: F10

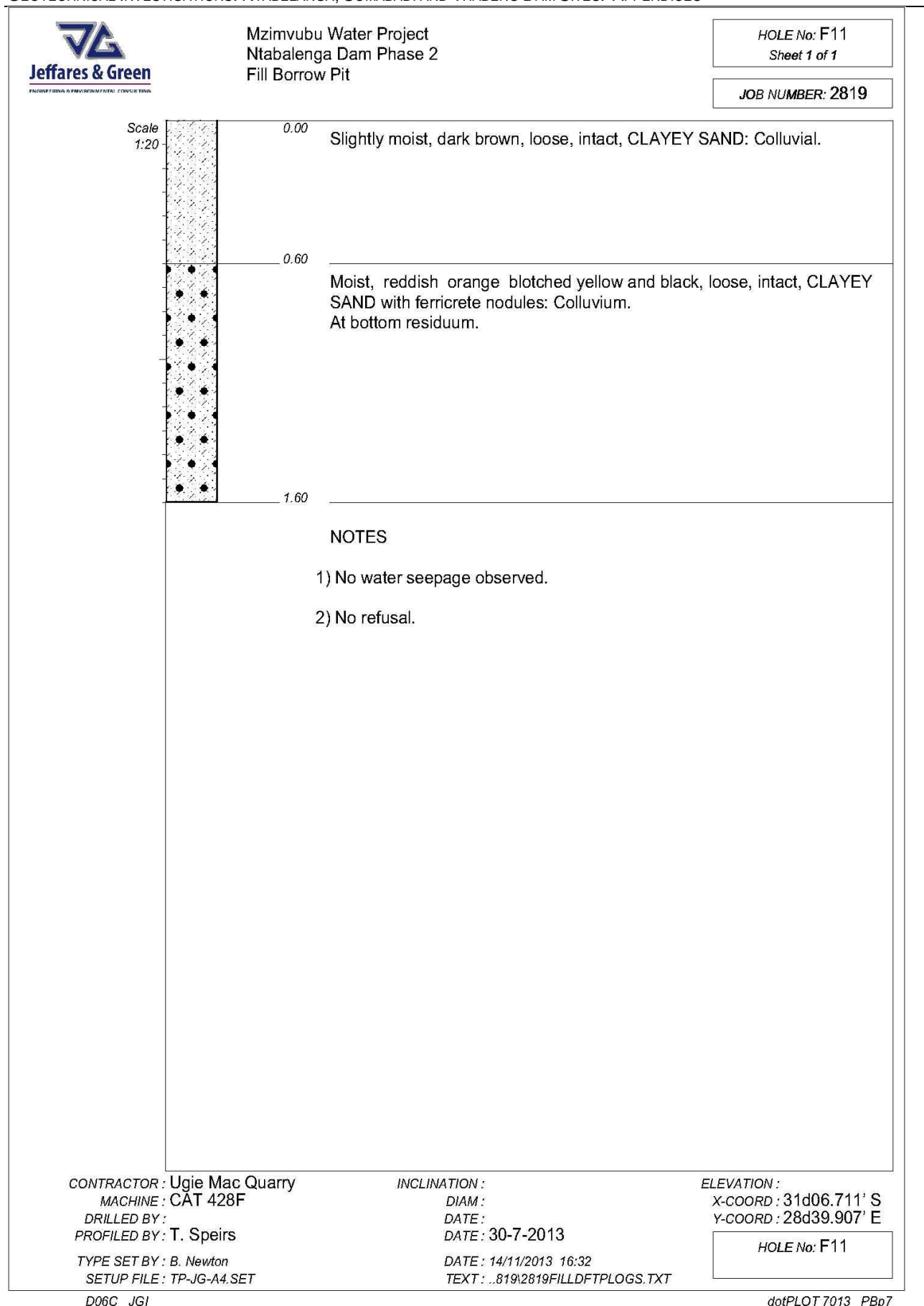


Fig G- 65: Fill Borrow Pit - Hole No: F11

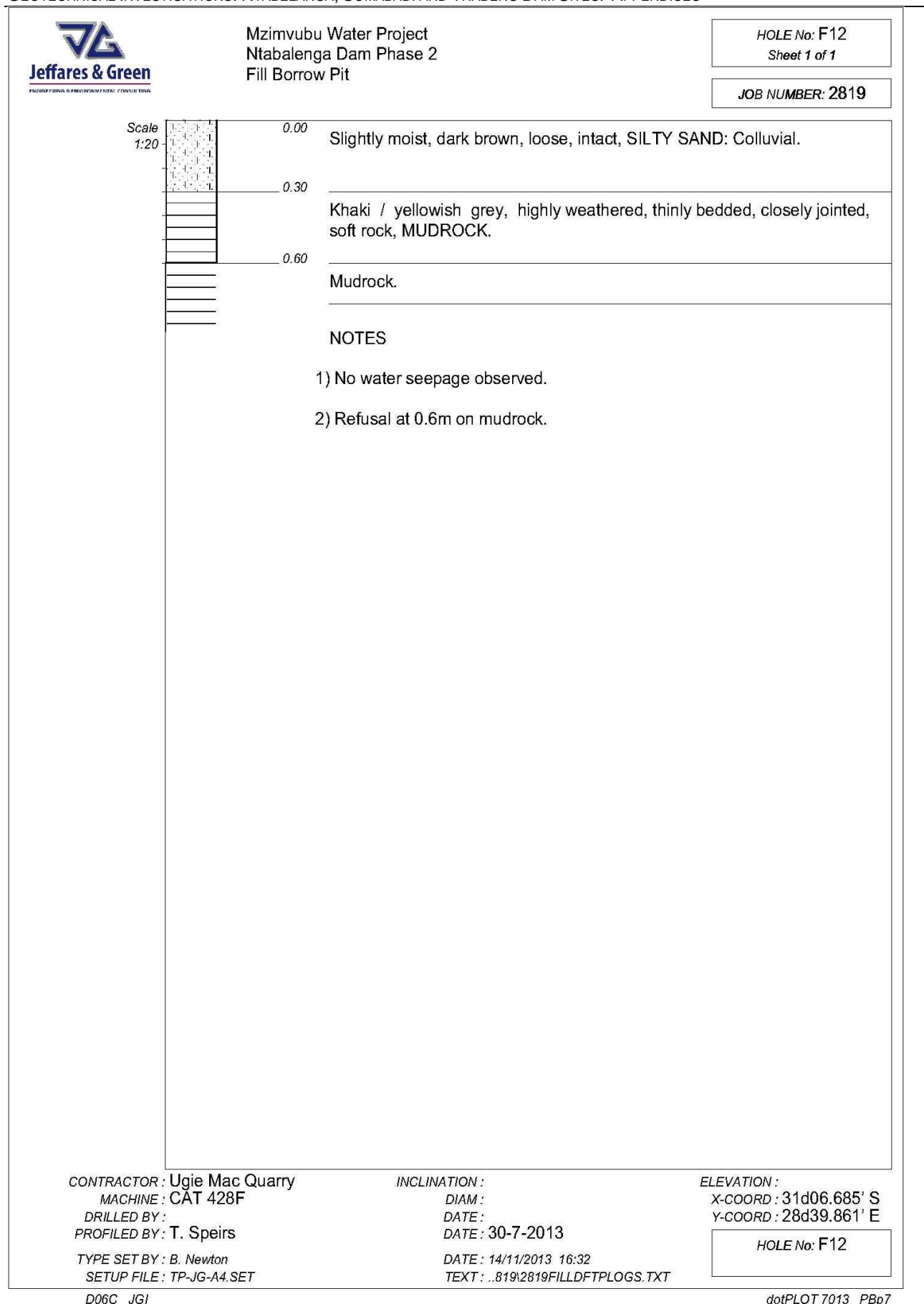


Fig G- 66: Fill Borrow Pit - Hole No: F12

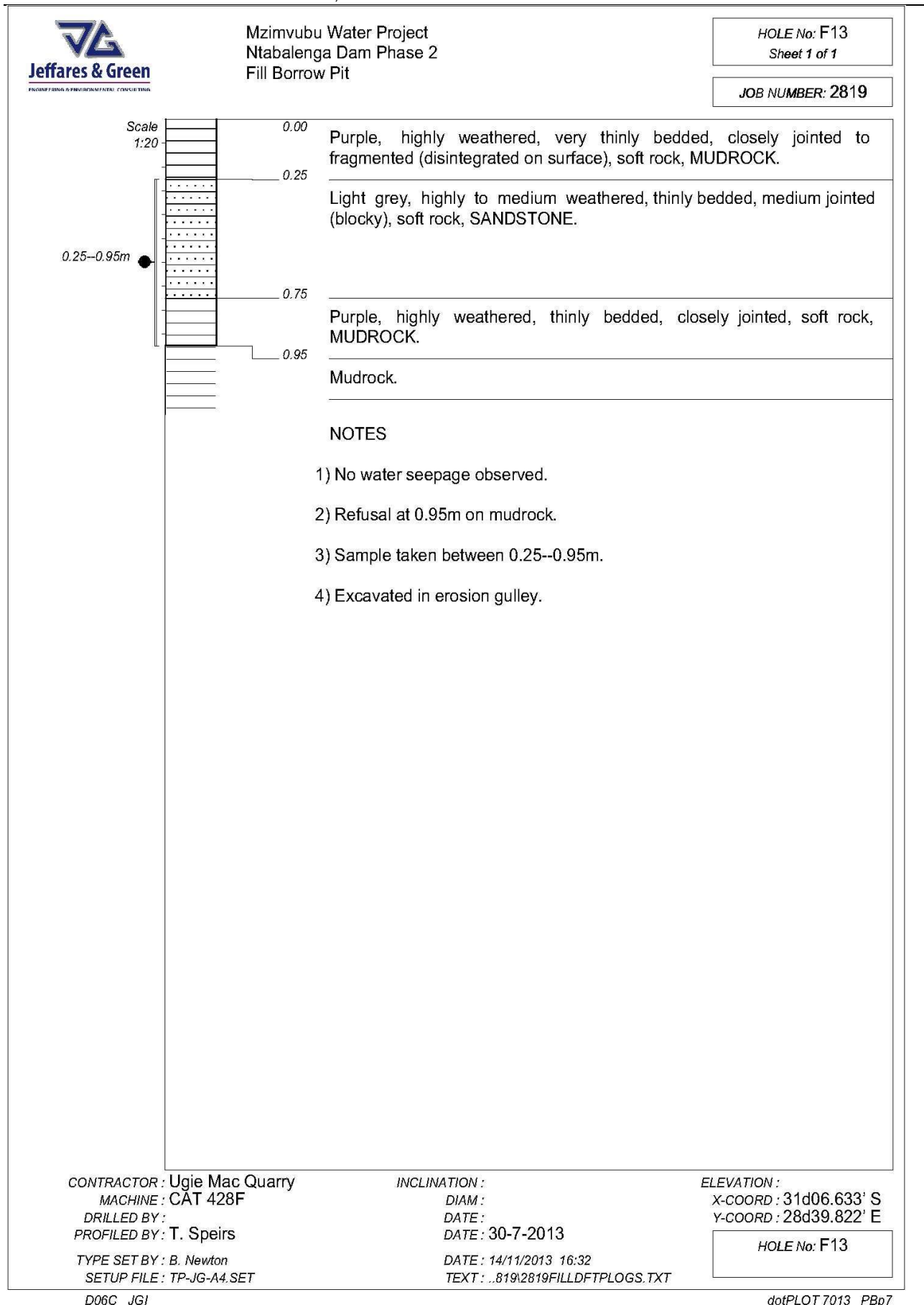


Fig G- 67: Fill Borrow Pit - Hole No: F13

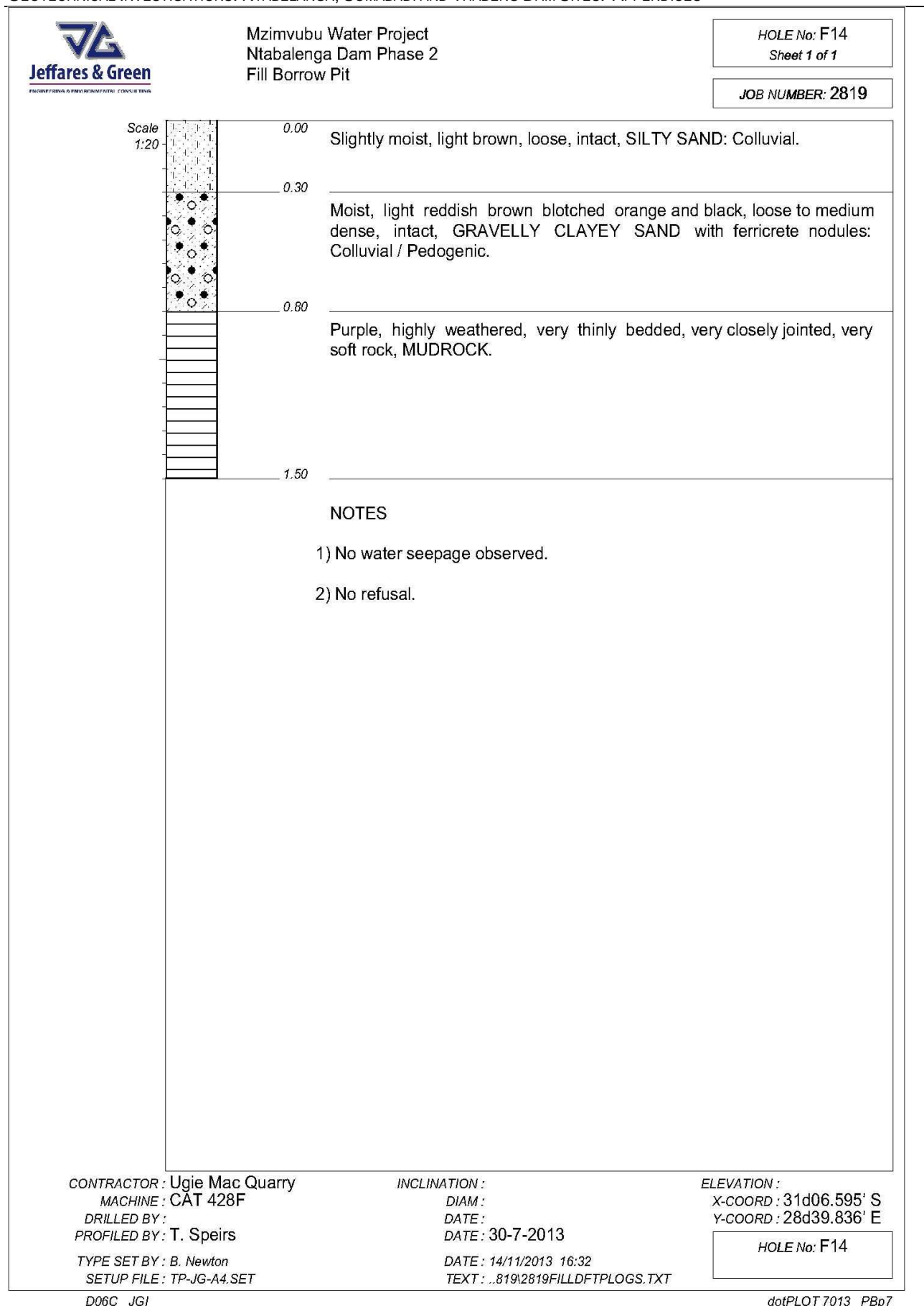
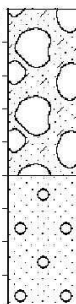


Fig G- 68: Fill Borrow Pit - Hole No: F14

HOLE No: F15
Sheet 1 of 1

Scale
1:20



Dry, dark brown, loose, intact, CLAYEY SAND with numerous dolerite boulders: Colluvium.

Slightly moist, light yellowish brown, loose, intact, GRAVELLY SAND with numerous dolerite cobbles.

NOTES

- 1) No water seepage observed.
- 2) Refusal at 0.9m on boulder / bedrock.
- 3) No sidewall collapse.
- 4) Not sampled.

ELEVATION :
X-COORD : 31d06.246' S
Y-COORD : 28d38.521' E

DATE: 14/11/2013 16:32
TEXT: ..819\2819FILLDFTPLOGS.TXT

HOLE No: F15

dotPLOT7013 PBp7

G - 80

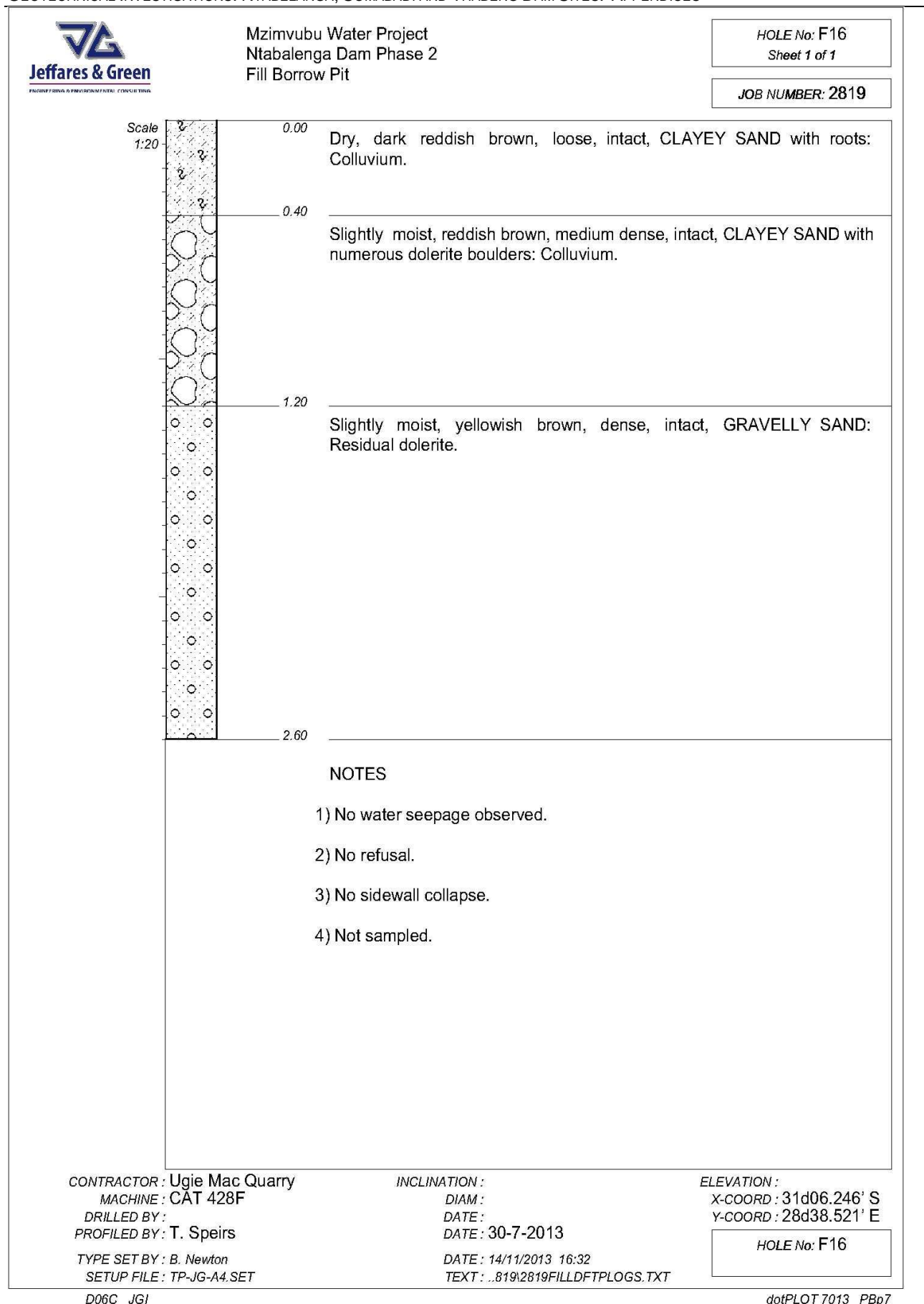


Fig G- 70: Fill Borrow Pit - Hole No: F16

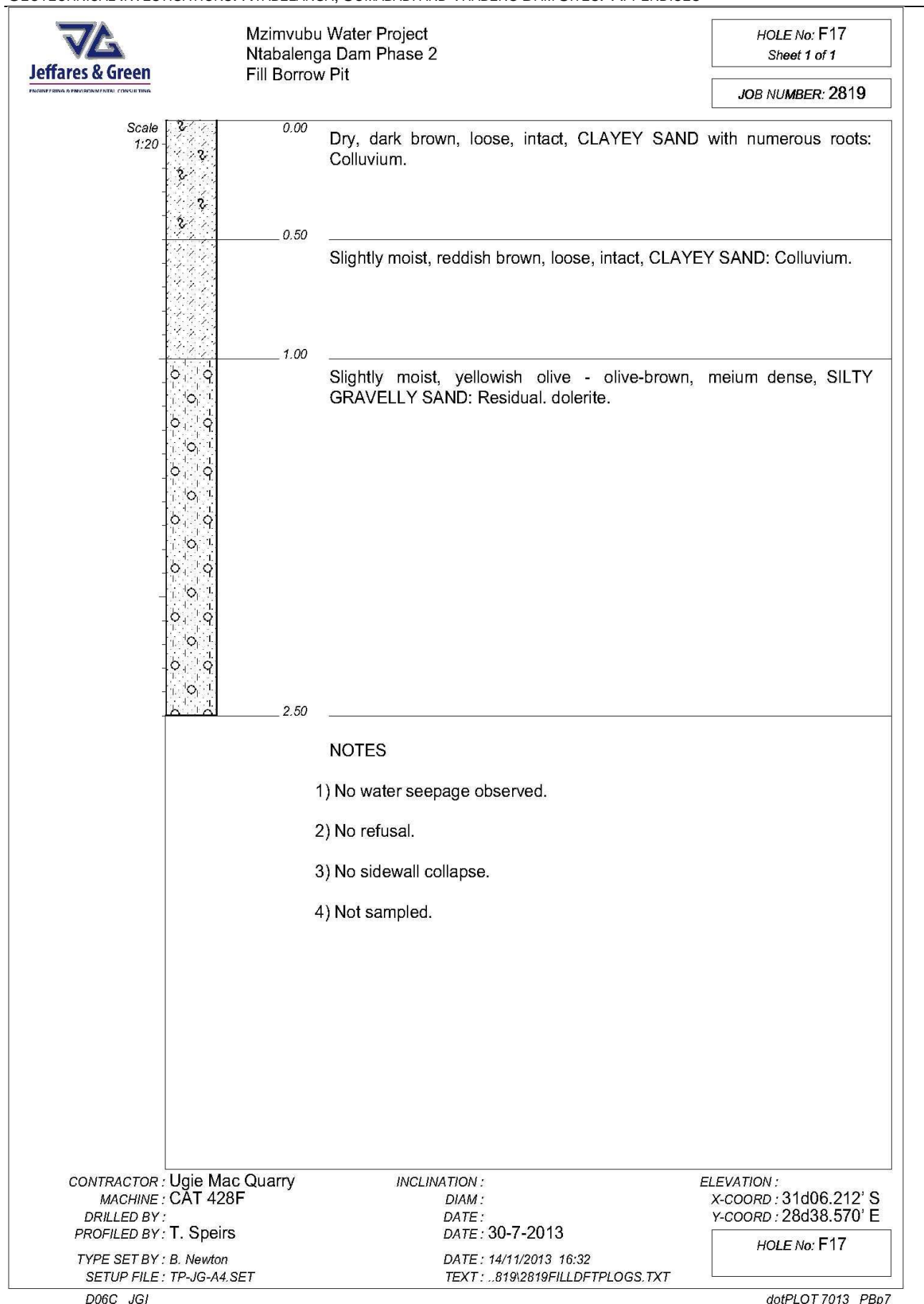


Fig G- 71: Fill Borrow Pit - Hole No: F17

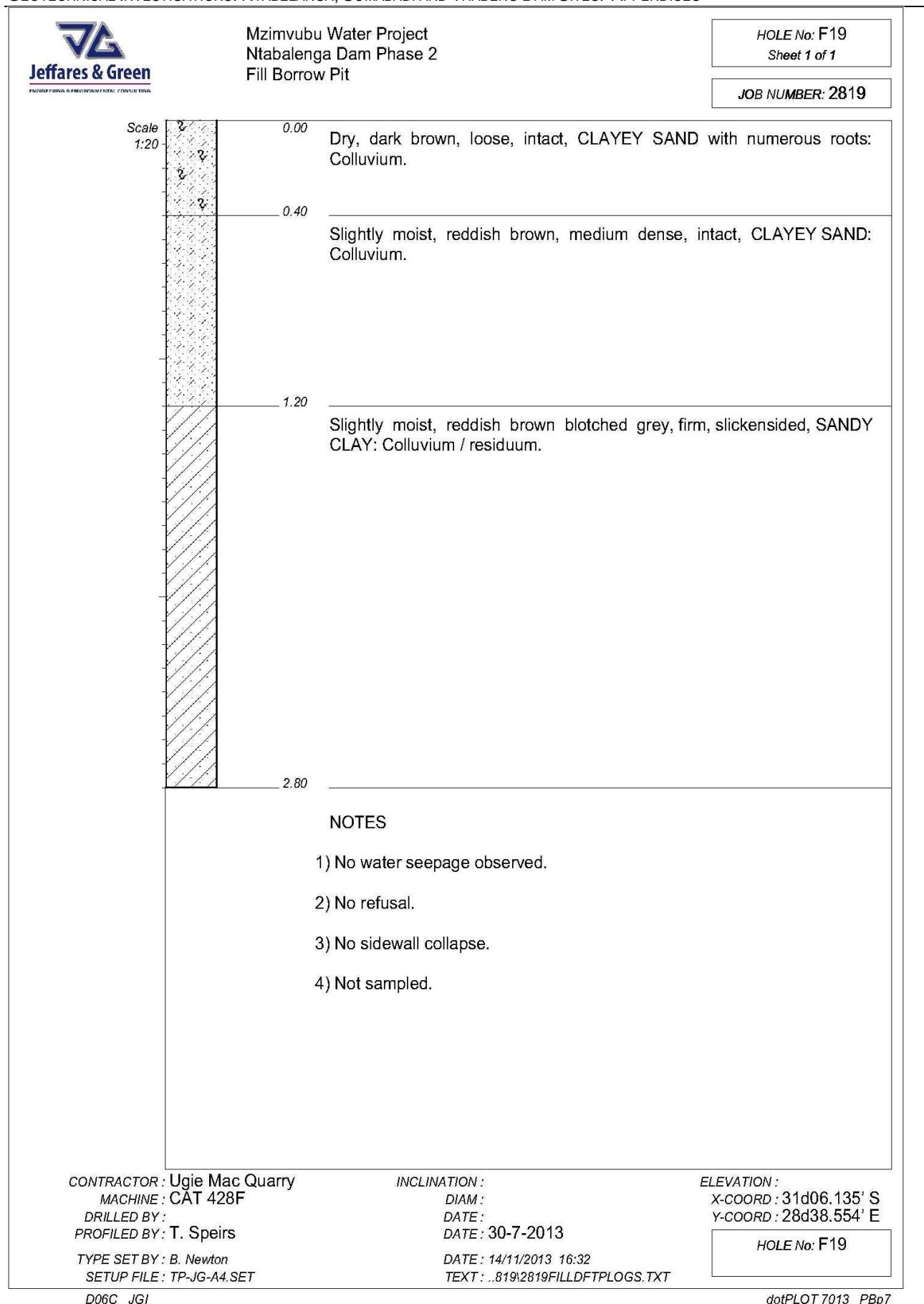


Fig G- 73: Fill Borrow Pit - Hole No: F19

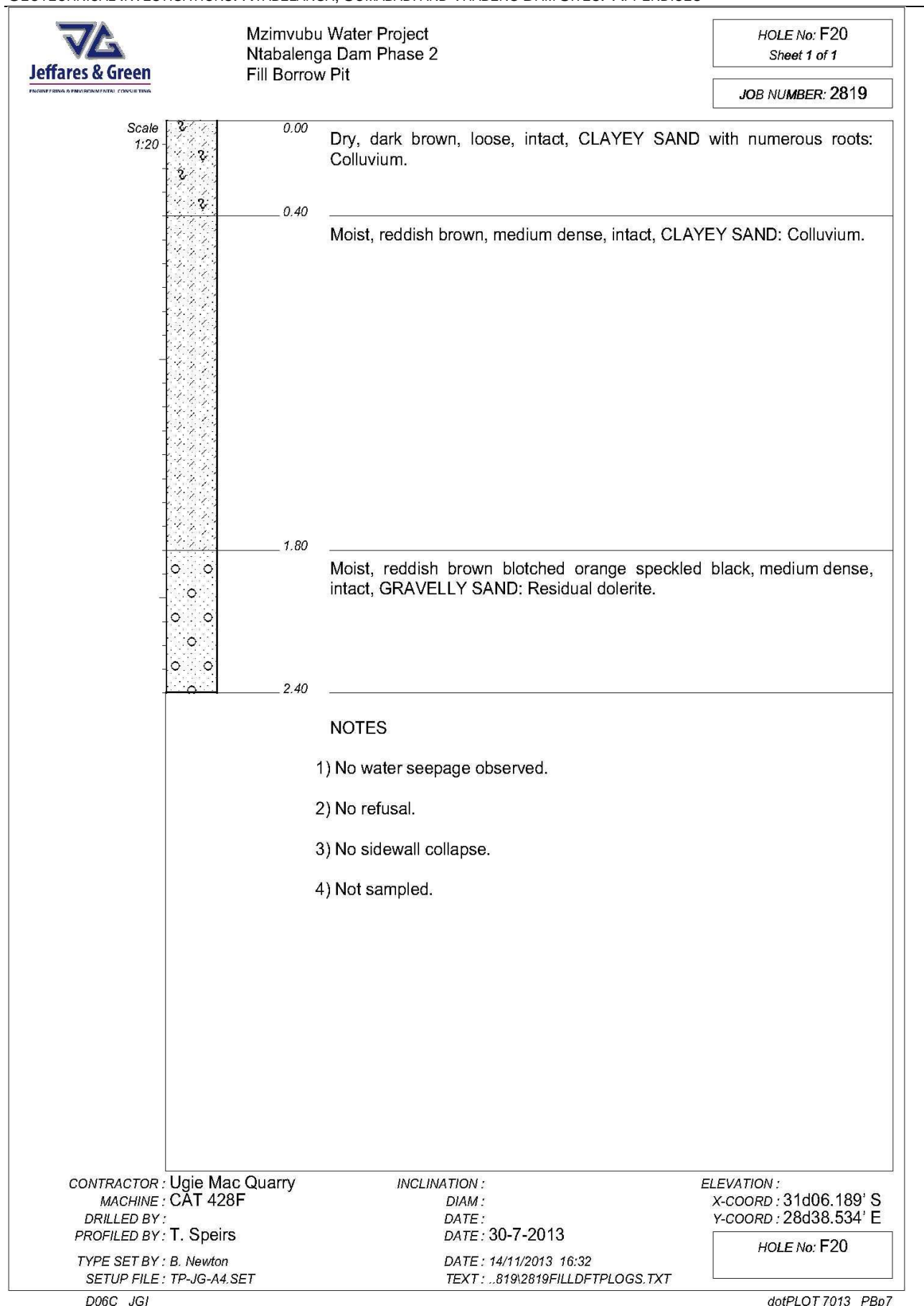


Fig G- 74: Fill Borrow Pit - Hole No: F20

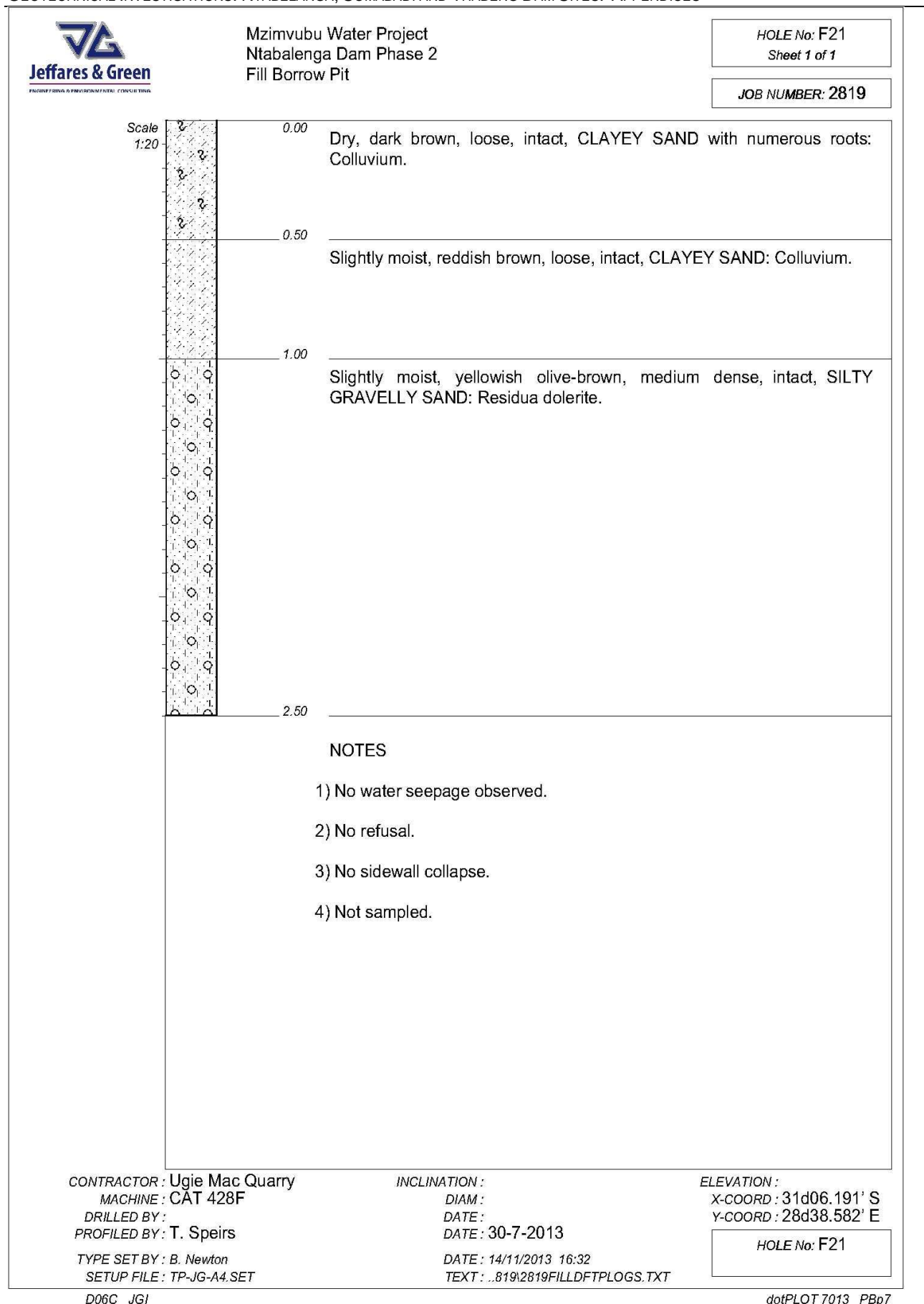


Fig G- 75: Fill Borrow Pit - Hole No: F21

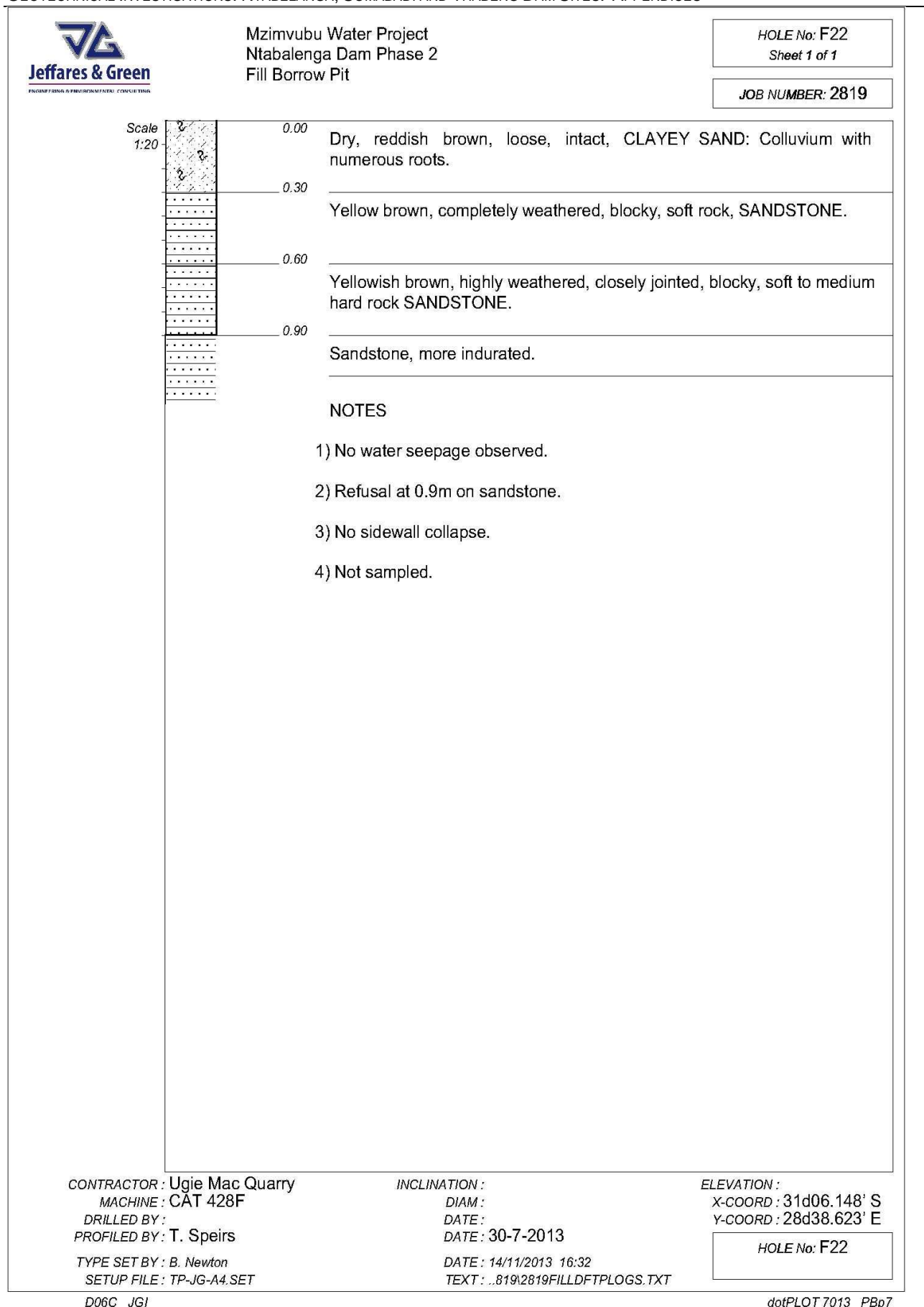


Fig G- 76: Fill Borrow Pit - Hole No: F22

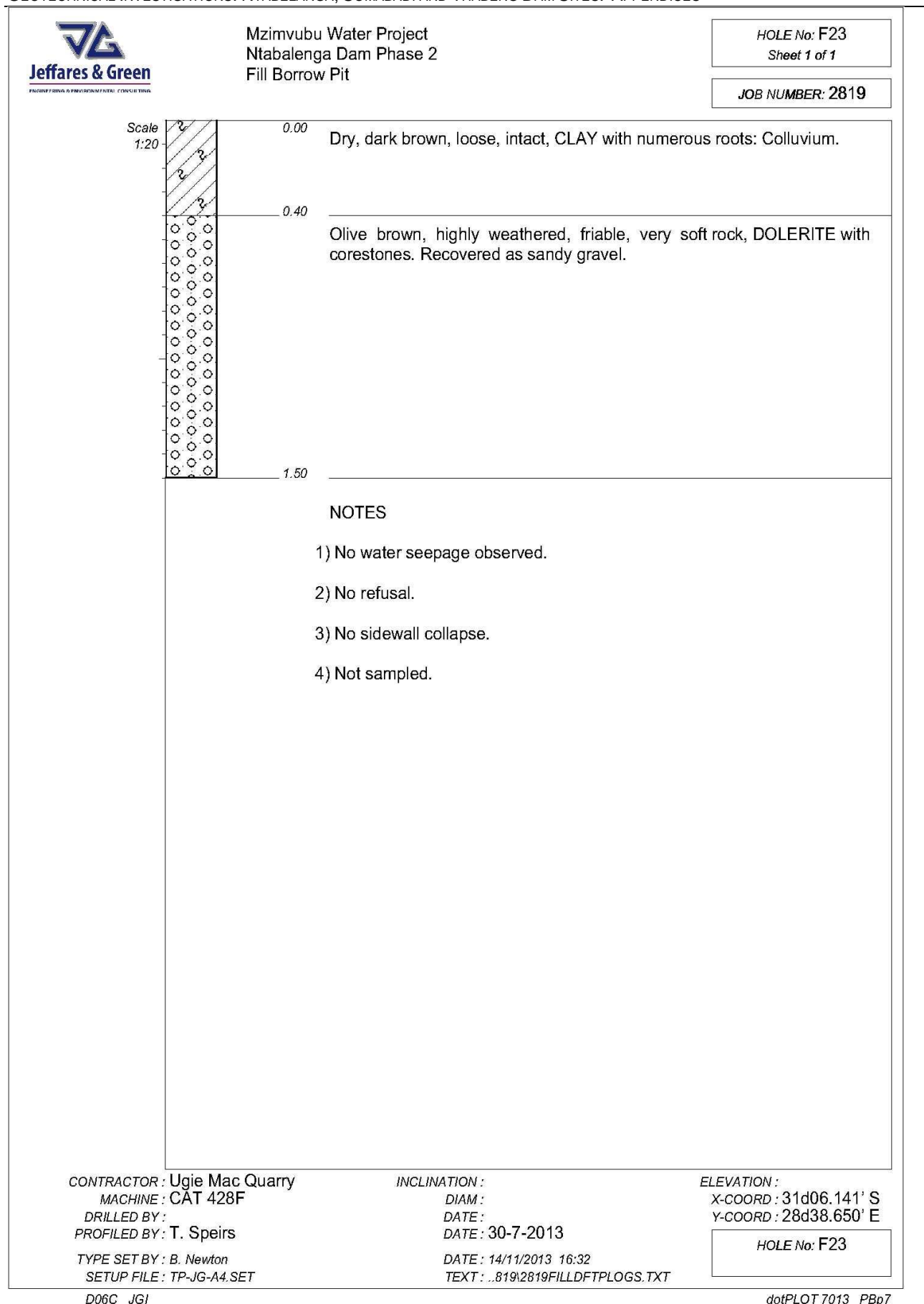


Fig G- 77: Fill Borrow Pit - Hole No: F23

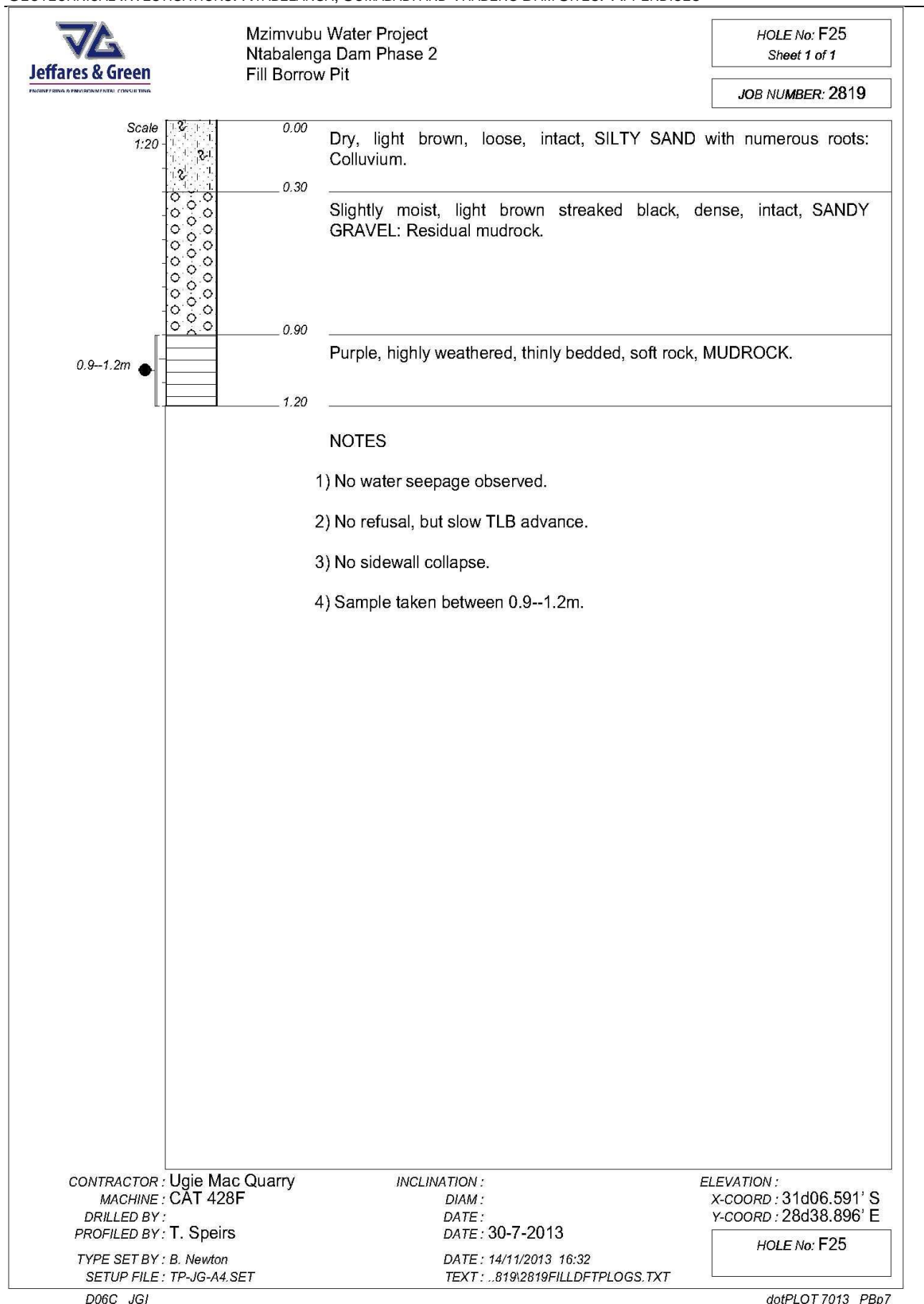


Fig G- 78: Fill Borrow Pit - Hole No: F25

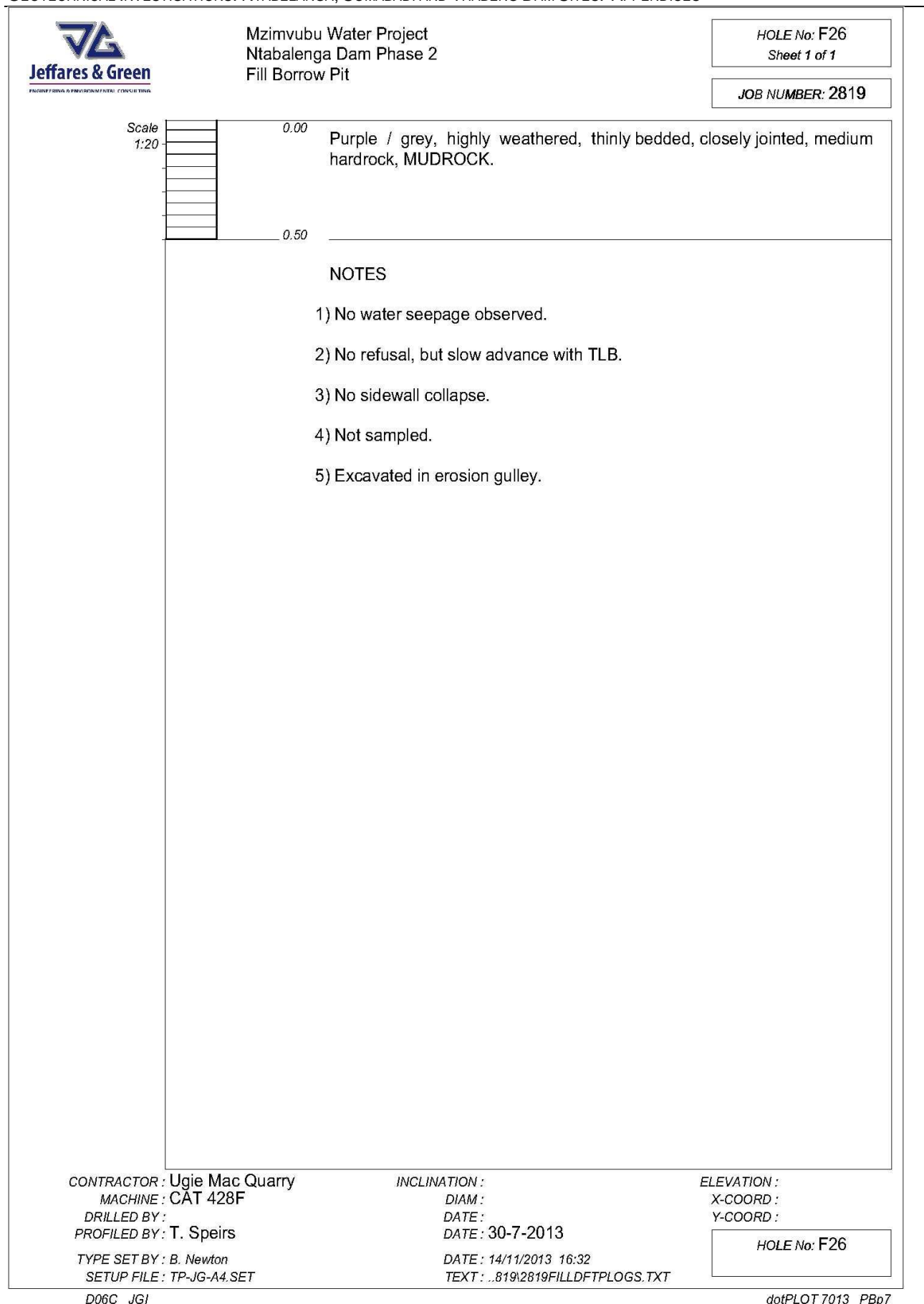


Fig G- 79: Fill Borrow Pit - Hole No: F26

HOLE No: F27
Sheet 1 of 1

	0.00	Dry, light brown, loose, intact, SILTY SAND with numerous roots: Colluvium.
	0.40	Slightly moist, light brown blotched orange and black, GRAVELLY SAND: Residual mudrock / sandstone.
	1.00	Light brown blotched orange and black, completely weathered, closely jointed, thinly bedded, very soft rock, fine silty SANDSTONE.

- 1) No water seepage observed.
- 2) No refusal, but slow advance with TLB.
- 3) No sidewall collapse.
- 4) Not sampled.

HOLE No: F27

dotPLOT7013 PBp7

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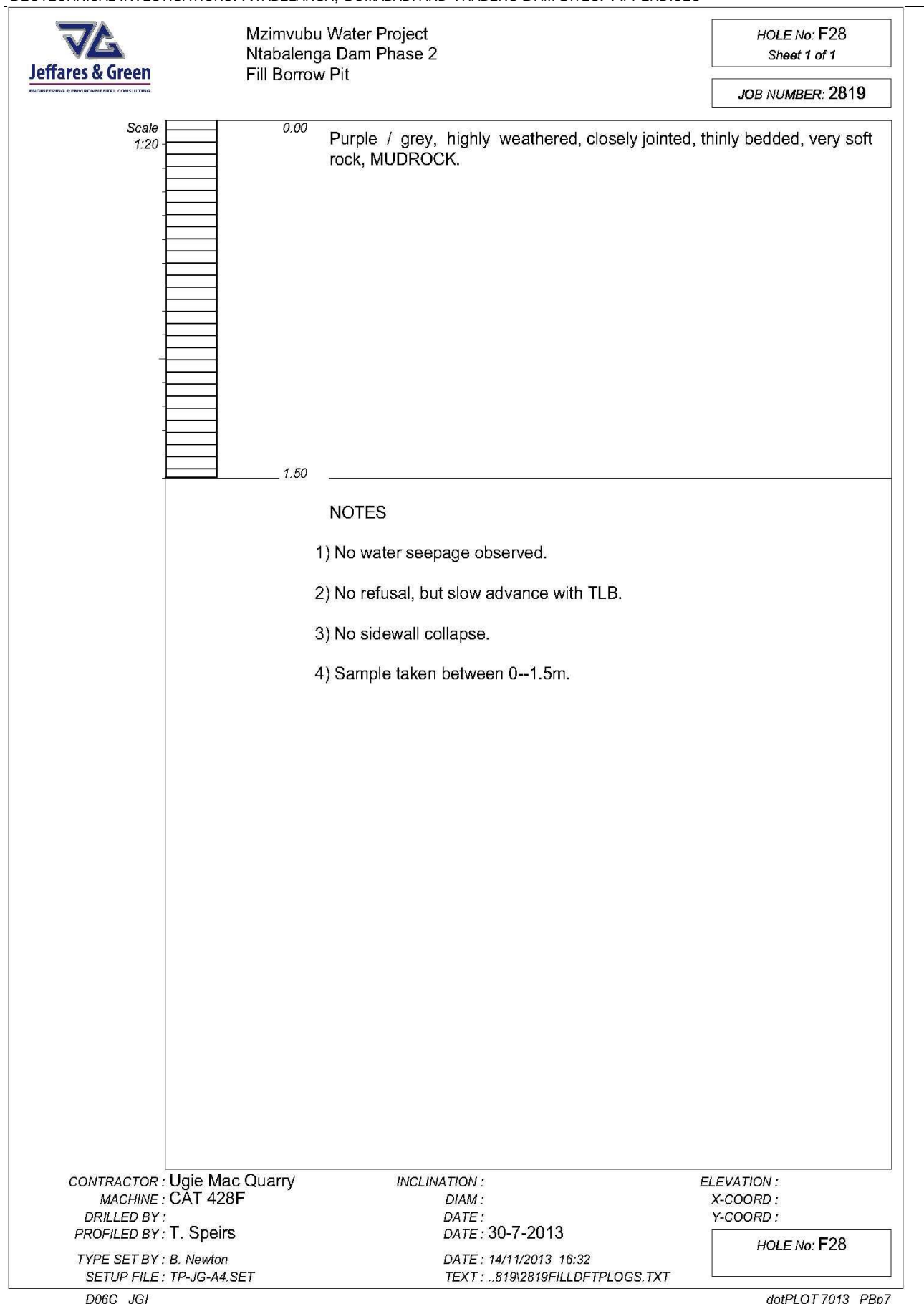


Fig G- 81: Fill Borrow Pit - Hole No: F28

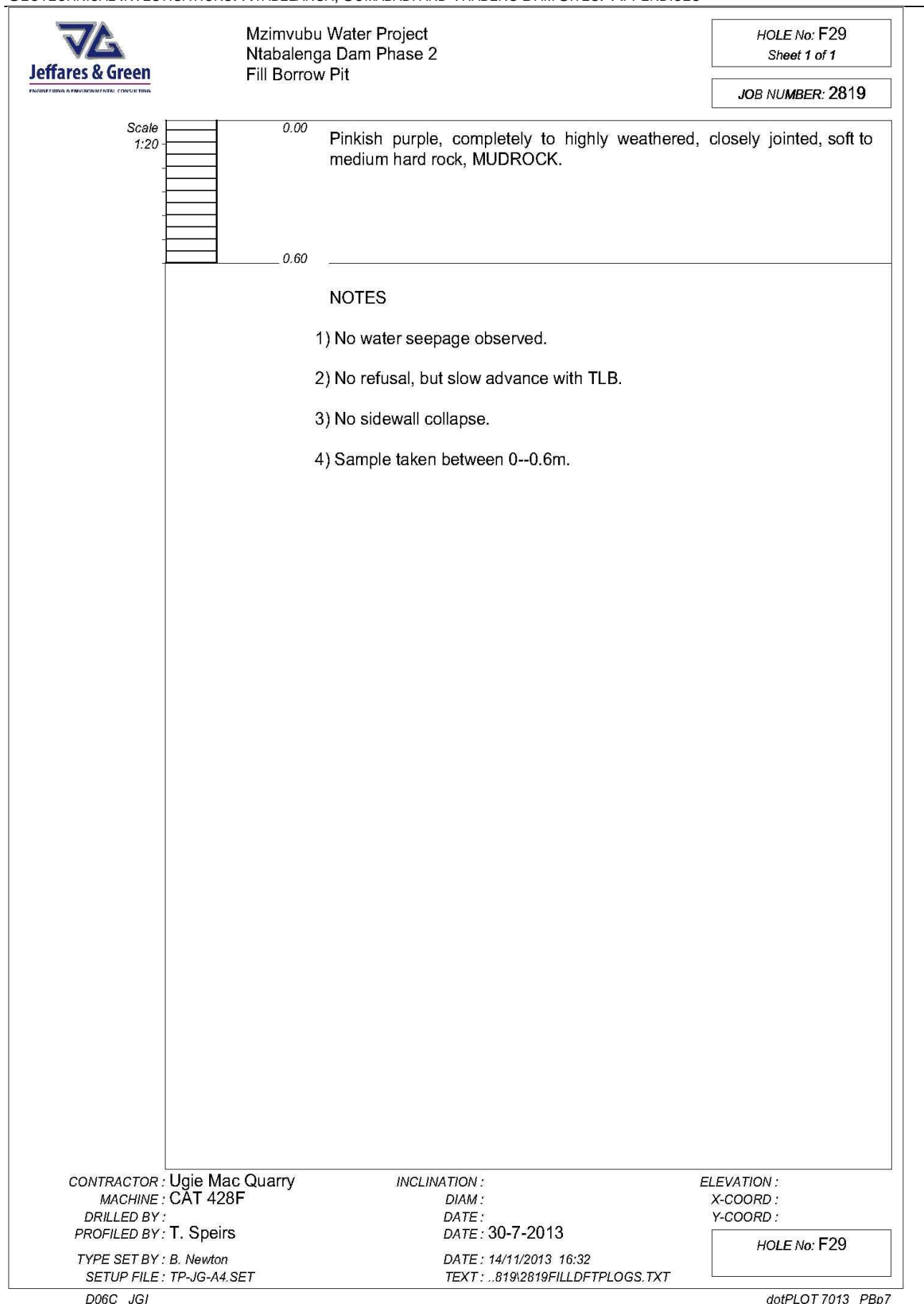


Fig G- 82: Fill Borrow Pit - Hole No: F29

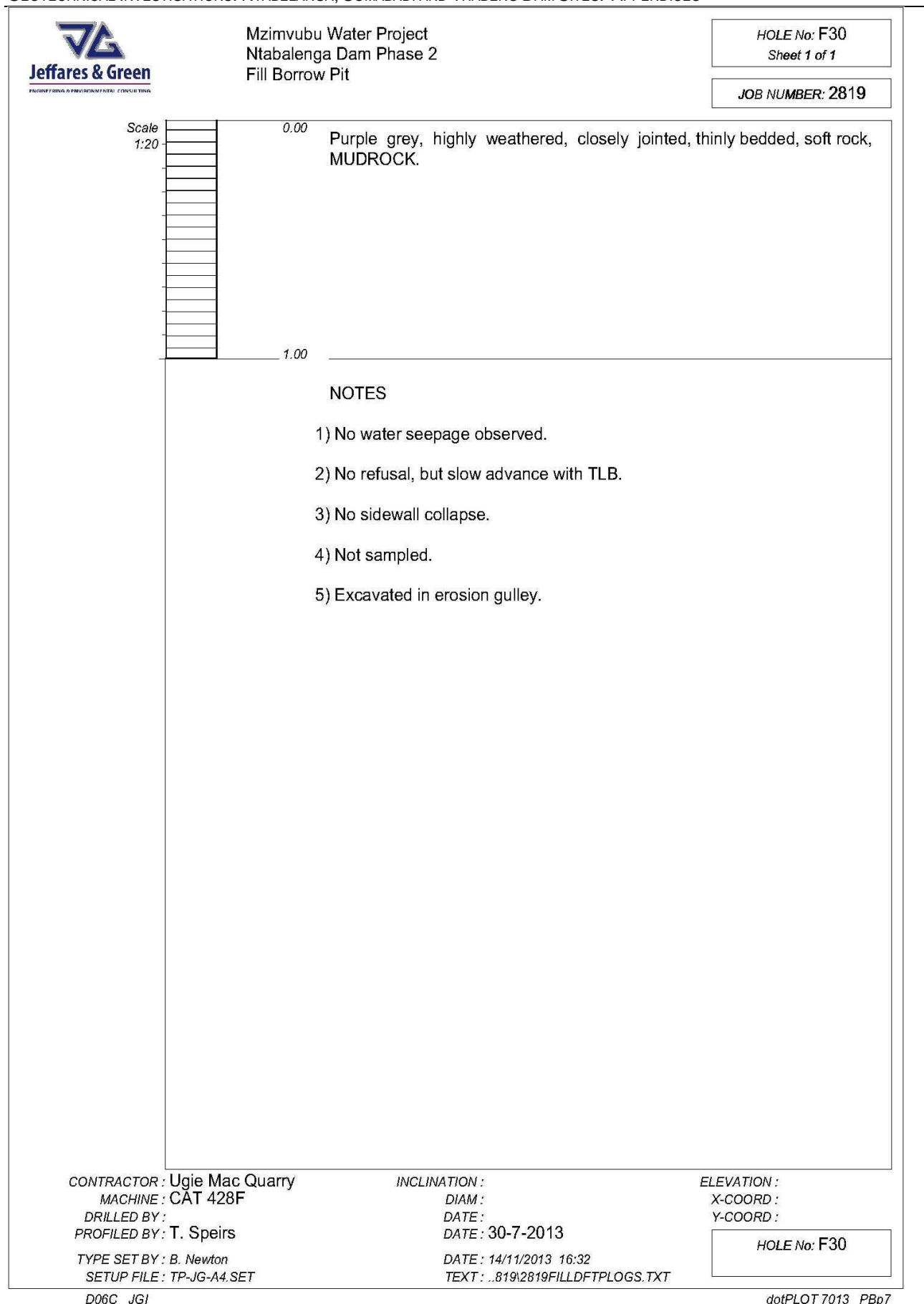


Fig G- 83: Fill Borrow Pit - Hole No: F30

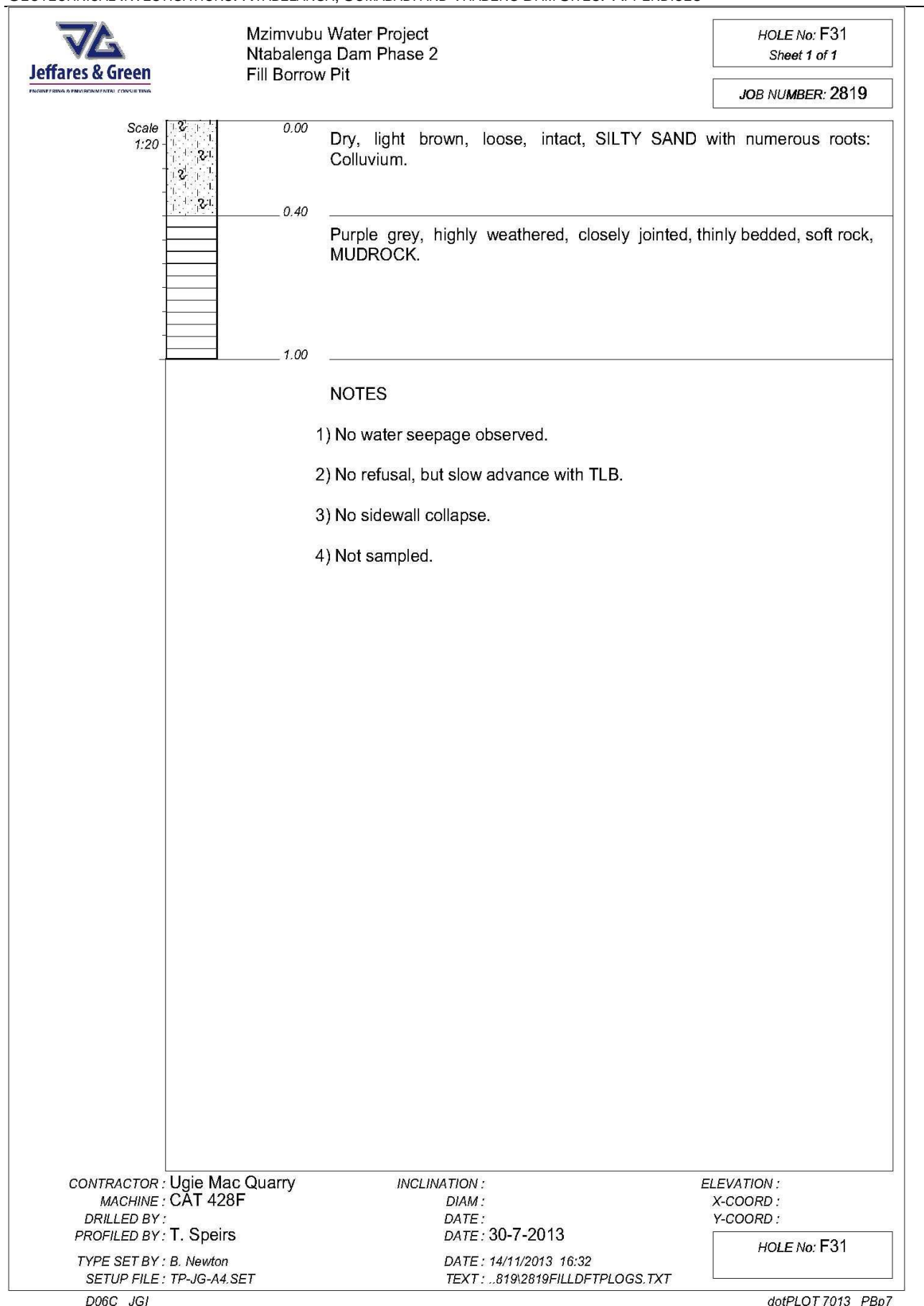


Fig G- 84: Fill Borrow Pit - Hole No: F31

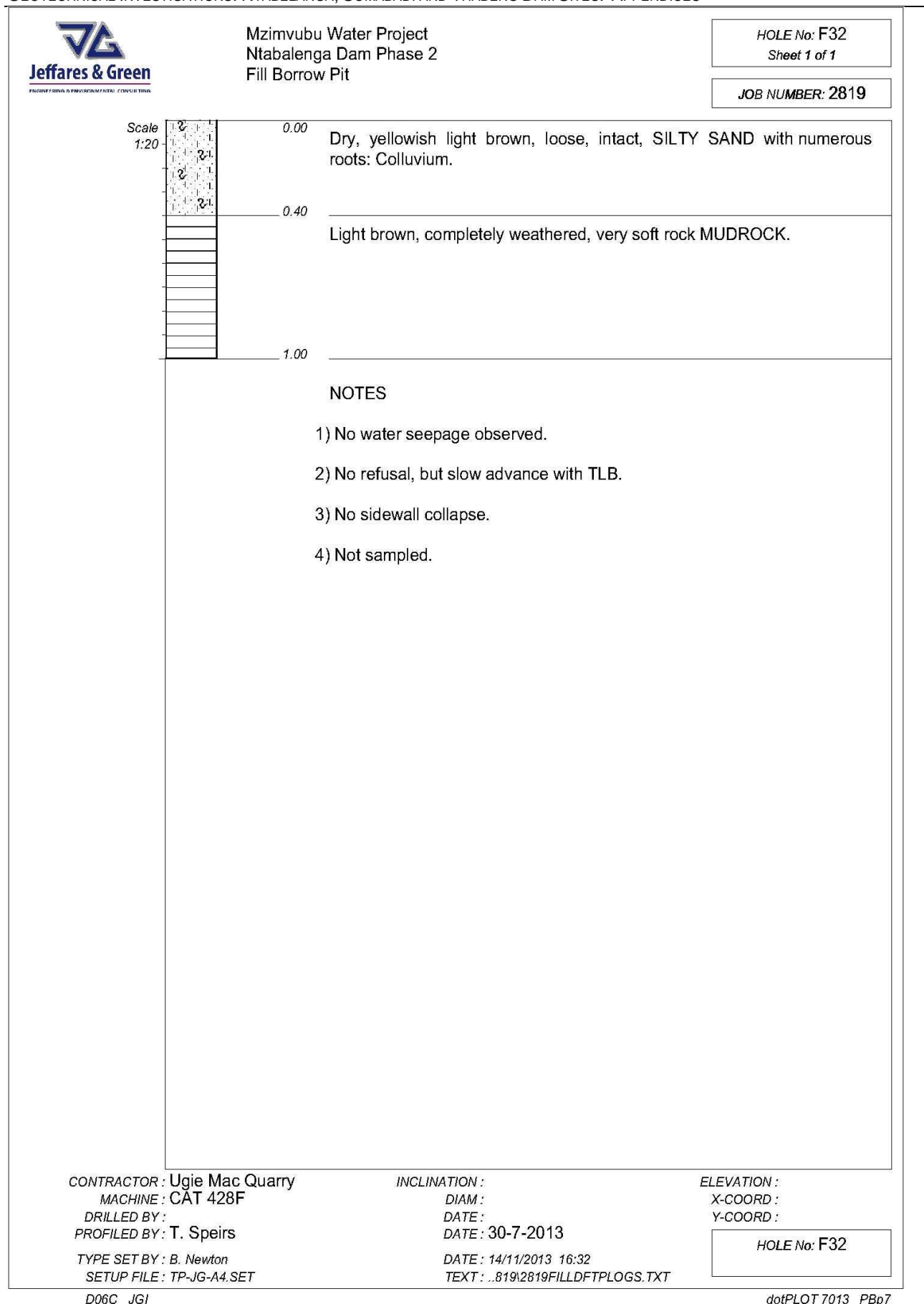


Fig G- 85: Fill Borrow Pit - Hole No: F32

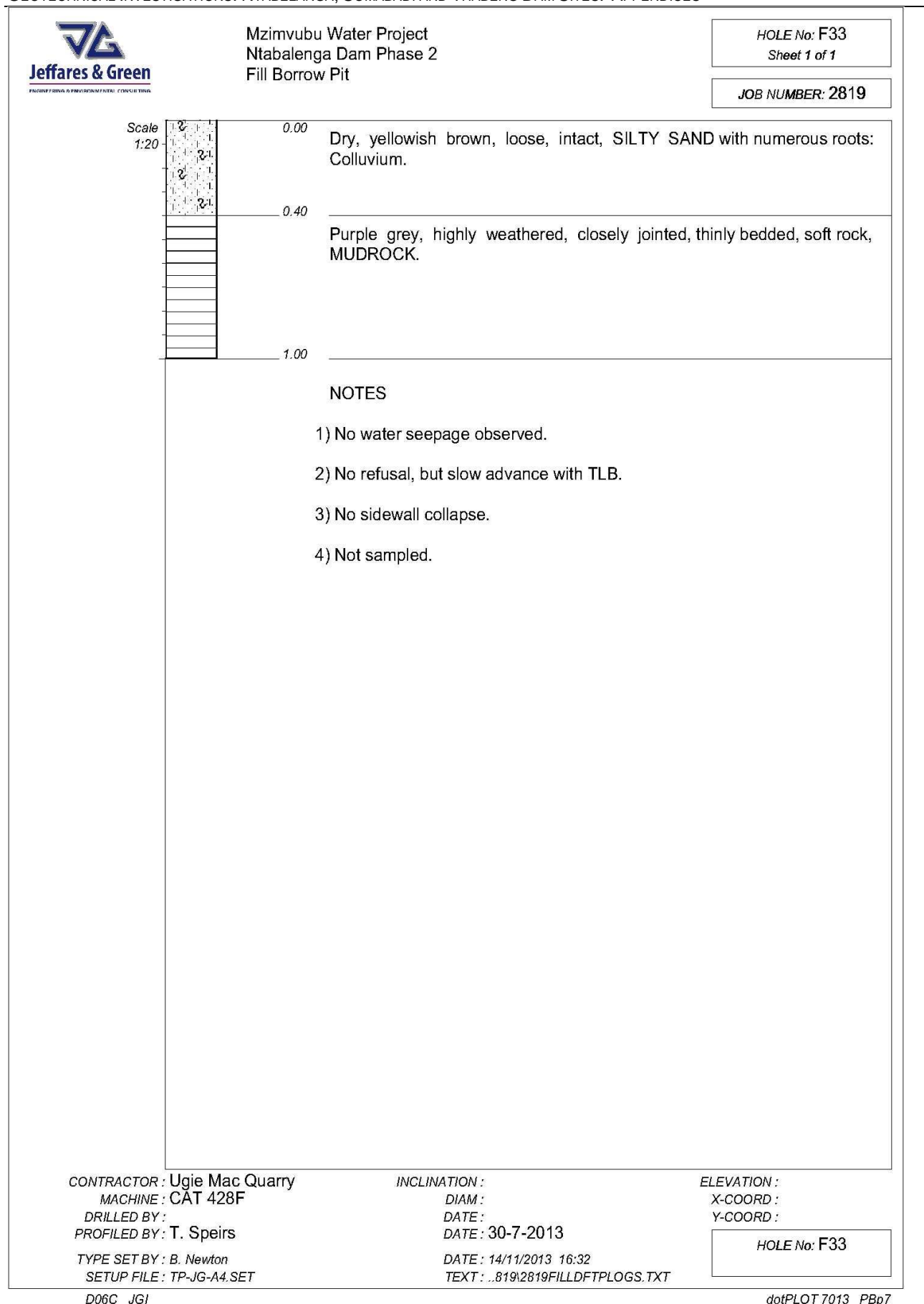


Fig G- 86: Fill Borrow Pit - Hole No: F33

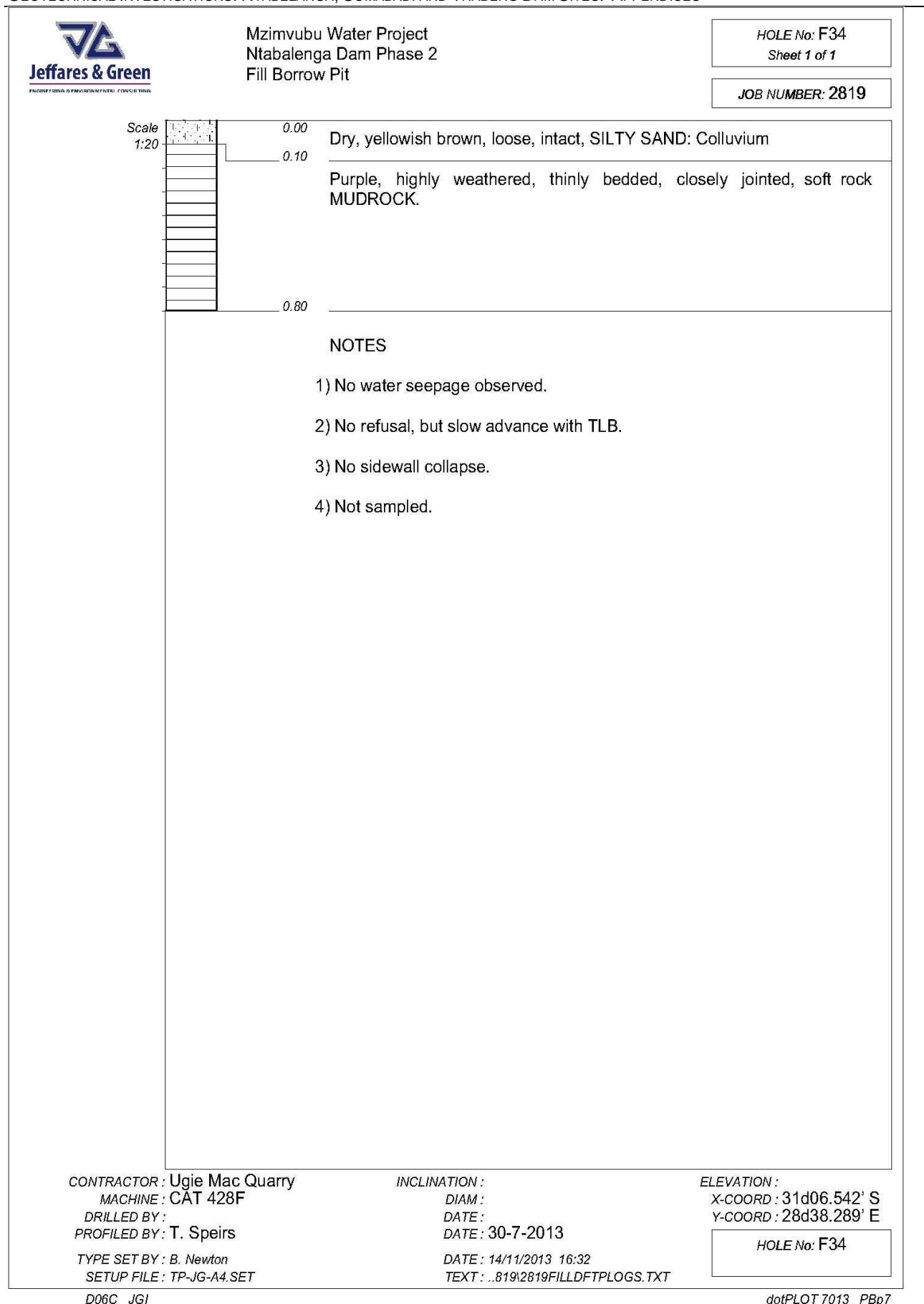


Fig G- 87: Fill Borrow Pit - Hole No: F34

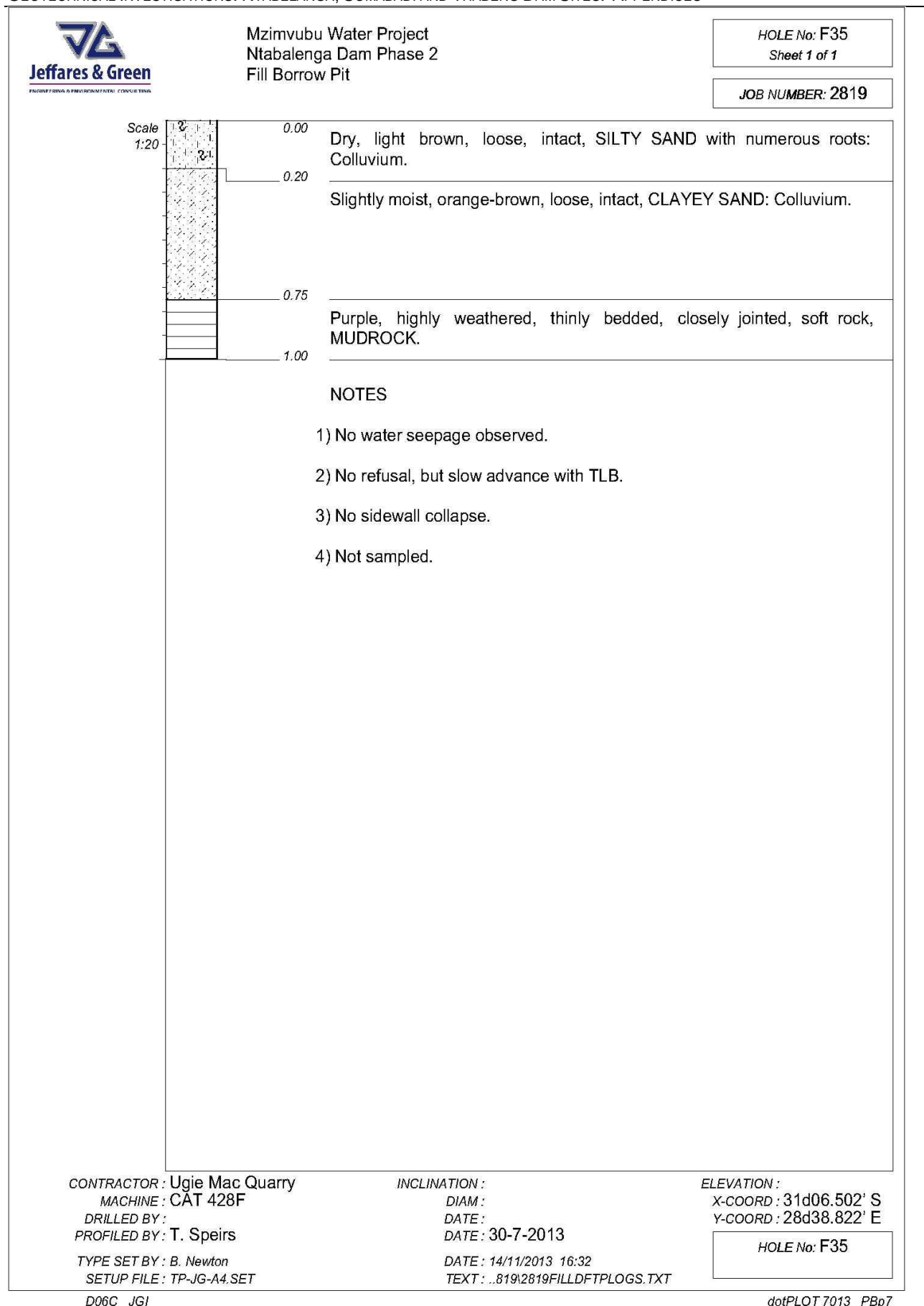


Fig G- 88: Fill Borrow Pit - Hole No: F35

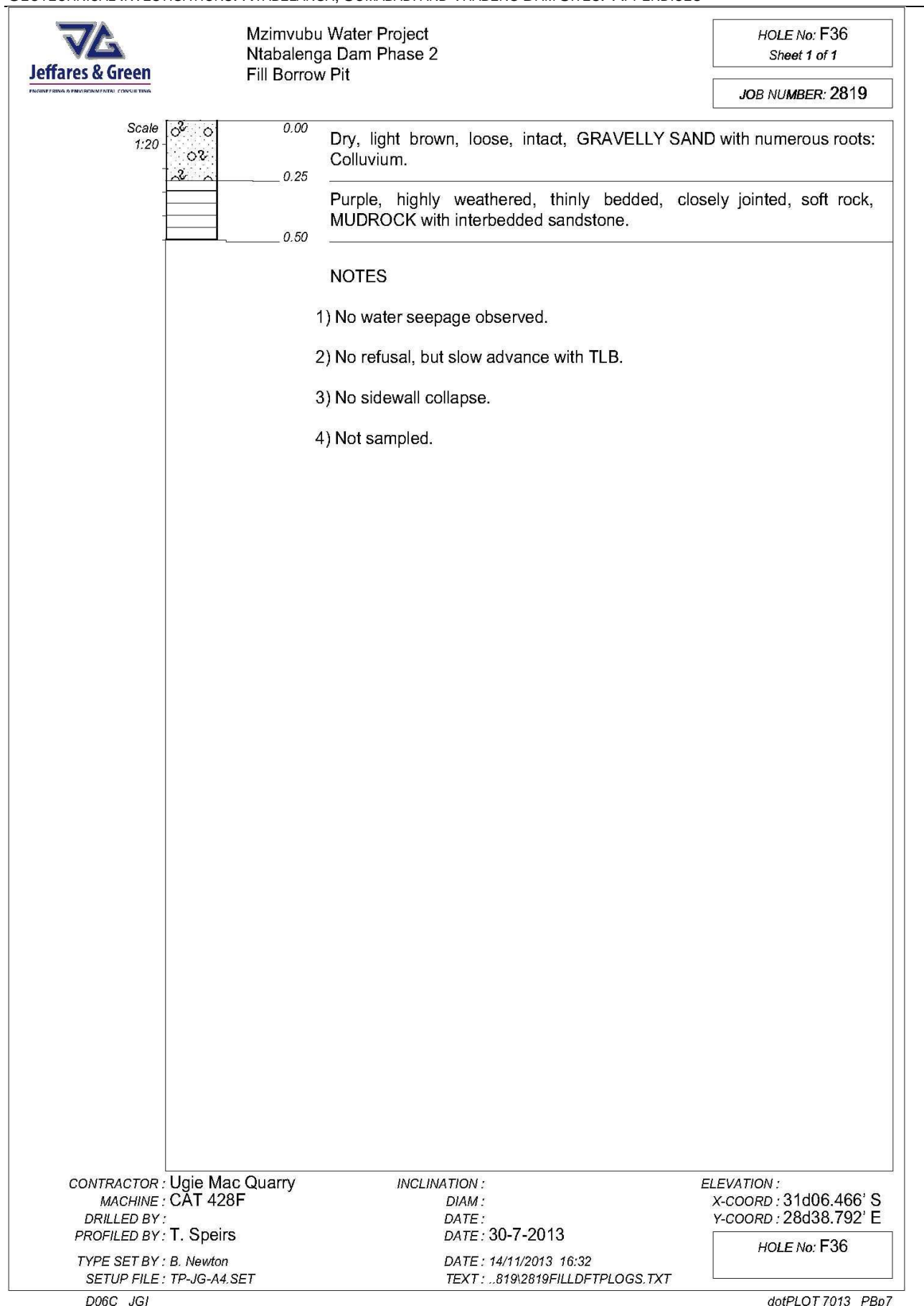


Fig G- 89: Fill Borrow Pit - Hole No: F36

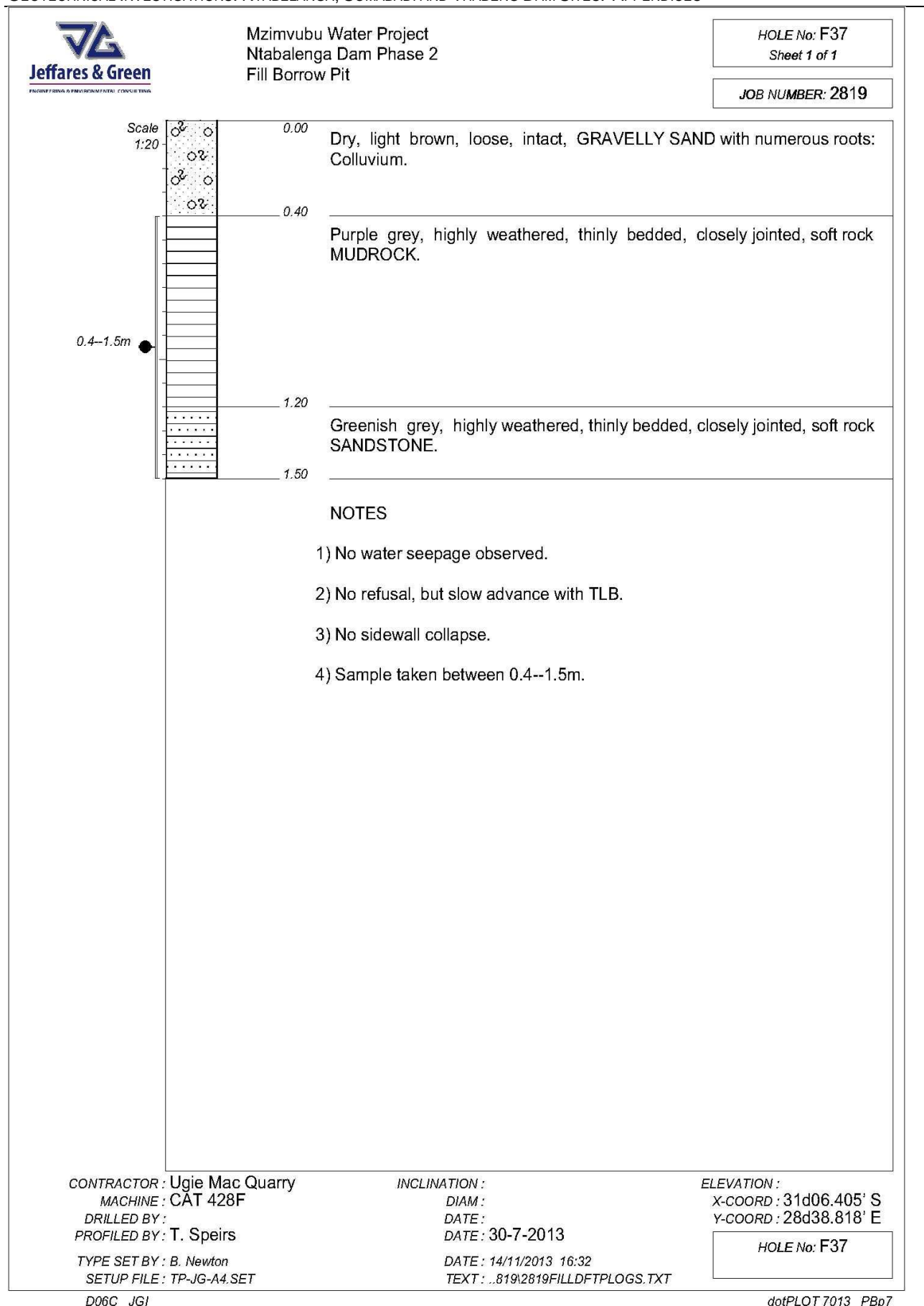


Fig G- 90: Fill Borrow Pit - Hole No: F37

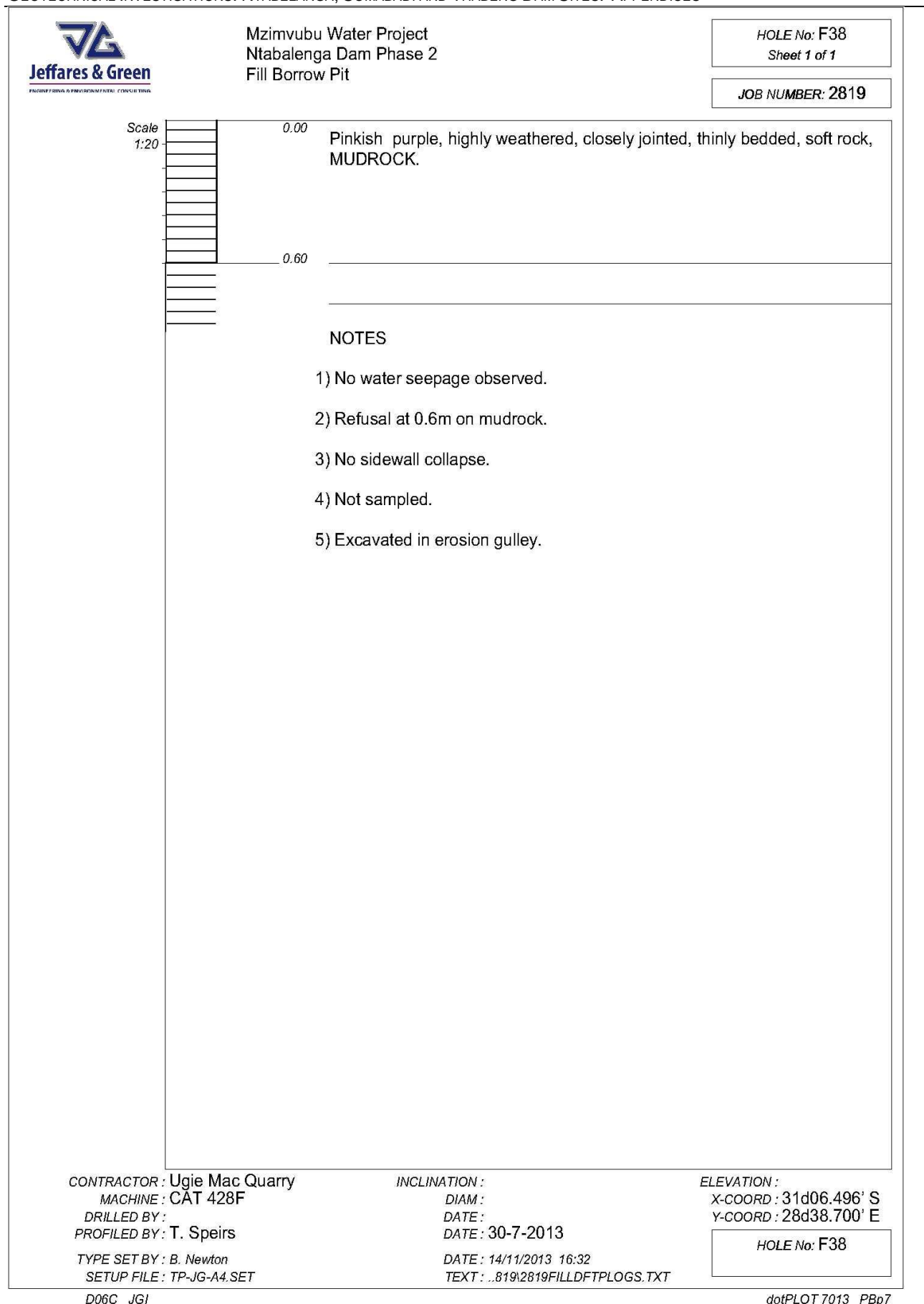


Fig G- 91: Fill Borrow Pit - Hole No: F38

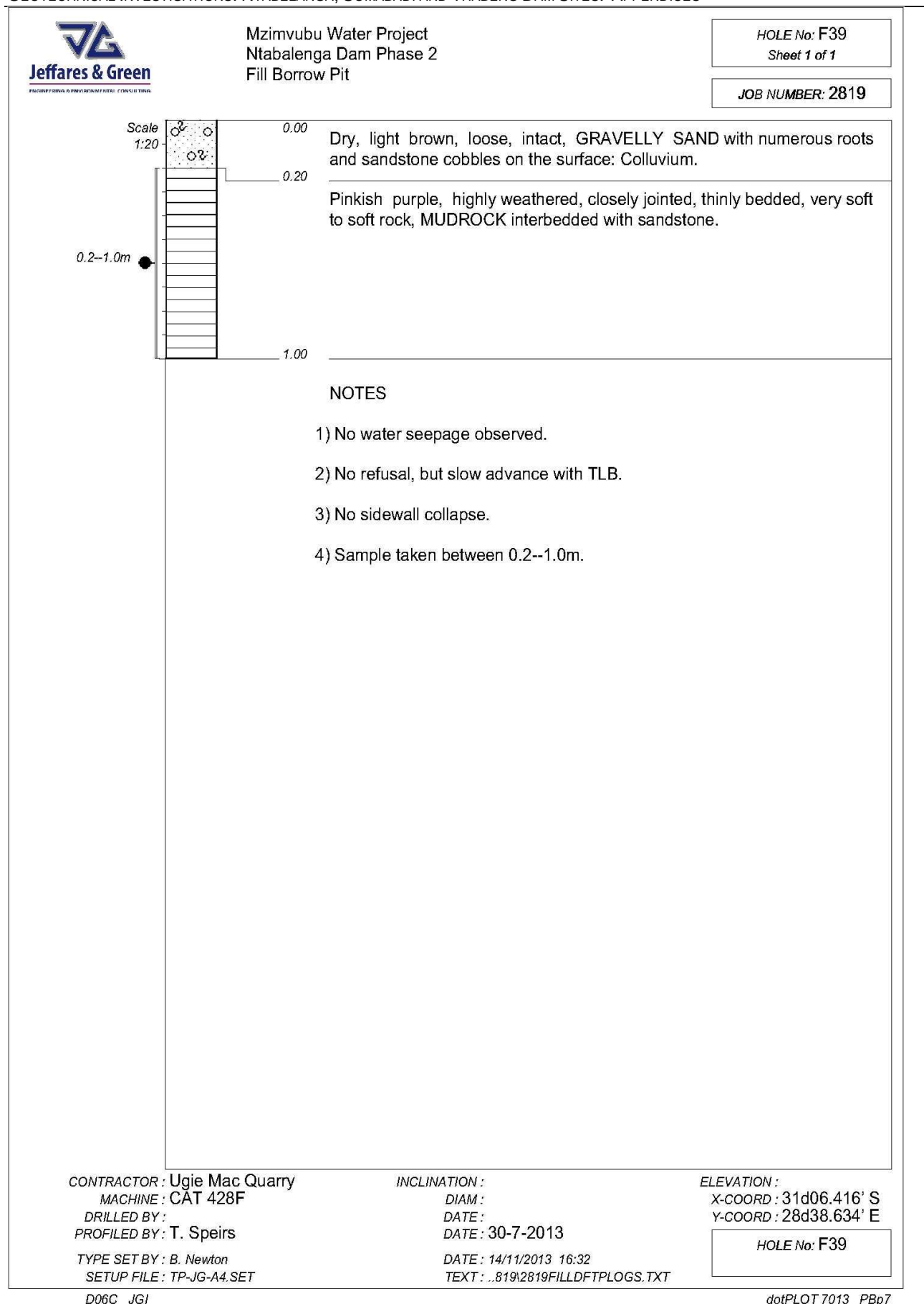


Fig G- 92: Fill Borrow Pit - Hole No: F39

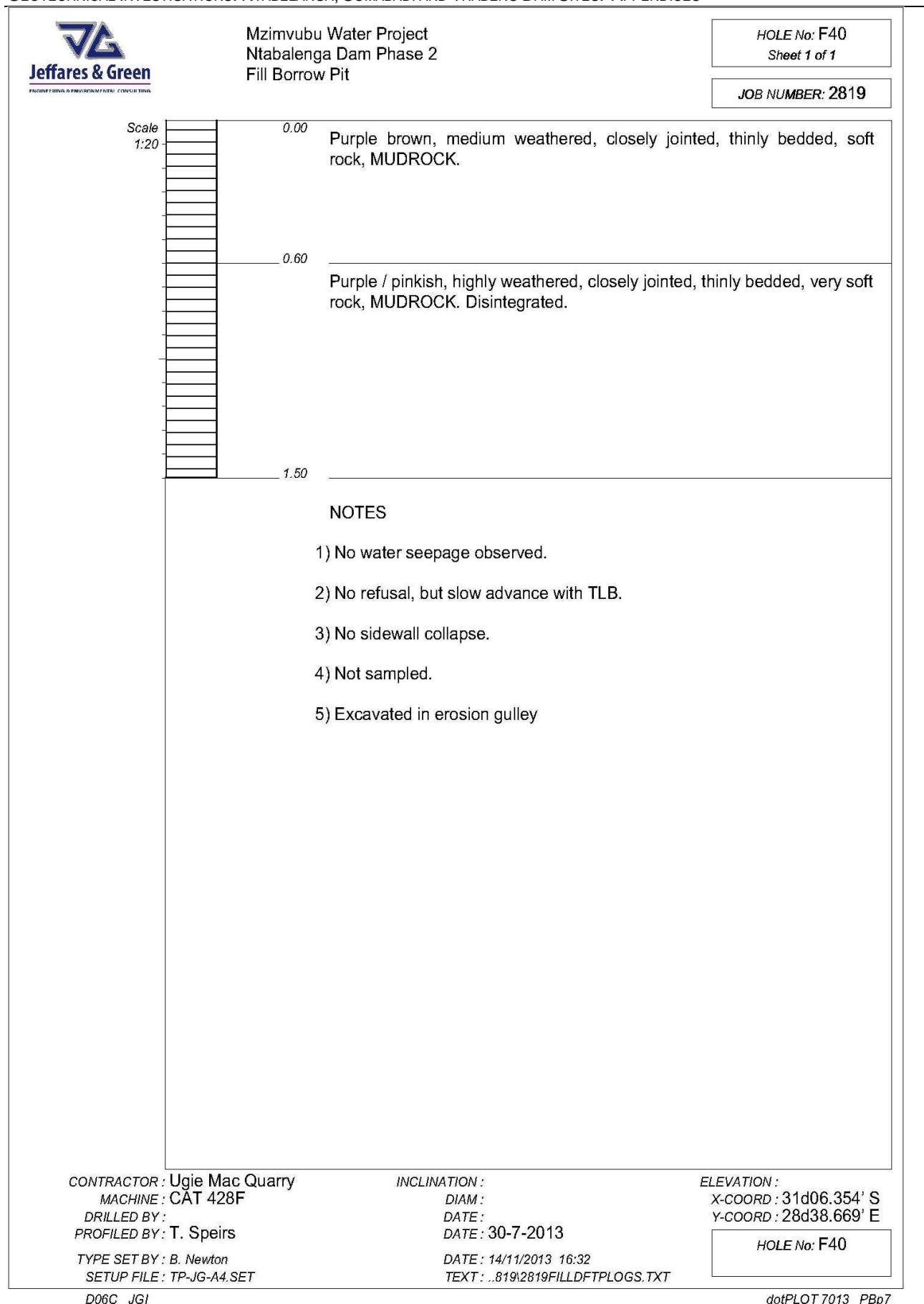


Fig G- 93: Fill Borrow Pit - Hole No: F40

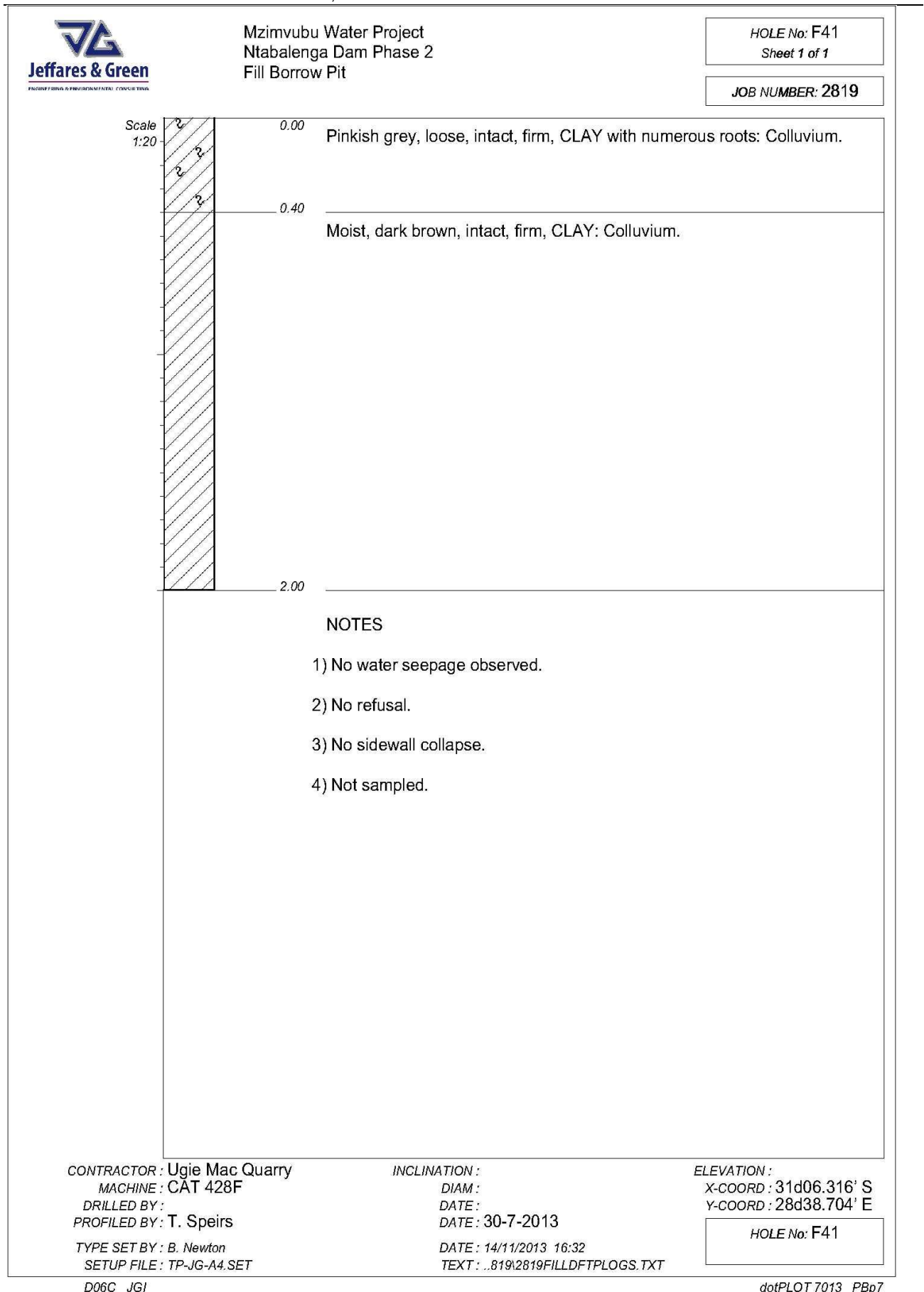


Fig G- 94: Fill Borrow Pit - Hole No: F41

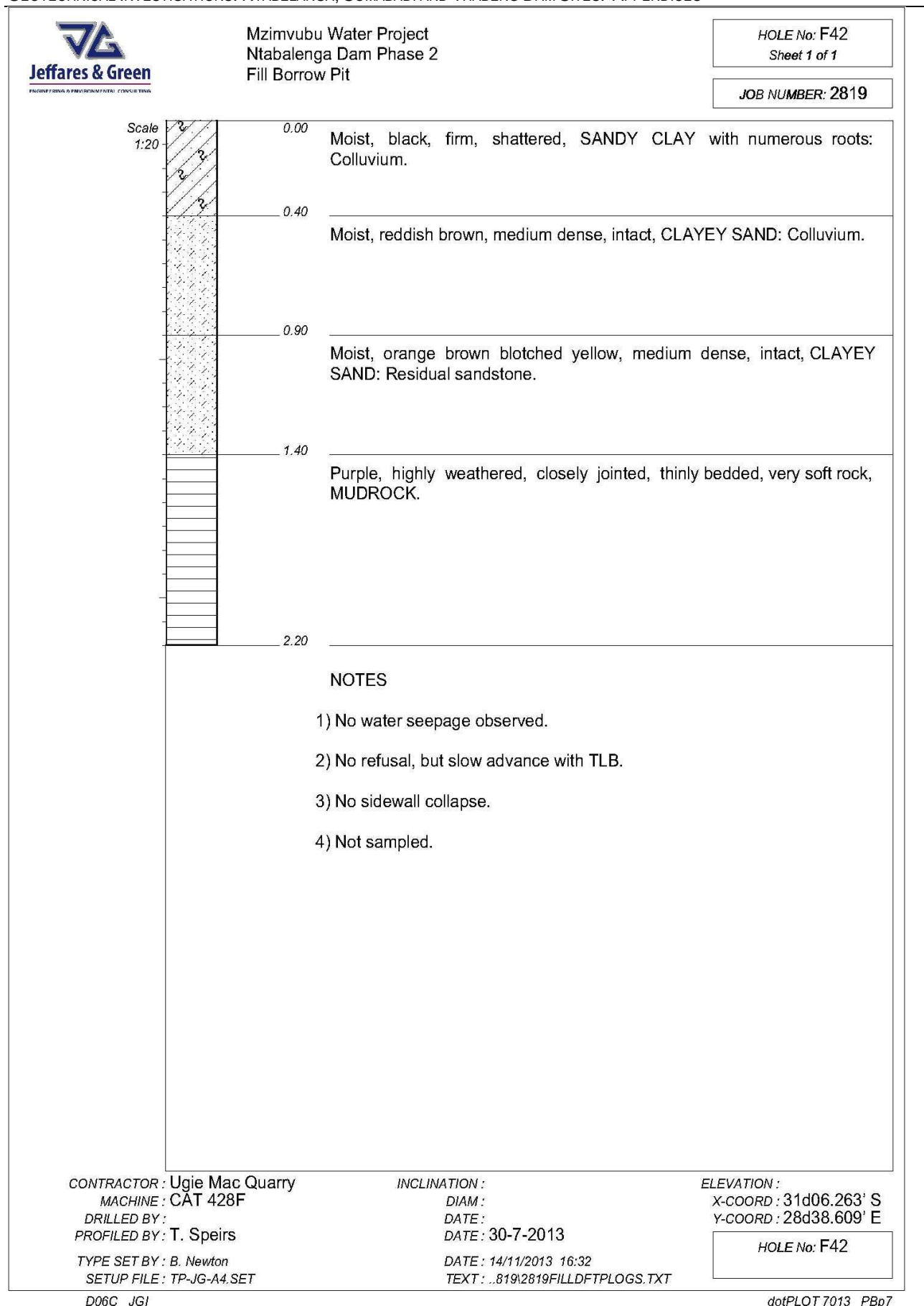


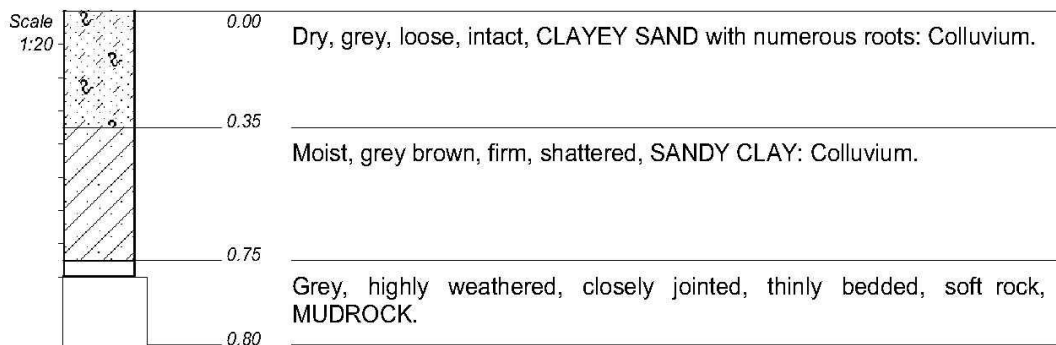
Fig G- 95: Fill Borrow Pit - Hole No: F42



Mzimvubu Water Project
 Ntabalenga Dam Phase 2
 Fill Borrow Pit

HOLE No: F43
 Sheet 1 of 1

JOB NUMBER: 2819



NOTES

- 1) No water seepage observed.
- 2) No refusal.
- 3) No sidewall collapse.
- 4) Not sampled.

CONTRACTOR : Ugie Mac Quarry
 MACHINE : CAT 428F
 DRILLED BY :
 PROFILED BY : T. Speirs

TYPE SET BY : B. Newton
 SETUP FILE : TP-JG-A4.SET

INCLINATION :
 DIAM :
 DATE :
 DATE : 30-7-2013

DATE : 14/11/2013 16:32
 TEXT : ...819\2819\FILLDFTPLOGS.TXT

ELEVATION :
 X-COORD :
 Y-COORD :

HOLE No: F43

D06C JGI

dotPLOT 7013 PBp7

Fig G- 96: Fill Borrow Pit - Hole No: F43

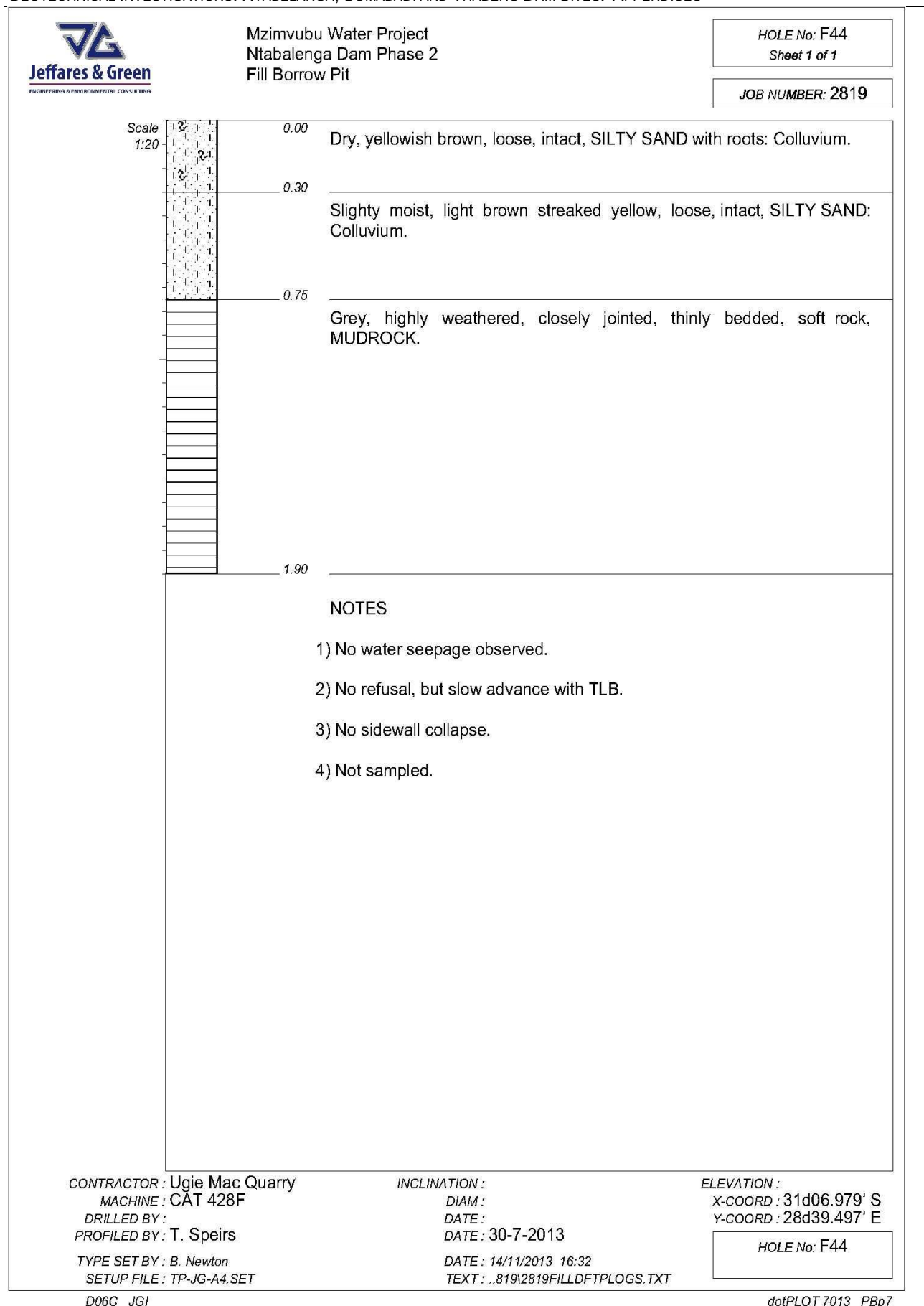


Fig G- 97: Fill Borrow Pit - Hole No: F44

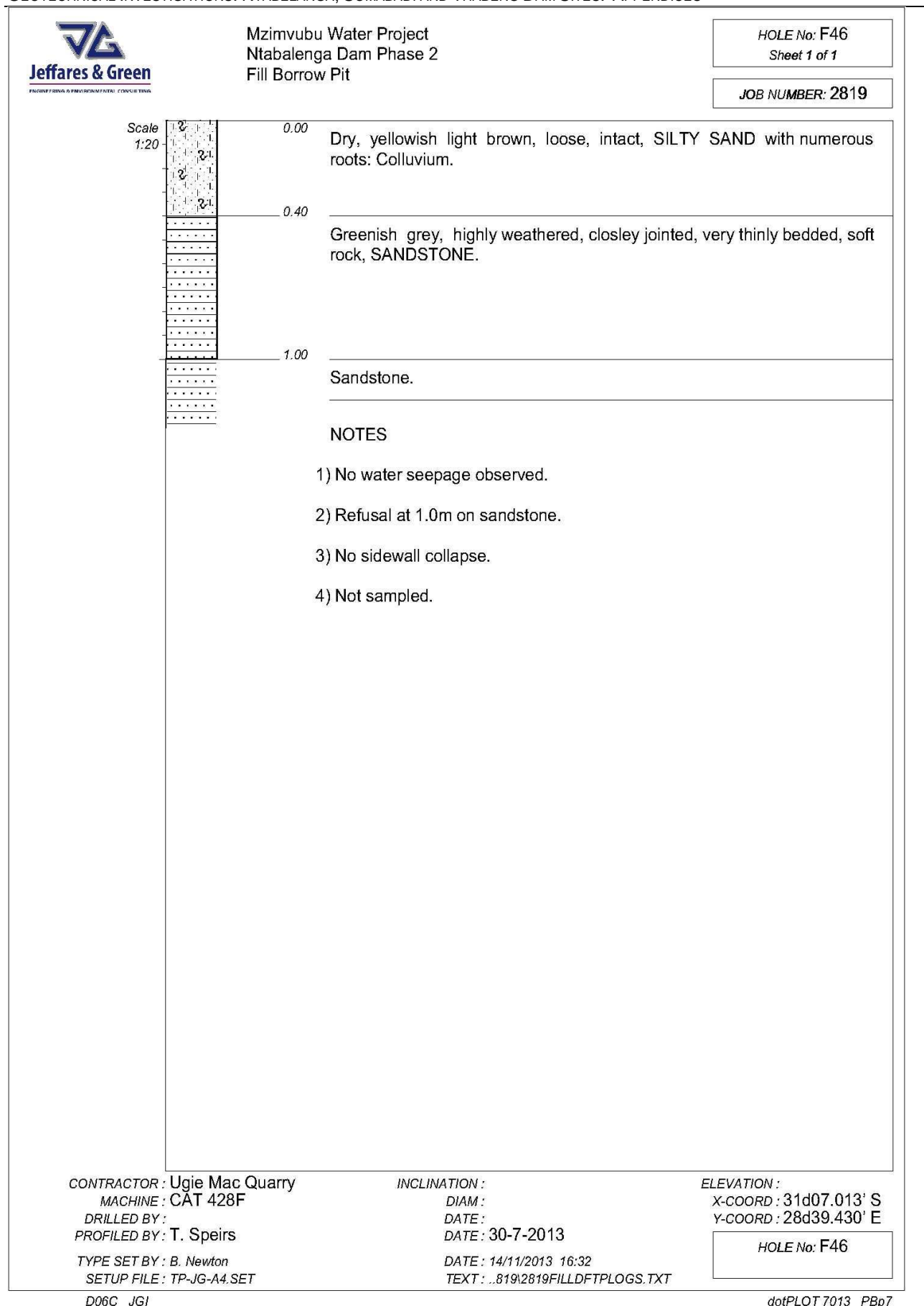


Fig G- 99: Fill Borrow Pit - Hole No: F46

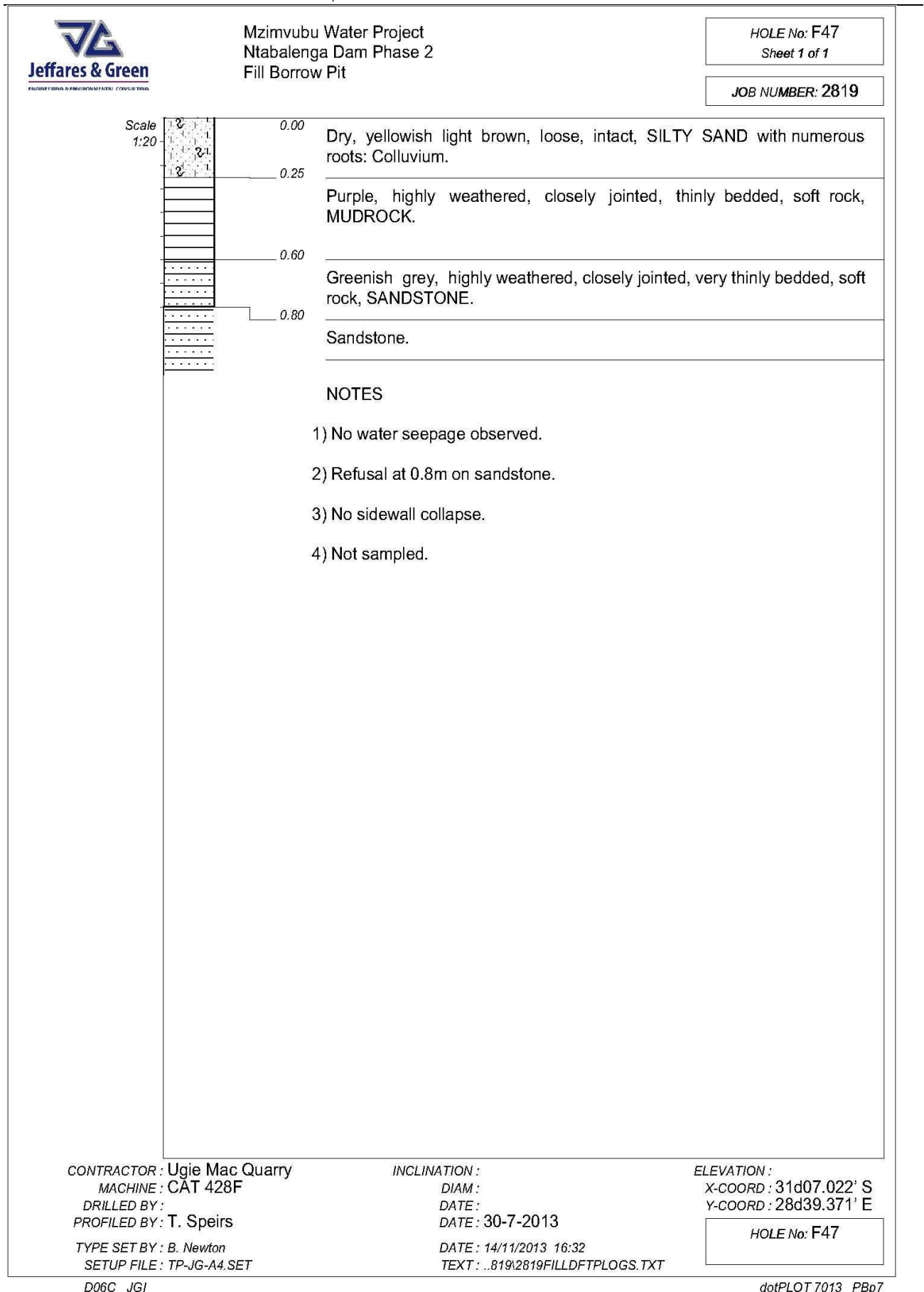


Fig G- 100: Fill Borrow Pit - Hole No: F47

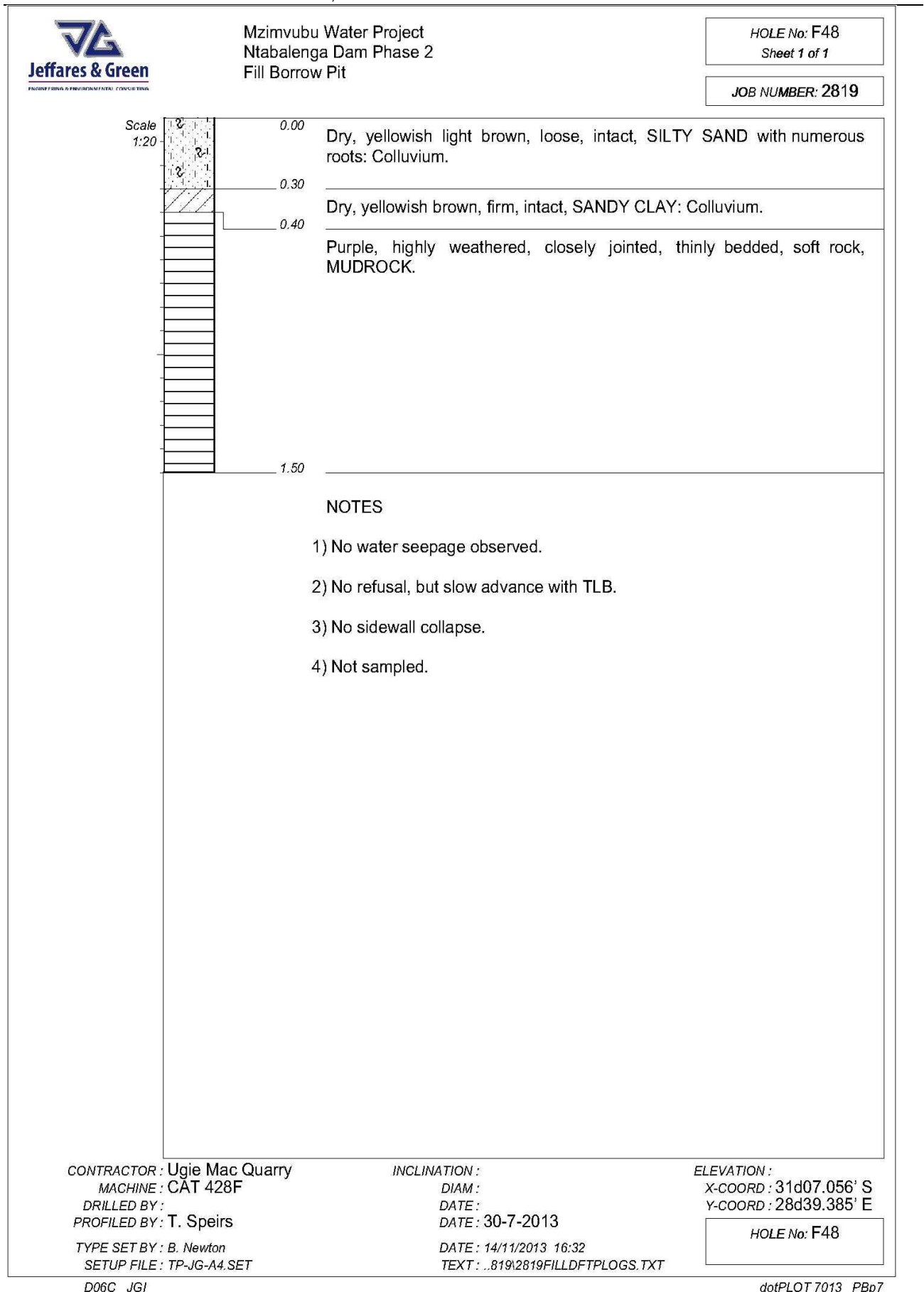


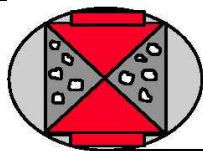
Fig G- 101: Fill Borrow Pit - Hole No: F48

APPENDIX H

LABORATORY TEST RESULTS

H1

UCS



CONTEST

Concrete Technology Services

P O Box 1675, Hillcrest, 3650, South Africa. Tel (031) 700 9394 (031) 700 9342
E-mail : ukhonkolo@contest.co.za

This report shall not be reproduced, except in full, without the approval of Contest

Ref: CJ13/09/935 2 October, 2013
Client: Jeffares & Green Consultants
Project: Mzimvubu Water Project - Ntabelanga Dam: Phase 2 Geotechnical Investigation
Subject: Compressive Strength Testing on Dolerite Rock Cores
Order: Mr T Speirs

LABORATORY REPORT TESTING OF ROCK CORES

1. CLIENT

1.1 Jeffares & Green, P O Box 794, HILTON, 3201.

2. BRIEF FROM CLIENT

2.1 Contest was requested to determine the compressive strength of five dolerite rock cores received on 20.09.2013 in accordance with SANS 5865:2006.

3. SAMPLES

3.1 Five dolerite rock cores were tested on 23.09.2013.

4. INFORMATION SUPPLIED BY THE CLIENT

4.1 Site : Ntabelanga Dam (Mzimvubu Water Project)
4.2 Location : Borehole:
: N1 - (7.82 - 7.95)
: N2 - (7.75 - 7.9)
: N2 - (12.31 - 12.49)
: NL 2/6 - (1.95 - 2.25)
: NL 2/9 - (4.89 - 2.25)
4.3 Date drilled : Not given
4.4 Drilling contractor : Not given

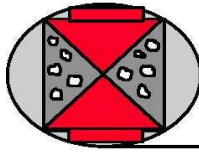
5. CORE PREPARATION

5.1 Testing of cores were carried out by our laboratories in Westmead
5.2 The cores were measured as received; any significant details recorded and then marked up for trimming.

Adam Investments cc. Reg. No 1988/019362/23 t/a CONTEST Concrete Technology Services
Managing Member: A J M Horton Pr Tech (Eng), Dip ACT, HND (Chem), HNC (Civ. Eng), FICT, MSA Corr I
Members: MT Clark, JS Dunnett, MC Mzobe, R/JL Raw B Tech (Civil Eng)

Page 1 of 2

Testing, Training and Consulting in Concrete



CONTEST

Concrete Technology Services

- 5.3 The cores were photographed in surface dry and wet states.
- 5.4 After trimming to length the cores were weighed in air and water, in order to determine the density.
- 5.5 Finally the cores were capped using sulphur mortar.

6. RESULTS

- 6.1 See appended core report and photographs.

COMMENT

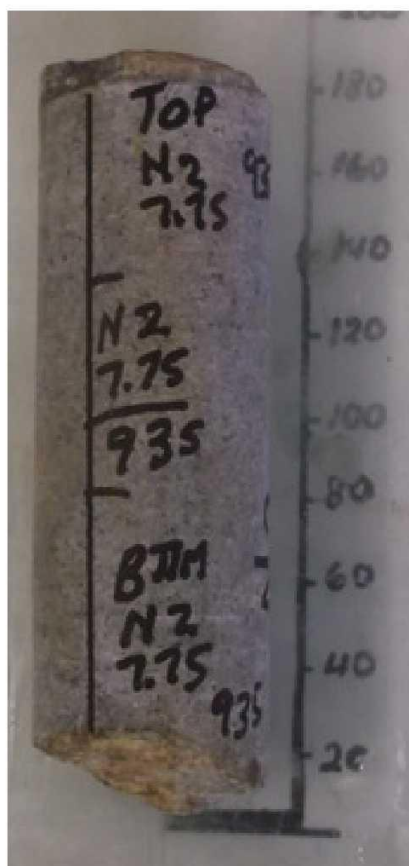
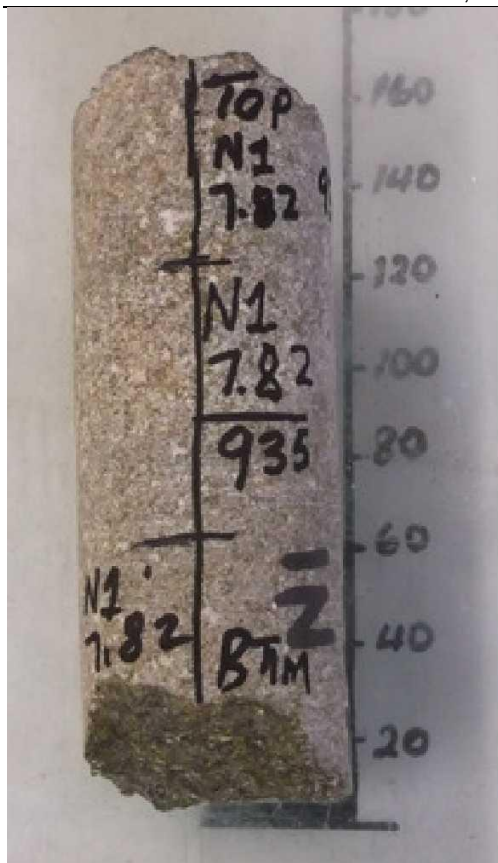
Core Number N1 (7.82 – 7.95) showed the typical signs of rock decomposition which are a change in colour of the rock from a dark grey for dolomite to a brown/yellow colouration. This decomposition would have contributed significantly to the lower compressive strength measured for this core.

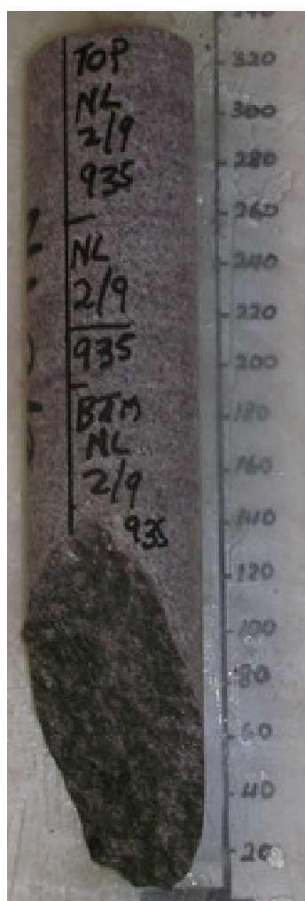
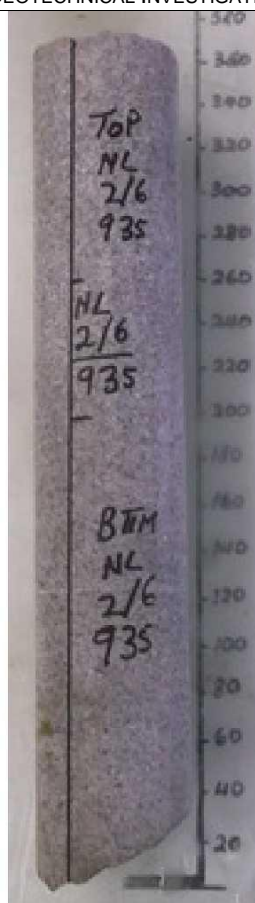
RJL RAW B Tech (Civil Eng)

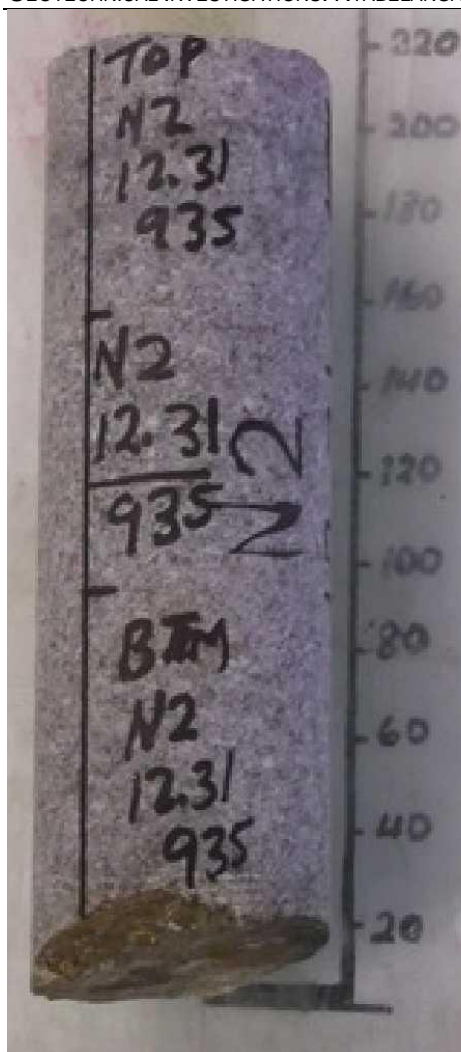
CORE REPORT					
Client	Jeffares & Green Consultants				
Project	Mzimvubu Water Project - Ntabelanga Dam: Phase 2 Geotechnical Investigation				
Job Number	CJ13/09/935				
Date Cast	Not given				
Date Tested	23.09.2013				
Age, Day	Not given				
Date Received	20.09.2013				
Direction of Dilling	Not given				
Report date	26.09.2013				
Client Reference	BOREHOLE NO - (DOLERITE ROCK CORES)				
	N1 (7.82-7.95)	N2 (7.75-7.9)	N2 (12.31-12.49)	NL 2/6 (1.95-2.25)	NL 2/9 (4.89-5.09)
DIMENSIONS					
Max length (mm)	125	155	350	300	195
Min length (mm)	120	140	295	175	175
Diameter (mm)	51.52	52.03	60.34	60.38	60.48
Trim Length (mm)	51.62	52.69	61.03	60.17	60.27
Capped length (mm)	51.40	52.67	61.04	60.07	60.19
Trim length/diameter	1.00	0.99	0.99	1.00	1.00
Cap length/diameter	1.00	0.99	0.99	1.01	1.00
REINFORCEMENT					
	Steel 1	Steel 1	Steel 1	Steel 1	Steel 1
Dist. from end (mm)	0.0	0.0	0.0	0.0	0.0
Diameter (mm)	0.0	0.0	0.0	0.0	0.0
Mass (g)	0.0	0.0	0.0	0.0	0.0
	Steel 2	Steel 2	Steel 2	Steel 2	Steel 2
Dist. from end (mm)	0.0	0.0	0.0	0.0	0.0
Diameter (mm)	0.0	0.0	0.0	0.0	0.0
Mass (g)	0.0	0.0	0.0	0.0	0.0
DENSITY					
Mass in air (g)	275	299	466	460	462
Density (kg/m3)	2894	2978	2996	2976	2981
Air Voids %	0.00	0.00	0.00	0.00	0.00
CORRECTIONS					
Length	1.00	1.00	1.00	1.00	1.00
Steel reinforcement	1.00	1.00	1.00	1.00	1.00
Air voids	1.00	1.00	1.00	1.00	1.00
LOADING					
Load at failure (kN)	97.3	354.8	390.5	375.4	584.0
Failure mode	normal	normal	normal	normal	normal
STRENGTH (MPa)					
Uncorrected Strength	46.7	166.8	136.6	131.1	203.2
Length corrected	46.7	166.8	136.6	131.1	203.2
Length/Steel corrected	46.7	166.8	136.6	131.1	203.2
Length/Voids/Steel corrected	46.7	166.8	136.6	131.1	203.2
Notes					
1. Sulphur mortar capping					
2. SABS Test Method 865:1994					
3.Length correction is non-standard					



RJL RAW







H2

PETROGRAPHIC



UNIVERSITEIT VAN PRETORIA
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YUNIBESITHI YA PRETORIA
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E-Mail: wiebke.grote@up.ac.za
<http://www.up.ac.za/academic/science>

CLIENT: Jeffares & Green (Pty) Ltd

DATE: 28 October 2013

SAMPLES: 5 Samples

YOUR REFERENCE: "CIVILAB SUBCONTRACT TESTING"

PROJECT: MZIMVUBU WATER PROJECT

ANALYSIS: Petrographic investigation of 5 dolerite core samples

Two thin sections from each core were prepared.

Summary:

Macroscopic description: Massive, fine to medium-grained dark grey intrusive igneous rock with a distinct dolerite texture.

Microscopic description:

When not stated otherwise the microscope pictures were taken with 10x magnification, field of view 1250µm wide and cross polarized illumination.

The dolerites appear holocrystalline, relatively fresh, fine to medium grained with an ophitic texture. The main constituent in the thin sections is plagioclase (feldspar) and clinopyroxene (augite). The alteration of the plagioclase to sericite and pyroxene to chlorite (or traces of hornblende and/or possible smectite) seems to be low, approximately around 10%.

The 5 samples (drill cores) are very similar.

Thin Section Description:

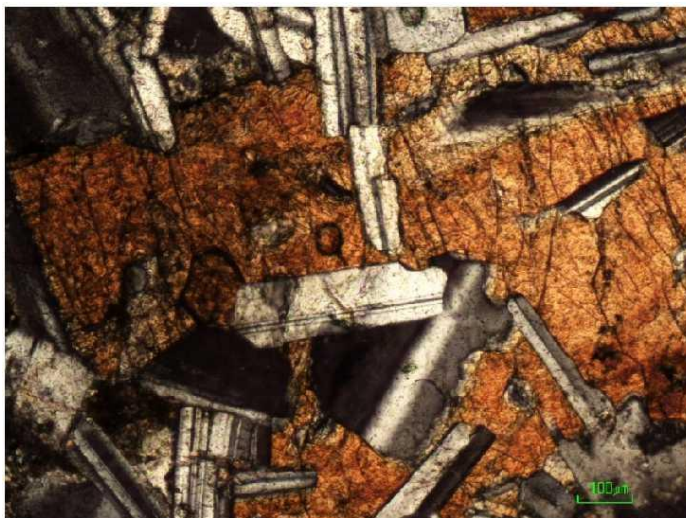
Sample name: N1_ 7.7 – 7.82

Constituents: Fine to medium grained euhedral lath-shaped plagioclase crystals (~60%) intergrown by clinopyroxene (~33%). Minor quartz (~2%) and less than 1% opaque minerals (oxides) is present. Secondary minerals (~5%) include chlorite, sericite (white mica) and traces of hornblende.

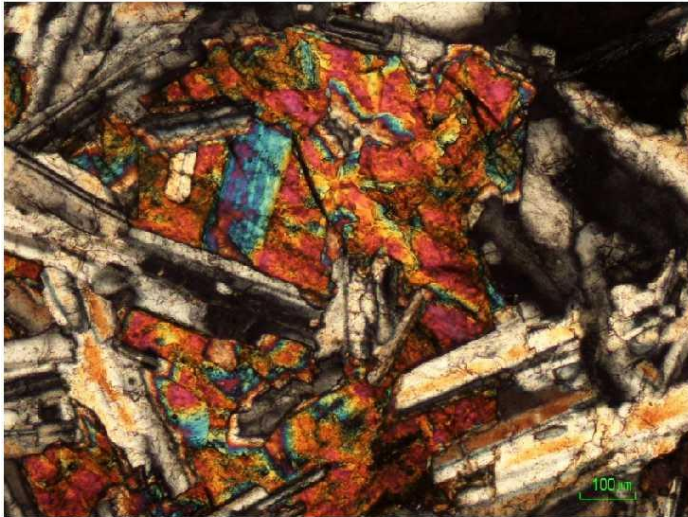
Grain size data: $\leq 500 \geq 1000$ micron

Description:

The section is dominated by generally lath-shaped medium to fine grained feldspar (plagioclase) showing albite twinning, and subhedral to anhedral clinopyroxene (augite). The laths of plagioclase are randomly orientated and the clinopyroxenes (augite) occupy a more interstitial position to the plagioclase. Some of the irregular shaped augites, exhibit a pink colour indicative of Ti-content. The pyroxenes show alteration to chlorite along cleavage and rims. Some plagioclase grains show secondary alteration to sericite. The opaque minerals (oxides) are irregular in shape. The degree of alteration is low.



N1_ 7.7 – 7.82: Larger pyroxene crystal encloses the plagioclase laths



N1_ 7.7 – 7.82: Pyroxene and plagioclase (Thin section little too thick)

Sample name: N1_ 11.84-12.2

Thin Section Description:

Constituents: Fine to medium grained euhedral lath-shaped plagioclase crystals (~55%) intergrown by clinopyroxene (~30%). Minor quartz (~3%) and about 1% opaque minerals (oxides) is present. Secondary minerals (~10%) include chlorite, sericite (white mica) and traces of hornblende and smectite (swelling clay).

Grain size data: $\leq 500 \geq 1000$ micron

Description:

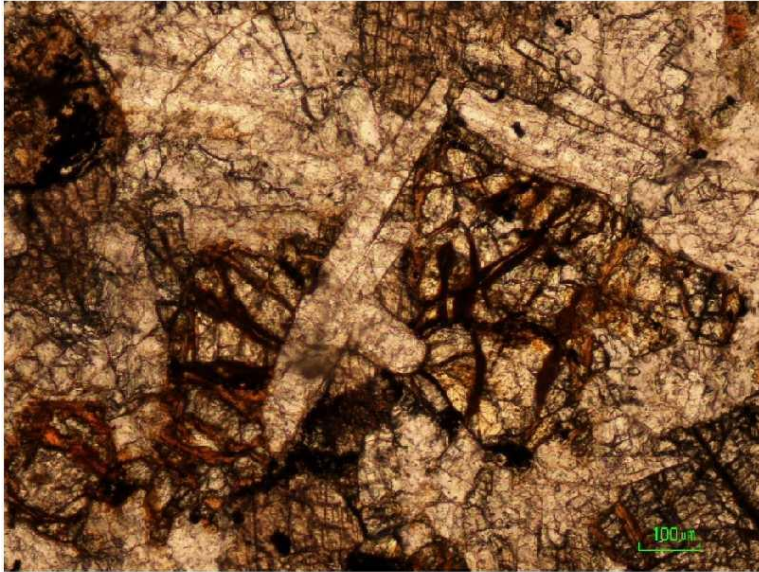
The section is dominated by generally lath-shaped medium to fine grained feldspar (plagioclase) showing polysynthetic twinning, and subhedral to anhedral clinopyroxene (augite). The laths of plagioclase are randomly orientated and the clinopyroxenes (augite) occupy a more interstitial position to the plagioclase. Some of the irregular augite crystals exhibit a pink colour indicative of Ti-content. The pyroxenes show alteration to chlorite and traces of hornblende along cleavage and rims. Some of the plagioclase have been replaced fine-grained white mica (sericite). The few opaques are irregular in shape. The degree of alteration is fairly low.



N1_ 11.84-12.2: Plagioclase showing polysynthetic twinning, enclosed by clinopyroxene.



N1_ 11.84-12.2: Alteration of plagioclase to sericite (white mica)



N1_ 11.84-12.2: Traces of smectite visible along cracks. (10x magnification, plane polarized light)

Sample name: N2_ 12.49-12.61

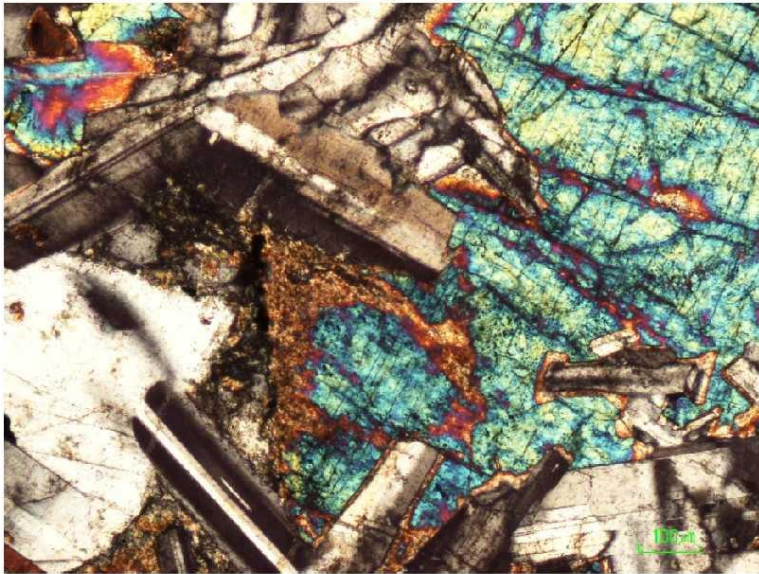
Thin Section Description:

Constituents: Fine to medium grained euhedral lath-shaped plagioclase crystals (~60%) intergrown by clinopyroxene (~26%). Minor quartz (~2%) and about 1% opaque minerals (oxides) is present. Secondary minerals (~11%) include chlorite, sericite (white mica), possibly traces of smectite (swelling clay).

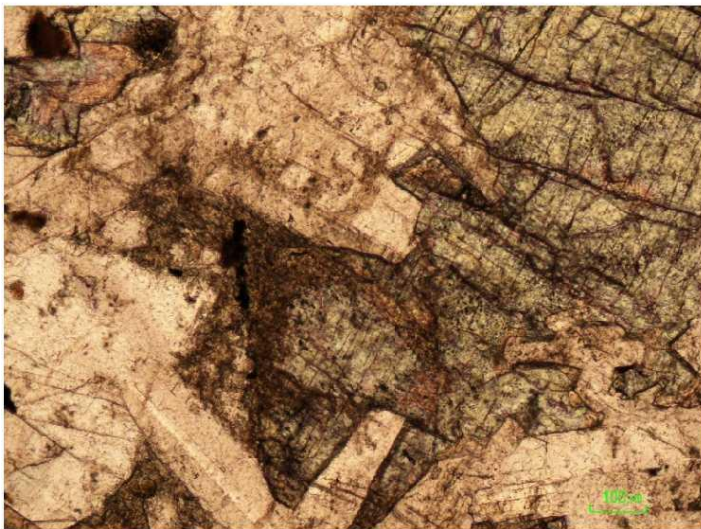
Grain size data: $\leq 500 \geq 1000$ micron

Description:

The section is dominated by generally lath-shaped medium to fine grained feldspar (plagioclase) showing albite twinning, and subhedral to anhedral clinopyroxene (augite). The laths of plagioclase are randomly orientated and the clinopyroxenes (augite) occupy a more interstitial position to the plagioclase. The pyroxenes show alteration to chlorite and possibly traces of smectite along cleavage and rims. A few plagioclase grains show partly alteration to sericite. The opaques are irregular in shape. The degree of alteration is relatively low.



N2_ 12.49-12.61: Plagioclase (showing albite or polysynthetic twinning) and Augite (showing second order interference colours, typical of clinopyroxenes). The augite crystal in the middle of the picture shows alteration on the edge.



N2_ 12.49-12.61: Same as above but under plane polarized light.
(x10 magnification, field of view 1250μm wide, plane polarized illumination)

Sample name: NL 2/6_2.25-2.47

Thin Section Description:

Constituents: Fine to medium grained euhedral lath-shaped plagioclase crystals (~60%) intergrown by clinopyroxene (~30%). Minor quartz (~3%) and about 1% opaque minerals (oxides) is present. Secondary minerals (~6%) include chlorite and sericite (white mica).

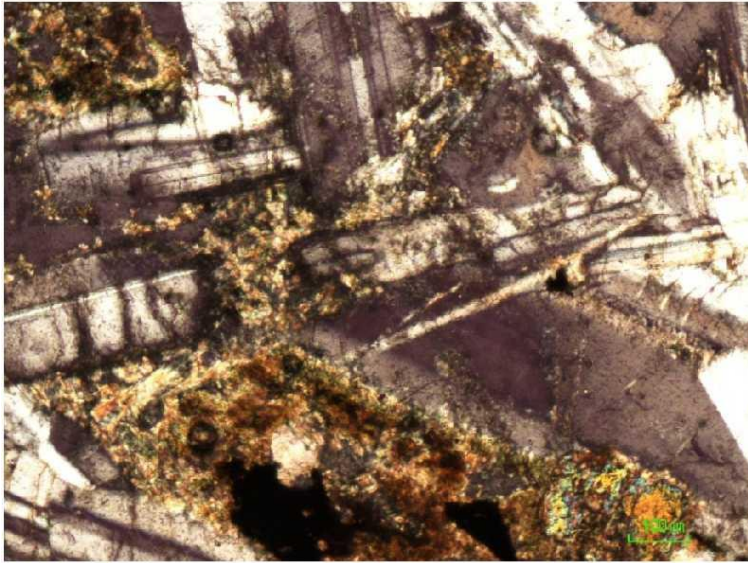
Grain size data: $\leq 500 \geq 1000$ micron

Description:

The section is dominated by generally lath-shaped medium to fine grained feldspar (plagioclase) showing albite twinning, and subhedral to anhedral clinopyroxene (augite). The laths of plagioclase are randomly orientated and the clinopyroxenes (augite) occupy a more interstitial position to the plagioclase. Some of the irregular augites exhibit a pink colour, indicative of Ti-content. The pyroxenes show alteration to chlorite along cleavage and rims. Some plagioclase grains show secondary alteration to sericite. The minor opaque minerals are irregular in shape. The degree of alteration is quite low.



NL 2/6_2.25-2.47: Quartz and Plagioclase



NL 2/6_2.25-2.47: Alteration of plagioclase is clearly visible. Black irregular shaped blobs are opaque minerals (oxides).

Sample name: NL 2/9 _ 4.3–4.58

Thin Section Description:

Constituents: Fine to medium grained euhedral lath-shaped plagioclase crystals (~58%) intergrown by clinopyroxene (~30%). Minor quartz (~4%) and about 1% opaque minerals (oxides) is present. Secondary minerals (~7%) include chlorite and sericite (white mica)

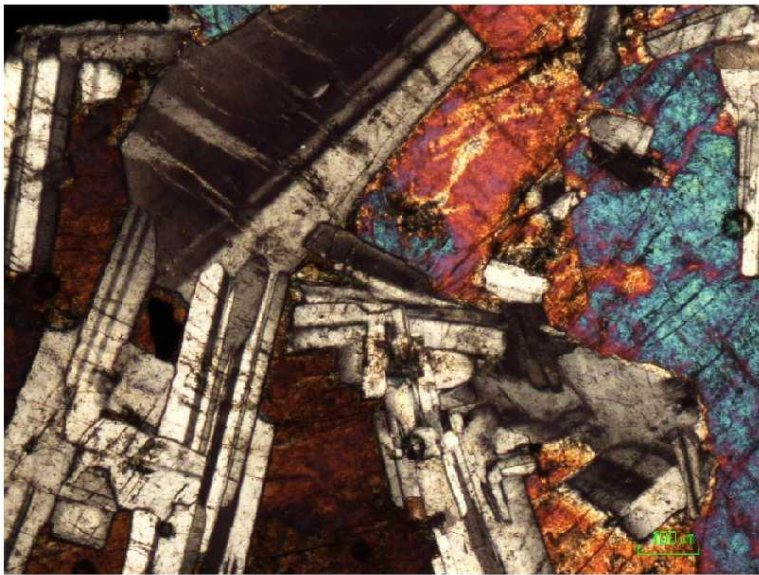
Grain size data: $\leq 500 \geq 1000$ micron

Description:

The section is dominated by generally lath-shaped medium to fine grained feldspar (plagioclase) showing albite twinning, and subhedral to anhedral clinopyroxene (augite). The laths of plagioclase are randomly orientated and the clinopyroxenes (augite) occupy a more interstitial position to the plagioclase. The pyroxenes show alteration to chlorite along cleavage and rims. Some plagioclase grains show secondary alteration to sericite. The opaques are irregular in shape. The degree of alteration is low.



NL 2/9 _ 4.3–4.58: Secondary chlorite, an alteration product, distinguishable by its green colour. (x10 magnification, field of view 1250µm wide, plane polarized illumination)



NL 2/9 _ 4.3–4.58: Plagioclase with polysynthetic twinning and augite showing interference color typical of second order.

If you have any questions, kindly contact the laboratory.

Analyst:
Wiebke Grote

H3

INDICATOR AND STANDARD PROCTOR m/d

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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E-mail: jhb@civilab.co.za • Website: www.civilab.co.za



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Civil Engineering Testing Laboratories

Client : JEFFARES & GREEN CONSULTING ENGINEERS
Address : P O BOX 1109
: SUNNINGHILL
: 2157

Client Reference :
Order No. : 2819

Attention : Tom Spiers
Facsimile : 011 807 1607
E-mail : spierst@jgi.co.za

Date Received : 23/08/2013
Date Tested : 23/08/2013 - Current
Date Reported : 11/11/2013

Project : Mzinubvu Water Project
Project No. : 2013-B-2004

Page : 1 of 44

Herewith please find the test report(s) pertaining to the above project. All tests were conducted in accordance with prescribed test method(s). Information herein consists of the following:

Test(s) conducted / Item(s) measured	Qty.	Test Method(s)	Authorized By	Page(s)
Atterberg Limits < 0.425mm	39.000	TMH1 A2, A3, A4	W van Zyl	2-21
Sieve Analysis 0.075mm (Mass Grading)	39.000	TMH1 A1	W van Zyl	2-21
Hydrometer Analysis	39.000	ASTM D422	W van Zyl	2-21
MDD & OMC	4.000	TMH1 A7	W van Zyl	22-25
Relative Density of Soil	4.000	TMH1 A12T	W van Zyl	2, 7, 12, 21
Dispersiveness: Double Hydrometer	11.000	BS1377 Part 5	W van Zyl	11 files, 11 pages
Dispersiveness: Pinhole	2.000	BS1377 Part 5	W van Zyl	
Permeability: Falling Head	3.000	KH Head	W van Zyl	1 file, 1 page
Oedometer: Standard	2.000	BS1377 Part 6	W van Zyl	2 files, 6 pages
Chloride Content	2.000	Refer to test results	Subcontracted	1 file, 1 page
Remaining: 2 x Oedometer, 1 x S.G., 4 x CU Triaxial, 1 x FH Permeability				

Any test results contained in this report and marked with * in the table above are "not SANAS accredited" and are not included in the schedule of accreditation for this laboratory.

Any information contained in this test report pertain only to the areas and/or samples tested. Documents may only be reproduced or published in their full context.

While every care is taken to ensure that all tests are carried out in accordance with recognised standards, neither Civilab (Proprietary) Limited nor its employees shall be liable in any way whatsoever for any error made in the execution or reporting of tests or any erroneous conclusions drawn therefrom or for any consequences thereof.

All interpretations, Interpolations, Opinions and/or Classifications contained in this report falls outside our scope of accreditation.

The following parameters, where applicable, were excluded from the classification procedure: Chemical modifications, Additional fines, Fractured Faces, Soluble Salts, pH, Conductivity, Coarse Sand Ratio, Durability (COLTO: G4-G9).

The following parameters, where applicable, were assumed: Rock types were assumed to be of an Arenaceous nature with Siliceous cementing material.

Unless otherwise requested or stated, all samples will be discarded after a period of 3 months.

Deviations in Test Methods:

Civilab (Proprietary) Limited. Registration No: 1998/019071/07

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E-mail: jhb@civilab.co.za•Website: www.civilab.co.za



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Civil Engineering Testing Laboratories

Client :	JEFFARES & GREEN CONSULTING ENGINEERS	Date Received:	23/08/2013
Project :	Mzinvubu Water Project	Date Reported:	11/11/2013
Project No :	2013-B-2004	Page No. :	2 of 44

FOUNDATION INDICATOR

Laboratory Number	1	2
Field Number	C1A	C2
Client Reference		
Depth (m)	0.4-1.0	0.4-2.6
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Method A12T

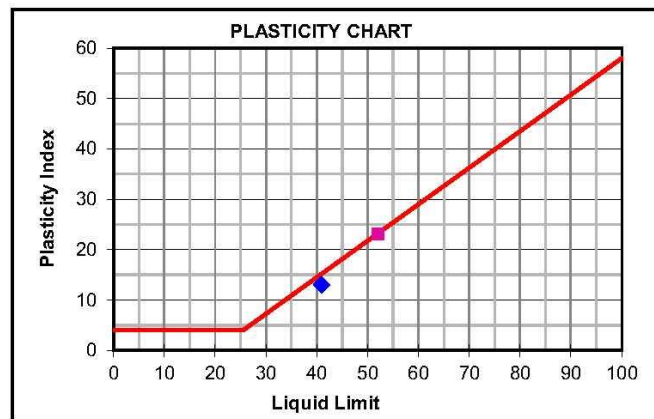
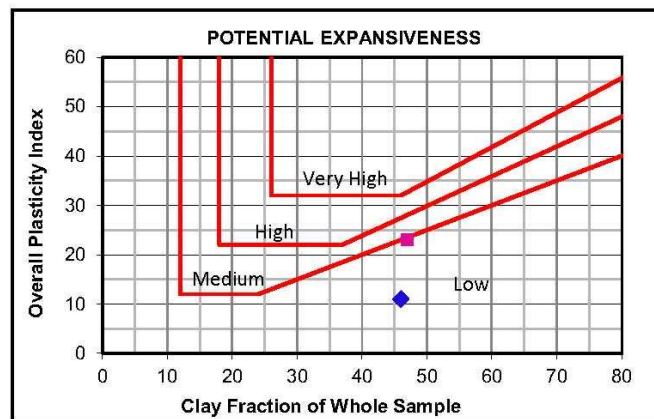
Moisture Content (%)	
Relative Density (S.G.)	2.541

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	99	100
	4.75 mm	94	100
	2.00 mm	90	100
	0.425 mm	85	100
	0.075 mm	81	76
Grading Modulus		0.44	0.24

Hydrometer Analysis - ASTM Method D422

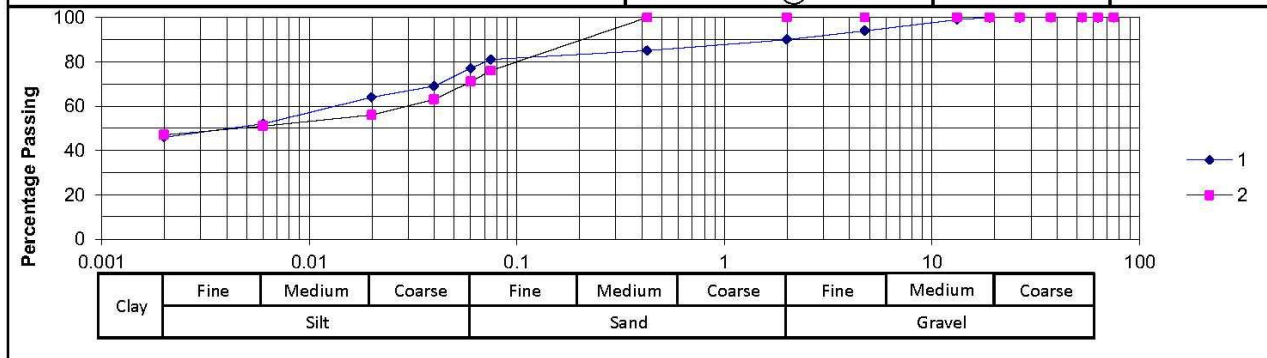
Percentage Passing	0.060 mm	77	71
	0.040 mm	69	63
	0.020 mm	64	56
	0.006 mm	52	51
	0.002 mm	46	47
Gravel	%	10	0
Sand	%	13	29
Silt	%	31	24
Clay	%	46	47



Laboratory Number		1	◆	2	■
Atterberg Limits - TMH1 Method A2, A3 & A4					
Liquid Limit	%	41		52	
Plasticity Index	%	13		23	
Linear Shrinkage	%	9.5		10.5	
Overall PI	%	11		23	

Classifications

HRB	A-7-6(11)	A-7-6(19)
Unified	ML	CH
Weston Swell @ 1 kPa		



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Civil Engineering Testing Laboratories

Client :	JEFFARES & GREEN CONSULTING ENGINEERS	Date Received:	23/08/2013
Project :	Mzinubu Water Project	Date Reported:	11/11/2013
Project No :	2013-B-2004	Page No. :	3 of 44

FOUNDATION INDICATOR

Laboratory Number	3	4
Field Number	C2A	C4A
Client Reference		
Depth (m)	0.5-1.9	0.4-2.1
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

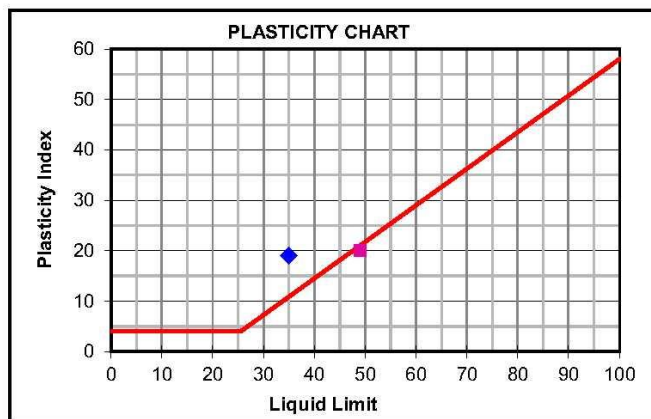
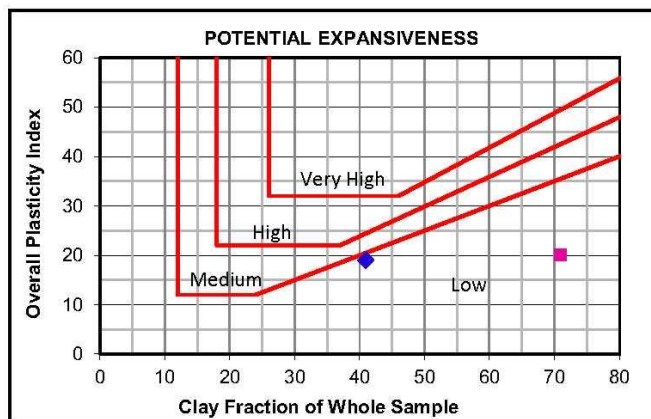
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test Report			
Sieve Size (mm)		Sample 1 (%)	Sample 2 (%)
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	100	100
	2.00 mm	100	100
	0.425 mm	99	100
0.075 mm	67	94	
Grading Modulus		0.34	0.06

Hydrometer Analysis - ASTM Method D422

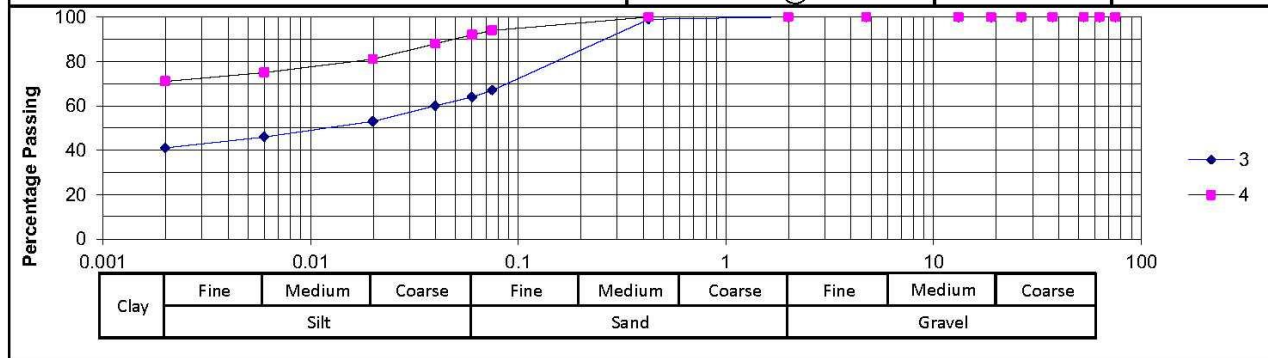
Percentage Passing	0.060 mm	64	92
	0.040 mm	60	88
	0.020 mm	53	81
	0.006 mm	46	75
	0.002 mm	41	71
Gravel	%	0	0
Sand	%	36	8
Silt	%	23	21
Clay	%	41	71



Laboratory Number		3	4
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	35	49
Plasticity Index	%	19	20
Linear Shrinkage	%	9.5	11.5
Overall PI	%	19	20

Classifications

HRB	A-6(10)	A-7-6(20)
Unified	CL	ML
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	5	6
Field Number	C5	C6
Client Reference		
Depth (m)	0.6-2.7	0.5-2.3
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

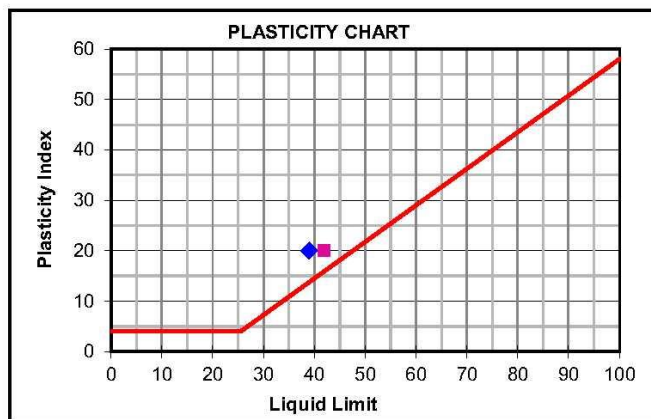
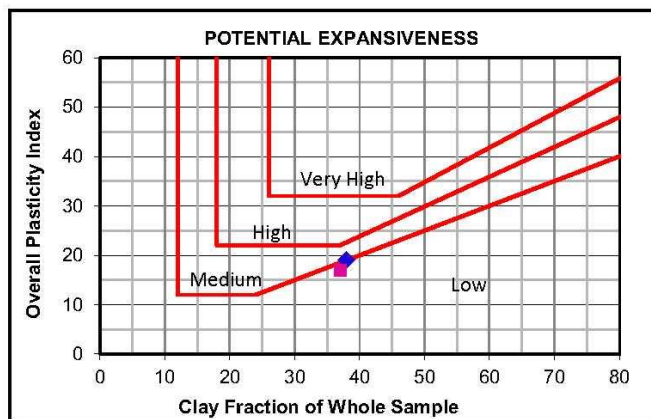
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test Report			
Sieve Size (mm)		Test Results (%)	Reference (%)
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	98	96
	2.00 mm	97	90
	0.425 mm	95	85
0.075 mm	87	79	
Grading Modulus		0.21	0.46

Hydrometer Analysis - ASTM Method D422

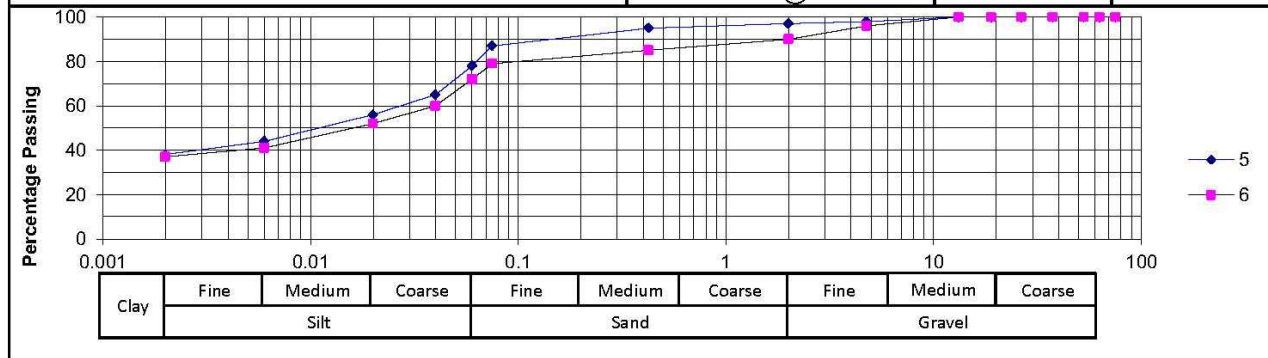
Percentage Passing	0.060 mm	78	72
	0.040 mm	65	60
	0.020 mm	56	52
	0.006 mm	44	41
	0.002 mm	38	37
Gravel	%	3	10
Sand	%	19	18
Silt	%	40	35
Clay	%	38	37



Laboratory Number	5	6	
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	39	42
Plasticity Index	%	20	20
Linear Shrinkage	%	10.0	9.5
Overall PI	%	19	17

Classifications

HRB	A-6(16)	A-7-6(16)
Unified	CL	CL
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	7	8
Field Number	C7	C8
Client Reference		
Depth (m)	0.9-2.9	0.4-2.5
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

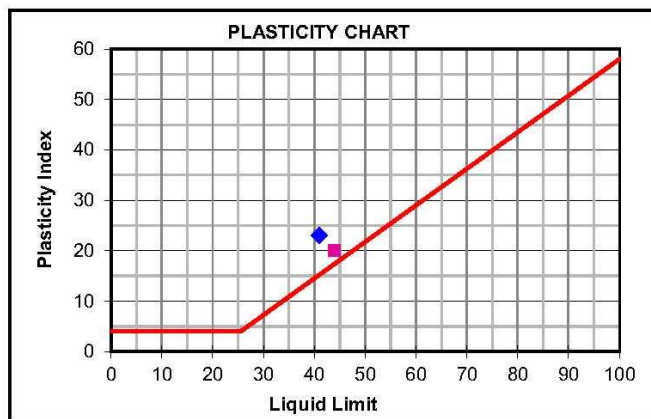
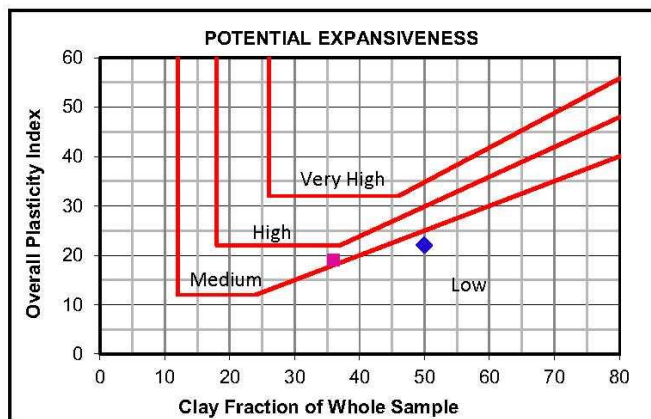
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test Report			
Sieve Size (mm)		Test 1 (%)	Test 2 (%)
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	99	100
	2.00 mm	97	100
	0.425 mm	95	97
0.075 mm	89	88	
Grading Modulus		0.19	0.15

Hydrometer Analysis - ASTM Method D422

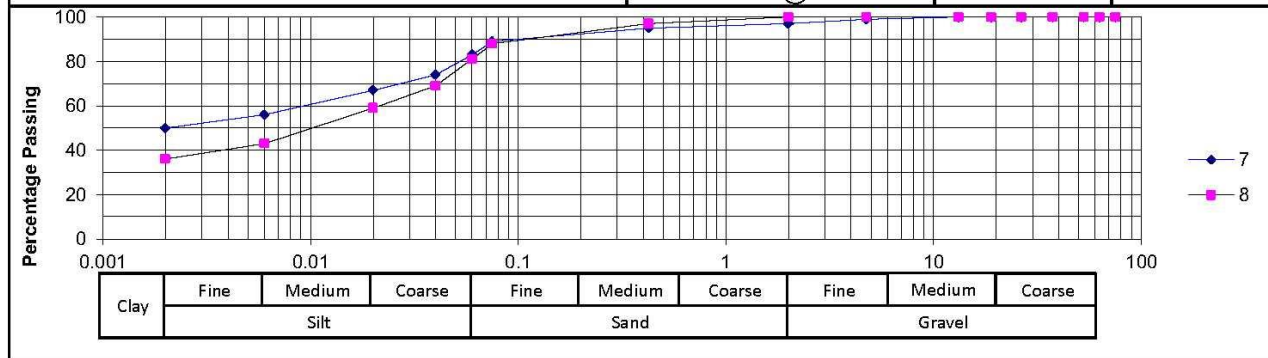
Percentage Passing	0.060 mm	83	81
	0.040 mm	74	69
	0.020 mm	67	59
	0.006 mm	56	43
	0.002 mm	50	36
Gravel	%	3	0
Sand	%	14	19
Silt	%	33	45
Clay	%	50	36



Laboratory Number		7	◆	8	■
Atterberg Limits - TMH1 Method A2, A3 & A4					
Liquid Limit	%	41		44	
Plasticity Index	%	23		20	
Linear Shrinkage	%	13.5		11.5	
Overall PI	%	22		19	

Classifications

HRB	A-7-6(20)	A-7-6(19)
Unified	CL	CL
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	9	10
Field Number	C9	C10
Client Reference		
Depth (m)	0.5-2.2	0.4-2.1
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

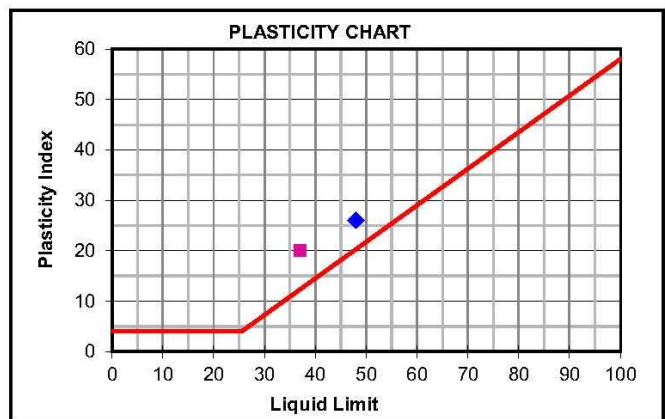
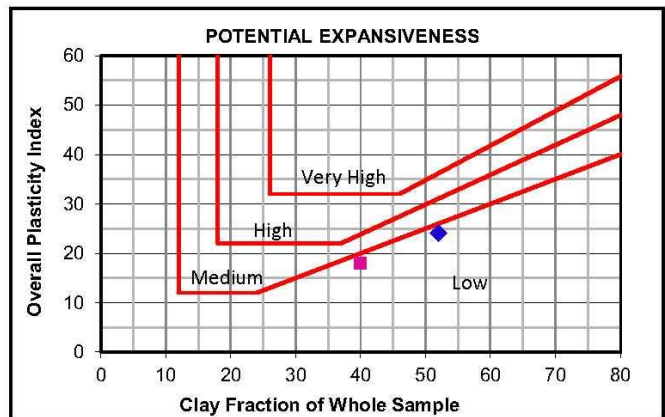
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test - Repetition (ASTM Method 700)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	98	99
	2.00 mm	97	96
	0.425 mm	94	91
0.075 mm	85	69	
Grading Modulus		0.24	0.44

Hydrometer Analysis - ASTM Method D422

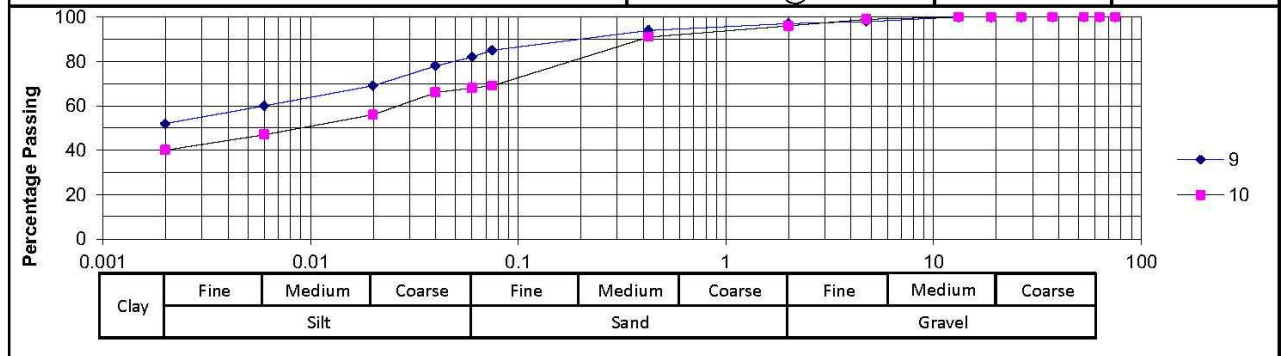
Percentage Passing	0.060 mm	82	68
	0.040 mm	78	66
	0.020 mm	69	56
	0.006 mm	60	47
	0.002 mm	52	40
Gravel	%	3	4
Sand	%	15	28
Silt	%	30	28
Clay	%	52	40



Laboratory Number		9	10
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	48	37
Plasticity Index	%	26	20
Linear Shrinkage	%	12.5	10.0
Overall PI	%	24	18

Classifications

HRB	A-7-6(20)	A-6(12)
Unified	CL	CL
Weston Swell @ 1 kPa		



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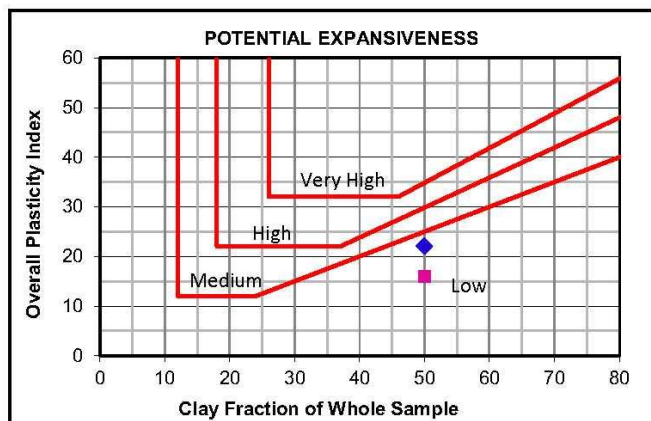
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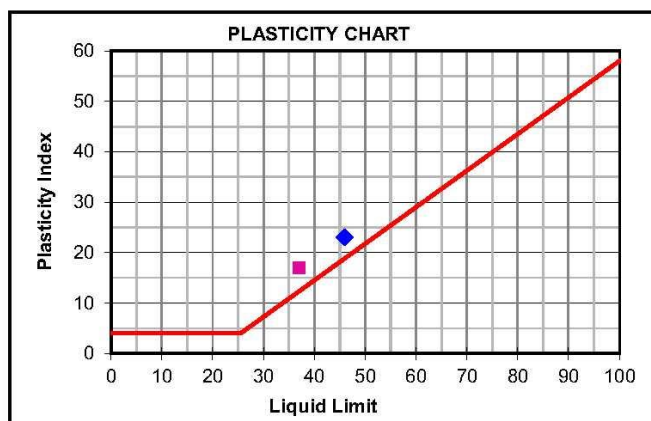
FOUNDATION INDICATOR

Laboratory Number	11	12
Field Number		C12
Client Reference		
Depth (m)	0.4-2.5	0.5-2.6
Position	Mix C2 + C4A + C7 + C8 + C10	
Coordinates	X	
	Y	
Description		Reddish Br. Colluvial Clayey Sand/
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		



Moisture Content & Relative Density-TMH1 Metod A12T		
Moisture Content (%)		
Relative Density (S.G.)	2.253	

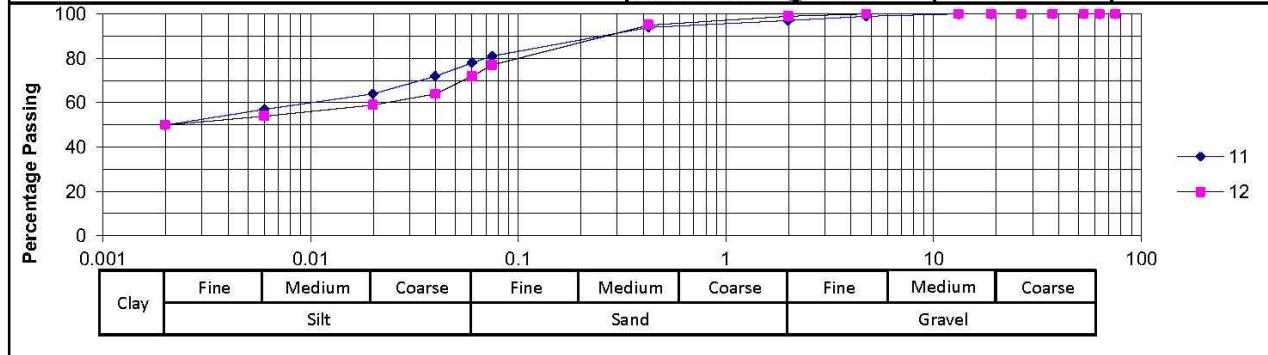
Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	99	100
	2.00 mm	97	99
	0.425 mm	94	95
	0.075 mm	81	77
Grading Modulus	0.28	0.29	



Hydrometer Analysis - ASTM Method D422			
Percentage Passing	0.060 mm	78	72
	0.040 mm	72	64
	0.020 mm	64	59
	0.006 mm	57	54
	0.002 mm	50	50
Gravel	%	3	1
Sand	%	19	27
Silt	%	28	22
Clay	%	50	50

Laboratory Number		11	12
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	46	37
Plasticity Index	%	23	17
Linear Shrinkage	%	11.5	10.0
Overall PI	%	22	16

Classifications		
HRB	A-7-6(19)	A-6(12)
Unified	CL	CL
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	13	14
Field Number	C15	C16
Client Reference		
Depth (m)	0.4-1.8	0.5-1.6
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

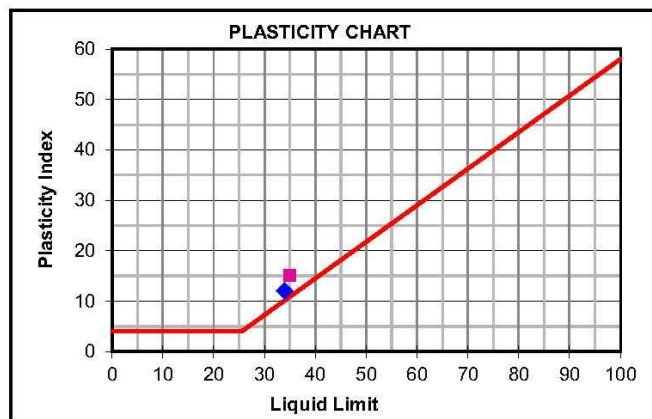
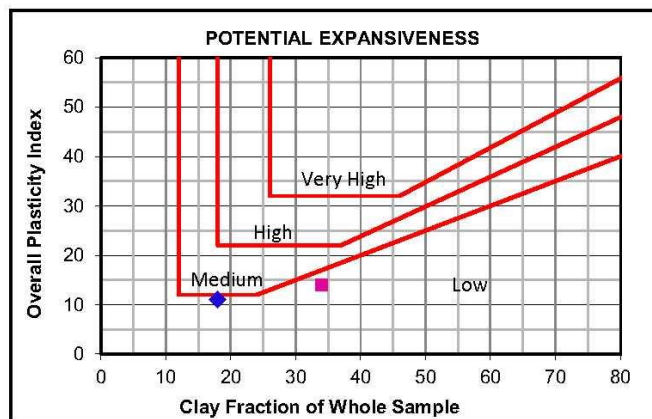
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Grading Analysis (ASTM D 1544) - 100% Passing 75mm Nominal Size			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	99	100
	4.75 mm	98	99
	2.00 mm	97	98
	0.425 mm	93	95
0.075 mm	76	78	
Grading Modulus		0.34	0.29

Hydrometer Analysis - ASTM Method D422

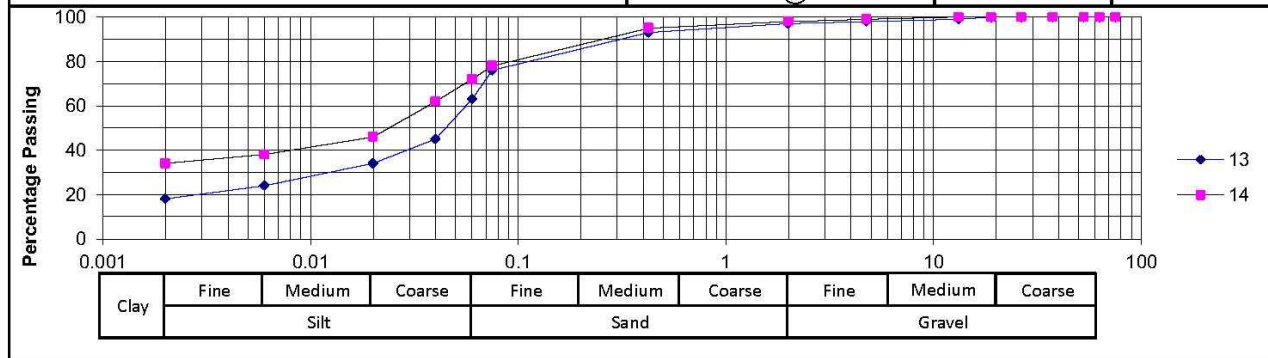
Percentage Passing	0.060 mm	63	72
	0.040 mm	45	62
	0.020 mm	34	46
	0.006 mm	24	38
	0.002 mm	18	34
Gravel	%	3	2
Sand	%	34	26
Silt	%	45	38
Clay	%	18	34



Laboratory Number		13	◆	14	■
Atterberg Limits - TMH1 Method A2, A3 & A4					
Liquid Limit	%	34		35	
Plasticity Index	%	12		15	
Linear Shrinkage	%	7.5		7.5	
Overall P	%	11		14	

Classifications

HRB	A-6(8)	A-6(11)
Unified	CL	CL
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	15	16
Field Number	C18	C20
Client Reference		
Depth (m)	0.3-2.9	0.3-2.2
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

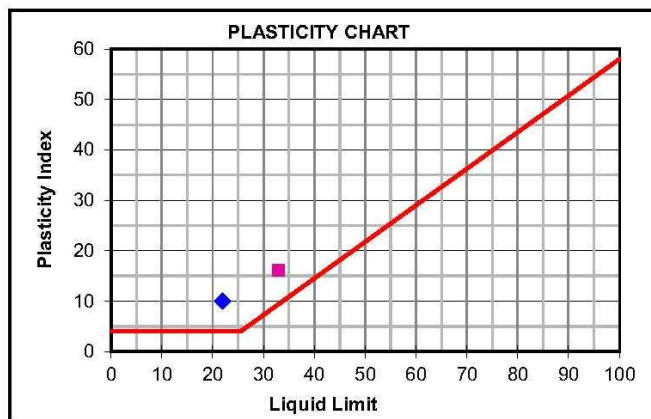
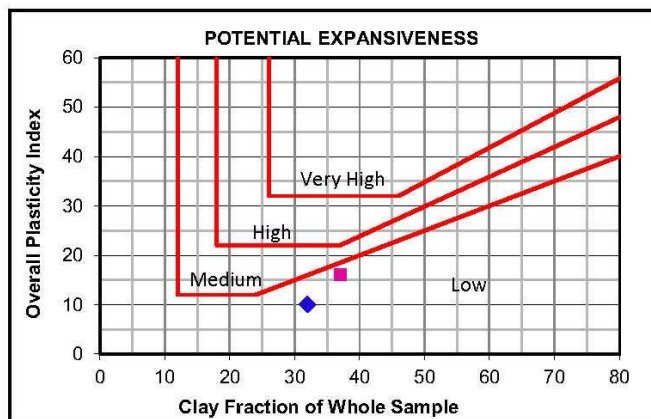
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test Report			
Sieve Size (mm)		Test Results (%)	Reference (%)
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	100	100
	2.00 mm	99	100
	0.425 mm	98	98
0.075 mm	65	66	
Grading Modulus		0.38	0.36

Hydrometer Analysis - ASTM Method D422

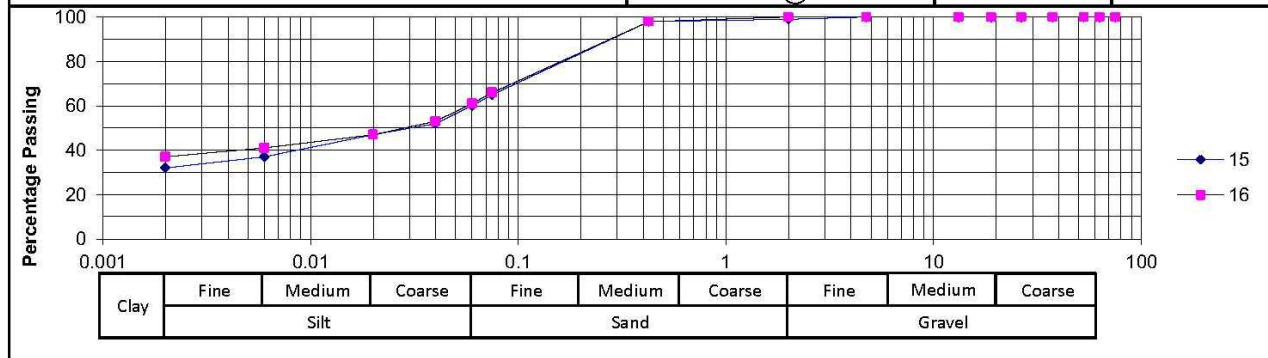
Percentage Passing	0.060 mm	60	61
	0.040 mm	52	53
	0.020 mm	47	47
	0.006 mm	37	41
	0.002 mm	32	37
Gravel	%	1	0
Sand	%	39	39
Silt	%	28	24
Clay	%	32	37



Laboratory Number		15	◆	16	■
Atterberg Limits - TMH1 Method A2, A3 & A4					
Liquid Limit	%	22		33	
Plasticity Index	%	10		16	
Linear Shrinkage	%	5.5		8.0	
Overall PI	%	10		16	

Classifications

HRB	A-4(3)	A-6(8)
Unified	CL	CL
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	17	18
Field Number	C22	C23
Client Reference		
Depth (m)	0.3-2.6	0.25-1.7
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

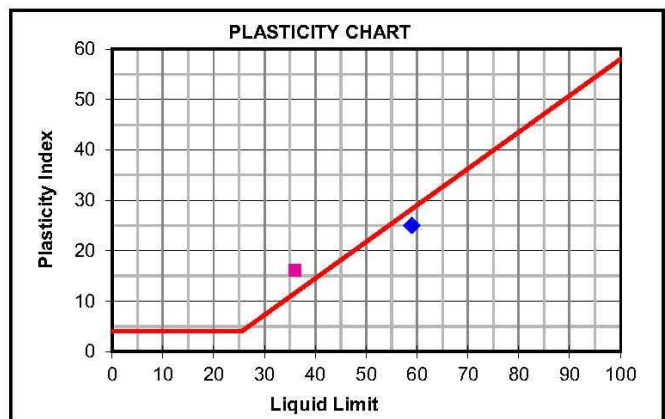
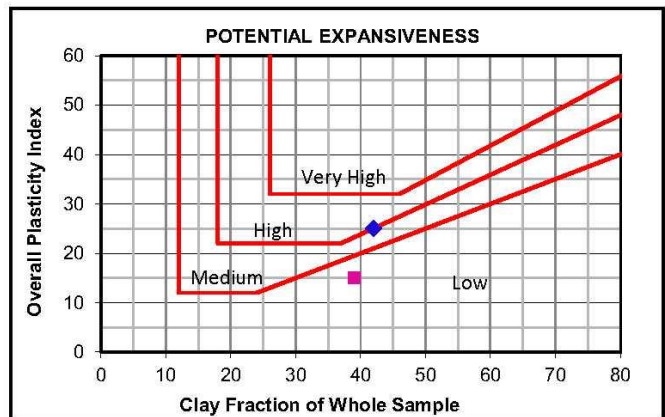
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test: Repetition 1 and 2 (Method 70.1)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	100	97
	2.00 mm	100	96
	0.425 mm	100	93
0.075 mm	97	72	
Grading Modulus		0.03	0.39

Hydrometer Analysis - ASTM Method D422

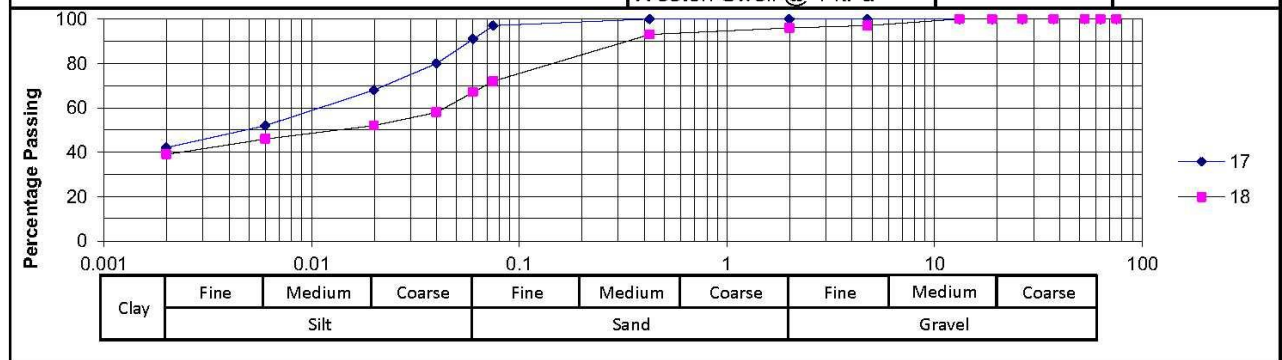
Percentage Passing	0.060 mm	91	67
	0.040 mm	80	58
	0.020 mm	68	52
	0.006 mm	52	46
	0.002 mm	42	39
Gravel	%	0	4
Sand	%	9	29
Silt	%	49	28
Clay	%	42	39



Laboratory Number		17	18
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	59	36
Plasticity Index	%	25	16
Linear Shrinkage	%	10.5	8.5
Overall PI	%	25	15

Classifications

HRB	A-7-5(20)	A-6(10)
Unified	ML	CL
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	19	20
Field Number	C25	C28
Client Reference		
Depth (m)	0.3-0.9	0.5-2.6
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

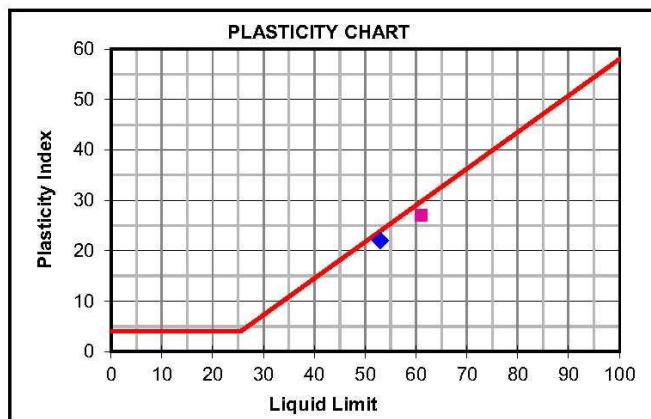
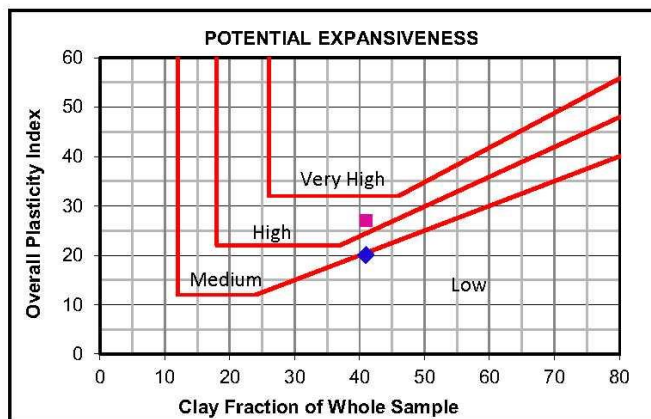
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test Report			
Sieve Size (mm)		Actual Percent Passing	Required Percent Passing
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	99	100
	2.00 mm	97	100
	0.425 mm	93	100
0.075 mm	87	98	
Grading Modulus		0.23	0.02

Hydrometer Analysis - ASTM Method D422

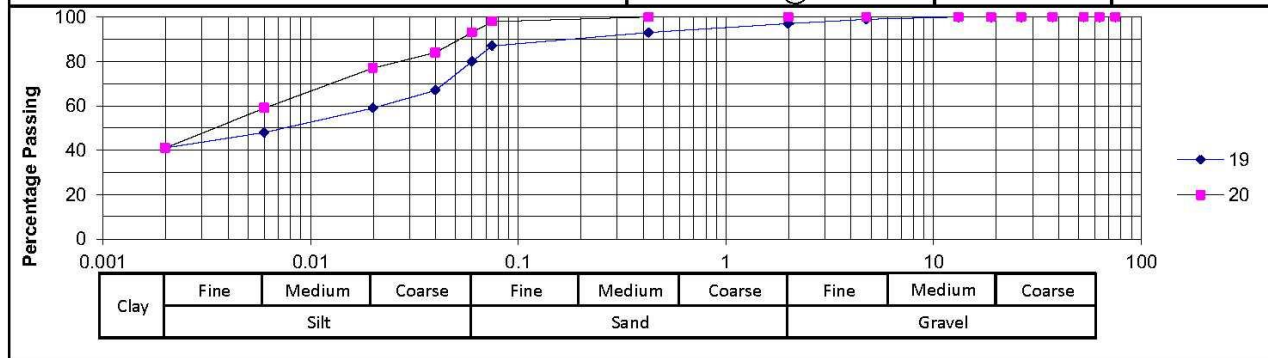
Percentage Passing	0.060 mm	80	93
	0.040 mm	67	84
	0.020 mm	59	77
	0.006 mm	48	59
	0.002 mm	41	41
Gravel	%	3	0
Sand	%	17	7
Silt	%	39	52
Clay	%	41	41



Laboratory Number		19	20
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	53	61
Plasticity Index	%	22	27
Linear Shrinkage	%	10.5	15.5
Overall PI	%	20	27

Classifications

HRB	A-7-5(20)	A-7-5(20)
Unified	ML	ML
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	21	22
Field Number	C30	
Client Reference		
Depth (m)	0.5-2.1	-
Position		Mix C12 + C18 + C22 + C28 + C30
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

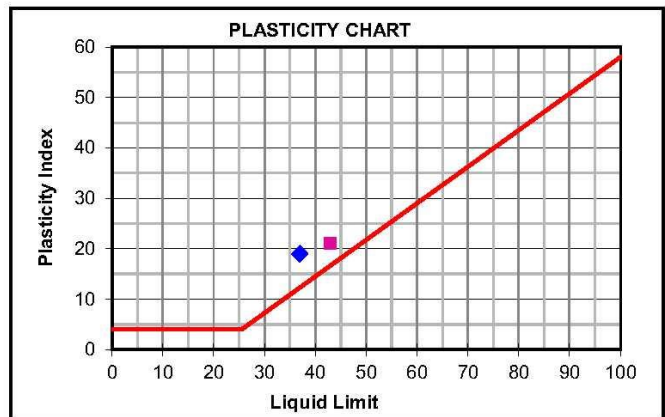
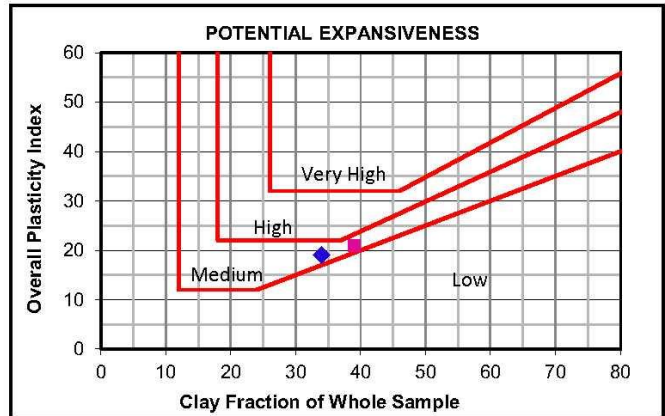
Moisture Content (%)		
Relative Density (S.G.)		2.657

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Grading Analysis (ASTM D 1544) - 100% Passing 75mm (No. 20)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	99	100
	2.00 mm	98	100
	0.425 mm	98	100
0.075 mm	65	76	
Grading Modulus		0.39	0.24

Hydrometer Analysis - ASTM Method D422

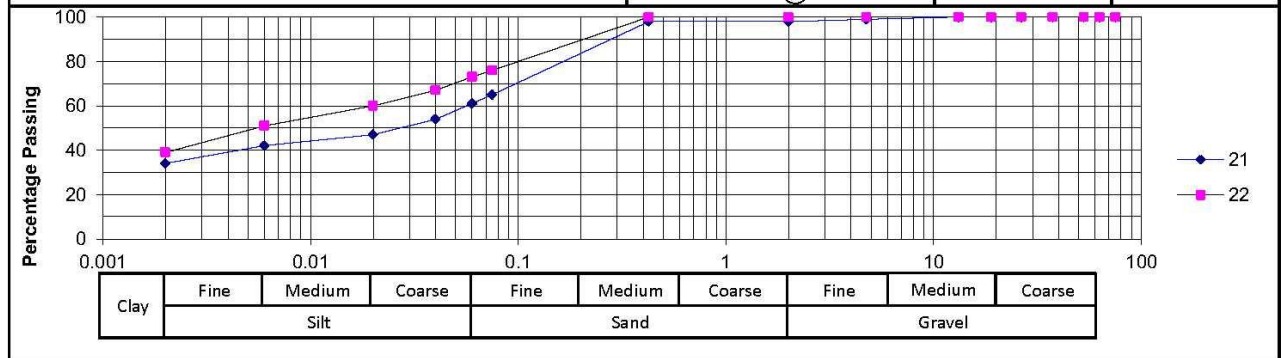
Percentage Passing	0.060 mm	61	73
	0.040 mm	54	67
	0.020 mm	47	60
	0.006 mm	42	51
	0.002 mm	34	39
Gravel	%	2	0
Sand	%	37	27
Silt	%	27	34
Clay	%	34	39



Laboratory Number		21	22
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	37	43
Plasticity Index	%	19	21
Linear Shrinkage	%	8.0	11.5
Overall PI	%	19	21

Classifications

HRB	A-6(10)	A-7-6(16)
Unified	CL	CL
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	23	24
Field Number	F5	F6
Client Reference		
Depth (m)	0.25-1.20	0.4-1.2
Position		
Coordinates	X	
	Y	
Description	Weathered Mudrock/ Sandstone	
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

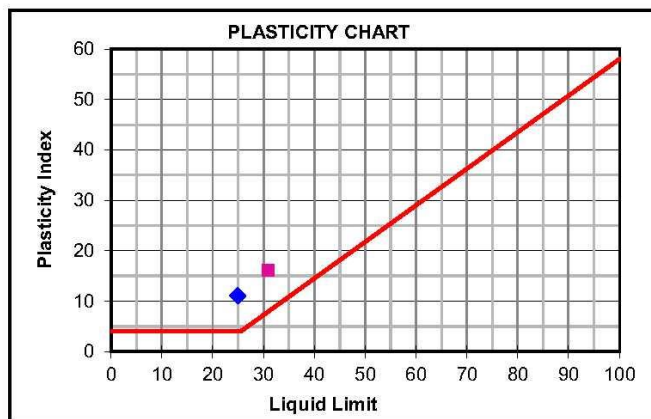
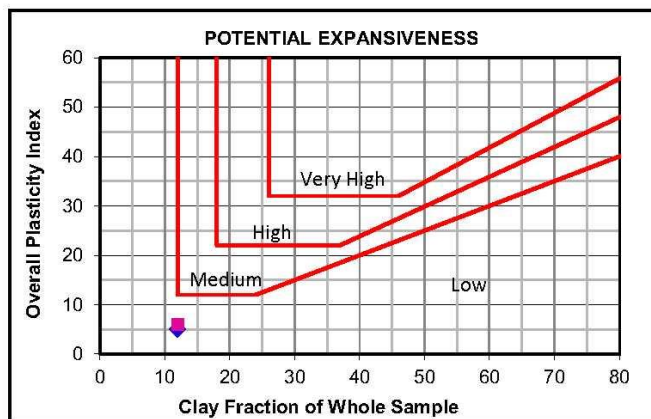
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	98
	4.75 mm	90	71
	2.00 mm	69	54
	0.425 mm	42	36
Grading Modulus	0.075 mm	29	28
		1.6	1.82

Hydrometer Analysis - ASTM Method D422

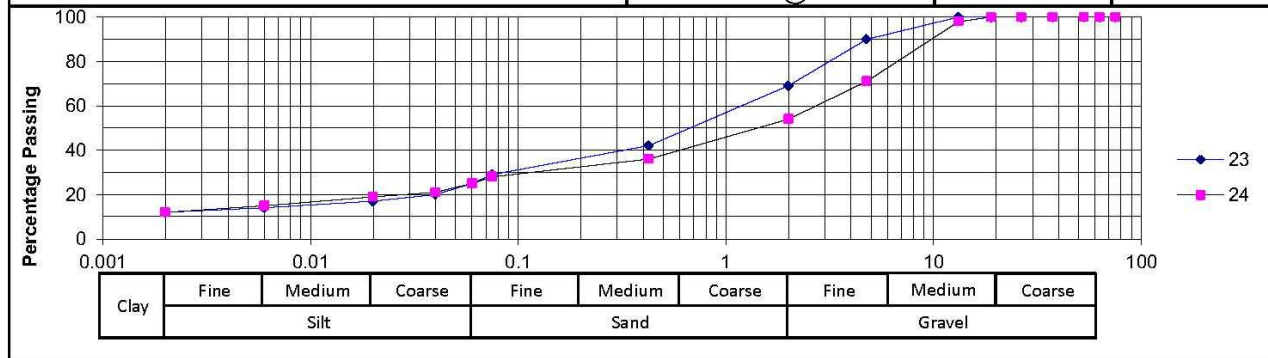
Percentage Passing	0.060 mm	25	25
	0.040 mm	20	21
	0.020 mm	17	19
	0.006 mm	14	15
	0.002 mm	12	12
Gravel	%	31	46
Sand	%	44	29
Silt	%	13	13
Clay	%	12	12



Laboratory Number		23	24
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	25	31
Plasticity Index	%	11	16
Linear Shrinkage	%	5.5	6.5
Overall PI	%	5	6

Classifications

HRB	A-2-6(0)	A-2-6(1)
Unified	SC	SC
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	25	26
Field Number	F8	F10
Client Reference		
Depth (m)	0.6-1.6	Channel 0.9m
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

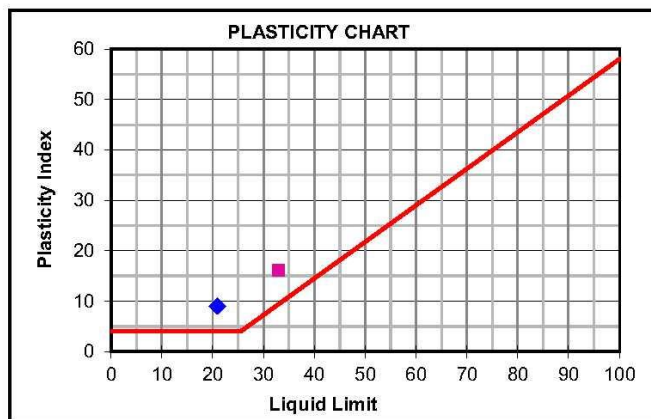
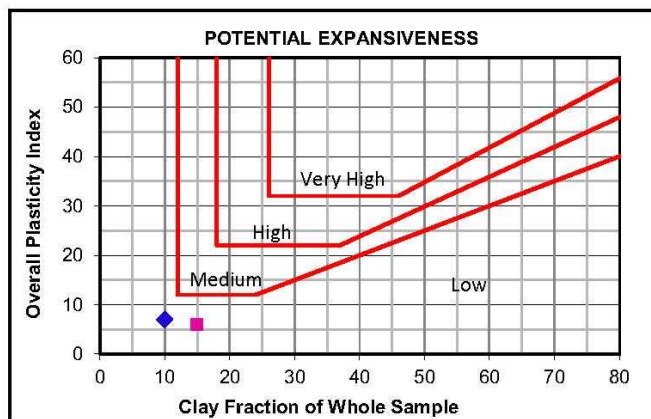
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Grading Analysis (ASTM D 1544) (mm) (Percent Passing)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	97	99
	4.75 mm	87	81
	2.00 mm	84	59
	0.425 mm	80	39
0.075 mm	31	32	
Grading Modulus		1.05	1.7

Hydrometer Analysis - ASTM Method D422

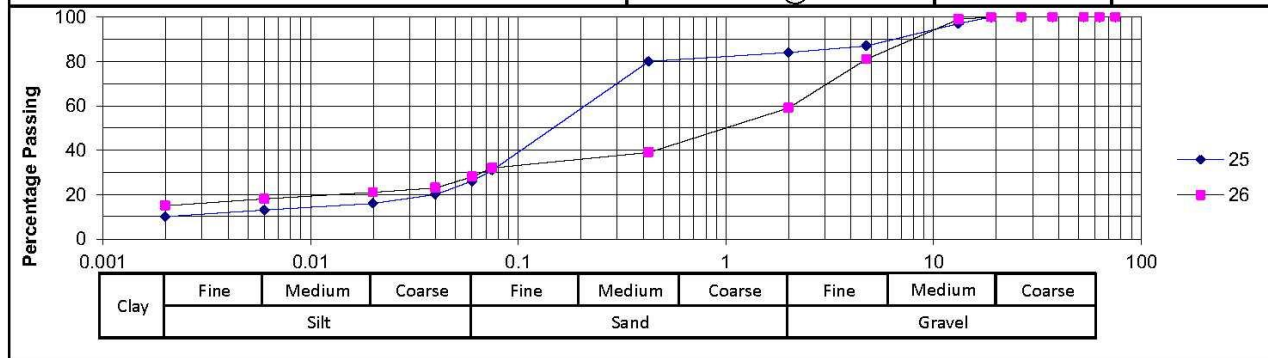
Percentage Passing	0.060 mm	26	28
	0.040 mm	20	23
	0.020 mm	16	21
	0.006 mm	13	18
	0.002 mm	10	15
Gravel	%	16	41
Sand	%	58	31
Silt	%	16	13
Clay	%	10	15



Laboratory Number		25	◆	26	■
Atterberg Limits - TMH1 Method A2, A3 & A4					
Liquid Limit	%	21		33	
Plasticity Index	%	9		16	
Linear Shrinkage	%	3.5		8.5	
Overall PI	%	7		6	

Classifications

HRB	A-2-4(0)	A-2-6(1)
Unified	SC	SC
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	27	28
Field Number	F12	F13
Client Reference		
Depth (m)	0.3-0.6	0.25-0.95
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

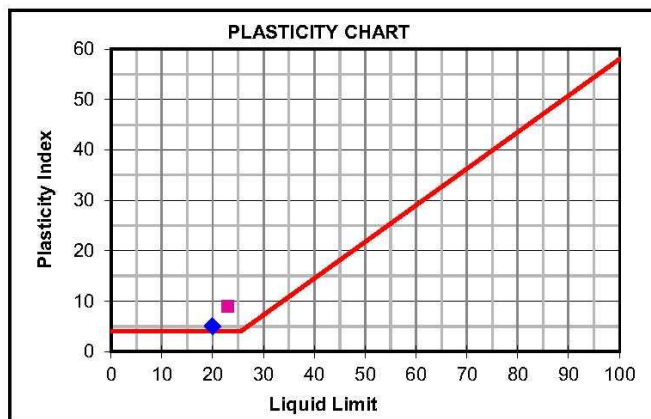
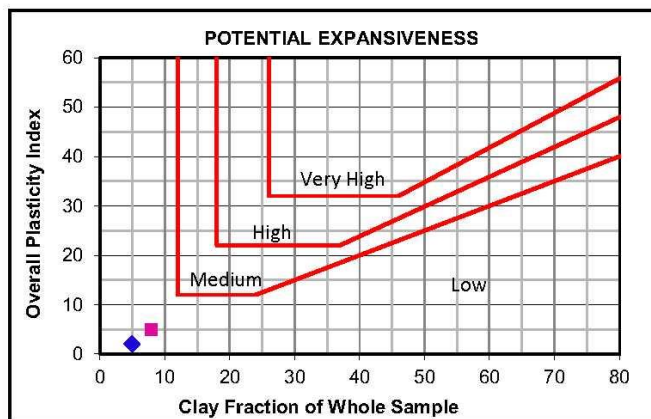
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Grading Analysis (ASTM D 1557)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	93	98
	4.75 mm	71	79
	2.00 mm	56	71
	0.425 mm	43	59
0.075 mm	26	23	
Grading Modulus		1.75	1.47

Hydrometer Analysis - ASTM Method D422

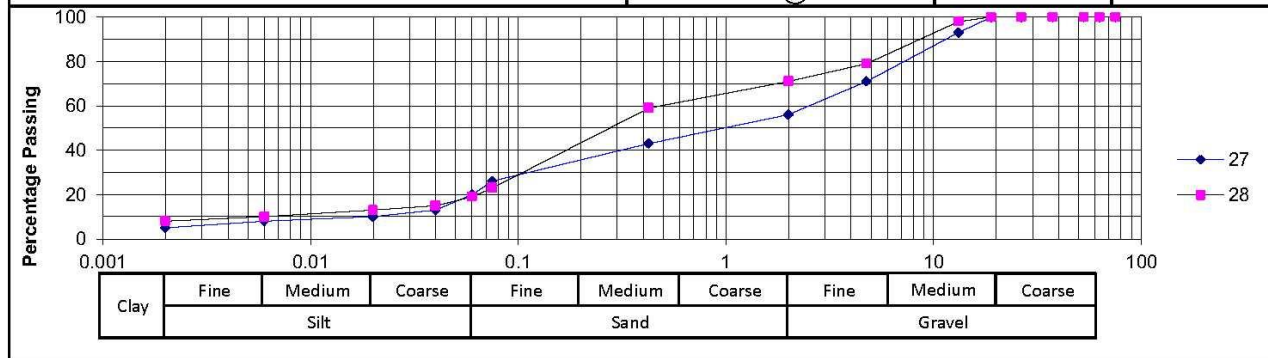
Percentage Passing	0.060 mm	20	19
	0.040 mm	13	15
	0.020 mm	10	13
	0.006 mm	8	10
	0.002 mm	5	8
Gravel	%	44	29
Sand	%	36	52
Silt	%	15	11
Clay	%	5	8



Laboratory Number		27	28
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	20	23
Plasticity Index	%	5	9
Linear Shrinkage	%	3.5	4.0
Overall PI	%	2	5

Classifications

HRB	A-2-4(0)	A-2-4(0)
Unified	SC-SM	SC
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	29	30
Field Number		F25
Client Reference		
Depth (m)	-	0.9-1.2
Position	Mixed Sample F5 + F8 + F10	
Coordinates	X	
	Y	
Description		Weathered Mudrock/ Sadstone
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

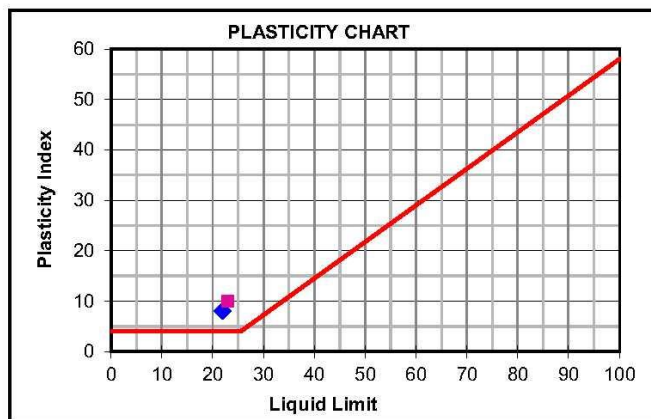
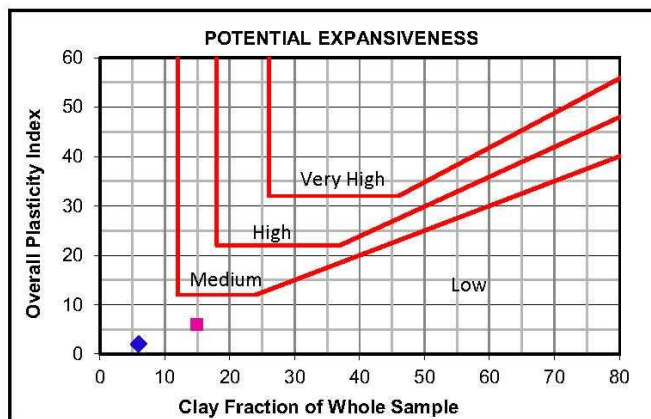
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis (ASTM) - Topgrading 75mm Maximum Size			
Percentage Passing	75.0 mm	98	100
	63.0 mm	95	100
	53.0 mm	91	100
	37.5 mm	84	100
	26.5 mm	77	100
	19.0 mm	71	100
	13.2 mm	68	99
	4.75 mm	45	82
	2.00 mm	36	71
	0.425 mm	30	61
0.075 mm	15	30	
Grading Modulus		2.19	1.38

Hydrometer Analysis - ASTM Method D422

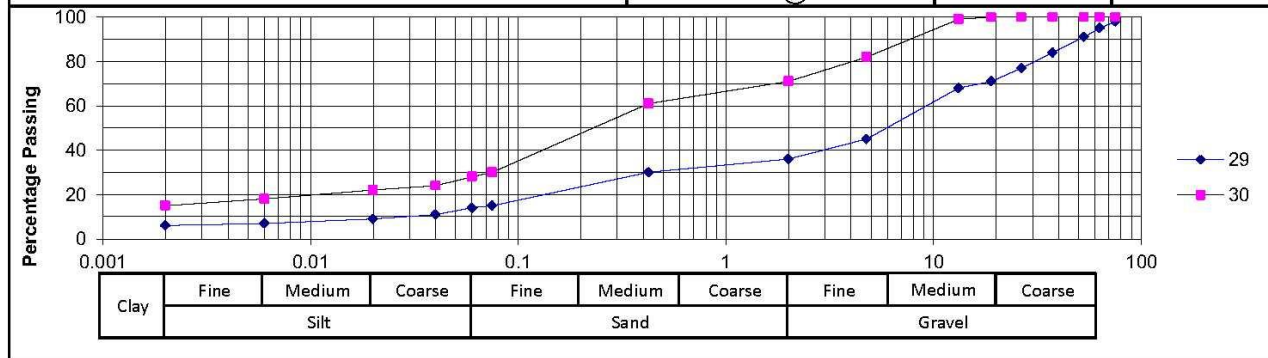
Percentage Passing	0.060 mm	14	28
	0.040 mm	11	24
	0.020 mm	9	22
	0.006 mm	7	18
	0.002 mm	6	15
Gravel	%	64	29
Sand	%	22	43
Silt	%	8	13
Clay	%	6	15



Laboratory Number		29	30
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	22	23
Plasticity Index	%	8	10
Linear Shrinkage	%	4.0	4.0
Overall PI	%	2	6

Classifications

HRB	A-2-4(0)	A-2-4(0)
Unified	GC	SC
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	31	32
Field Number	F28	F29
Client Reference		
Depth (m)	0.00-1.5	0.00-0.6
Position		
Coordinates	X	
	Y	
Description		Weathered Mudrock / Sandstone
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

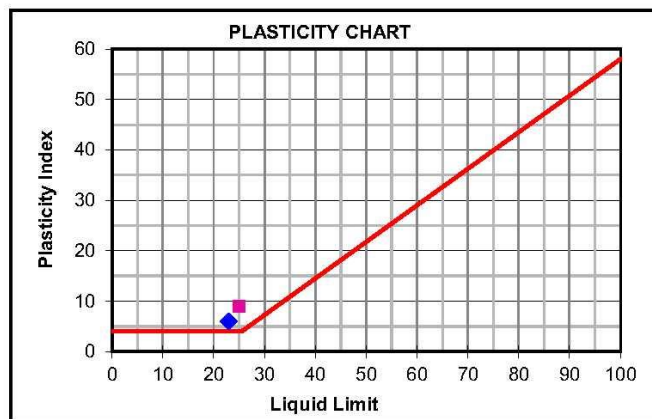
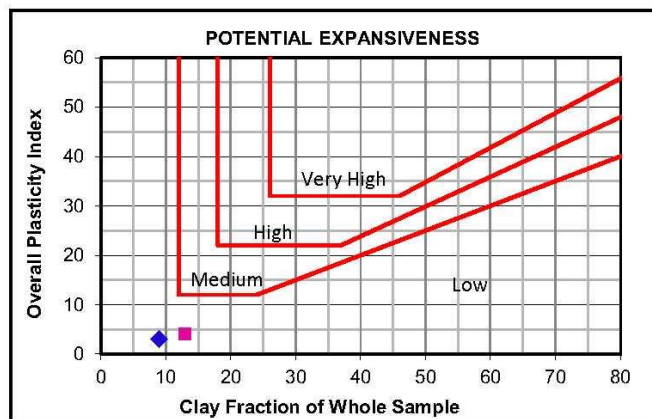
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test Report			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	96	94
	2.00 mm	82	77
	0.425 mm	57	45
	0.075 mm	45	32
Grading Modulus		1.16	1.46

Hydrometer Analysis - ASTM Method D422

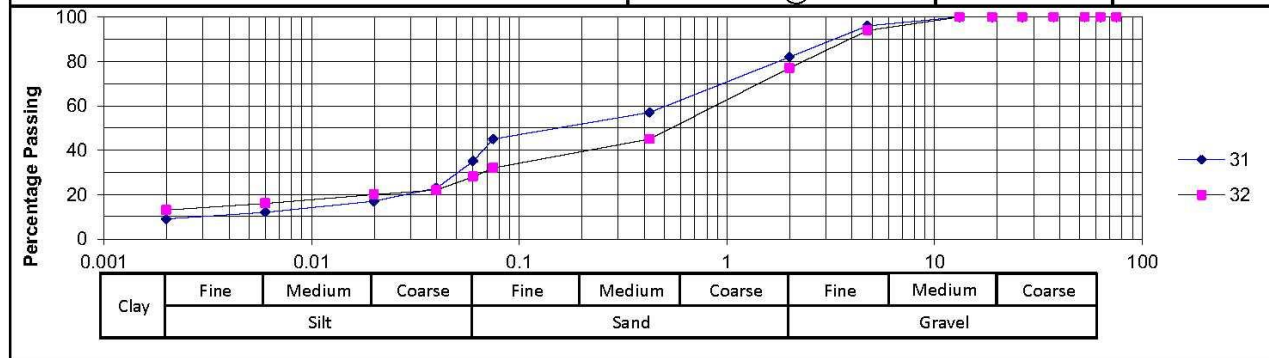
Percentage Passing	0.060 mm	35	28
	0.040 mm	23	22
	0.020 mm	17	20
	0.006 mm	12	16
	0.002 mm	9	13
Gravel	%	18	23
Sand	%	47	49
Silt	%	26	15
Clay	%	9	13



Laboratory Number		31	32
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	23	25
Plasticity Index	%	6	9
Linear Shrinkage	%	4.0	6.0
Overall PI	%	3	4

Classifications

HRB	A-4(0)	A-2-4(0)
Unified	SC-SM	SC
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	33	34
Field Number	F31	F33
Client Reference		
Depth (m)	0.4-1.0	0.4-1.0
Position		
Coordinates	X	
	Y	
Description		Weathered Mudrock/ Sandstone
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

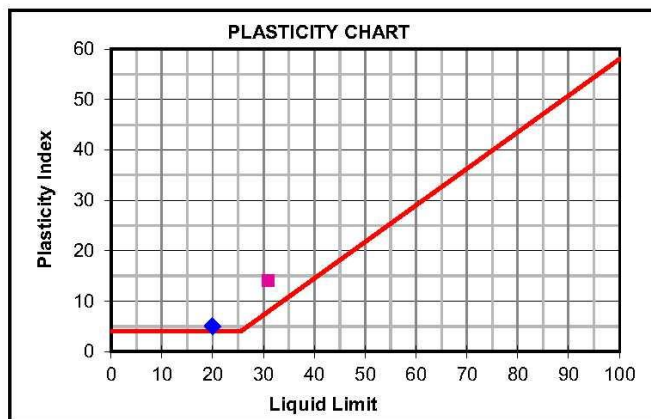
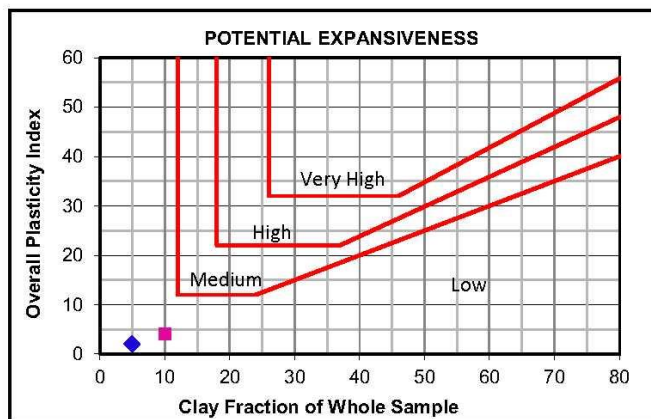
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis (wet) (Population) - 4mm Method (A)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	98	100
	4.75 mm	76	75
	2.00 mm	57	43
	0.425 mm	38	25
0.075 mm	30	17	
Grading Modulus		1.75	2.15

Hydrometer Analysis - ASTM Method D422

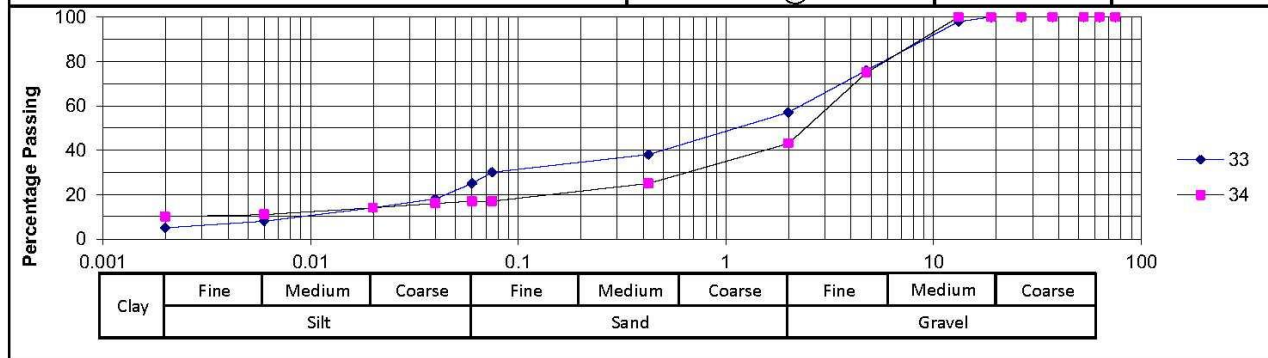
Percentage Passing	0.060 mm	25	17
	0.040 mm	18	16
	0.020 mm	14	14
	0.006 mm	8	11
	0.002 mm	5	10
Gravel	%	43	57
Sand	%	32	26
Silt	%	20	7
Clay	%	5	10



Laboratory Number		33	34
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	20	31
Plasticity Index	%	5	14
Linear Shrinkage	%	3.5	7.5
Overall PI	%	2	4

Classifications

HRB	A-2-4(0)	A-2-6(0)
Unified	SC-SM	SC
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	35	36
Field Number	F34	F37
Client Reference		
Depth (m)	0.1-0.8	0.0-1.5
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

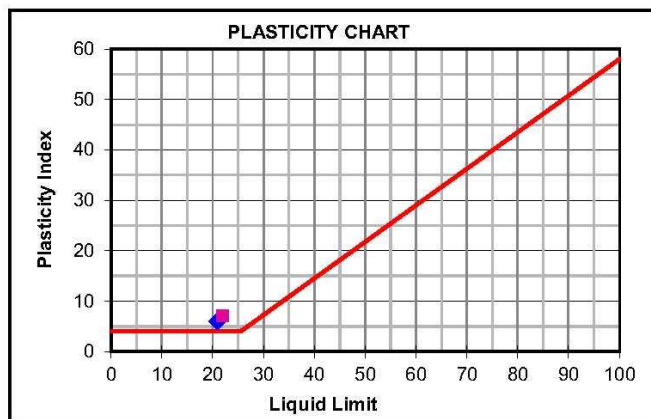
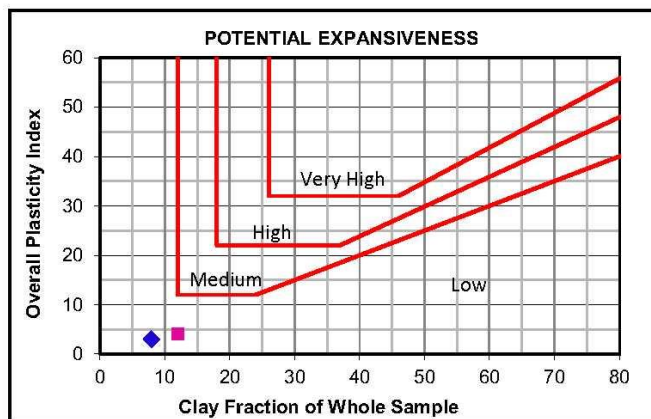
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Grading Analysis (ASTM D 1557) (mm) (Percent Passing)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	99
	4.75 mm	85	85
	2.00 mm	68	72
	0.425 mm	55	59
0.075 mm	38	33	
Grading Modulus		1.39	1.36

Hydrometer Analysis - ASTM Method D422

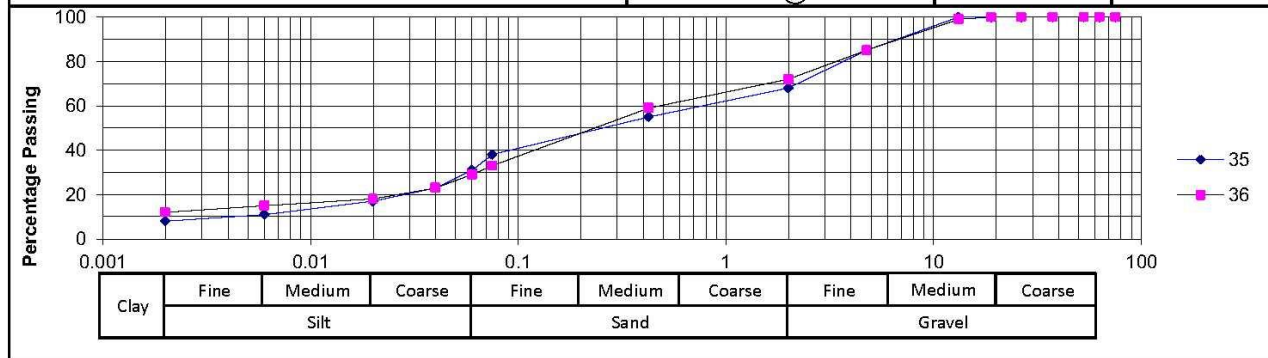
Percentage Passing	0.060 mm	31	29
	0.040 mm	23	23
	0.020 mm	17	18
	0.006 mm	11	15
	0.002 mm	8	12
Gravel	%	32	28
Sand	%	37	43
Silt	%	23	17
Clay	%	8	12



Laboratory Number		35	◆	36	■
Atterberg Limits - TMH1 Method A2, A3 & A4					
Liquid Limit	%	21		22	
Plasticity Index	%	6		7	
Linear Shrinkage	%	4.0		4.0	
Overall PI	%	3		4	

Classifications

HRB	A-4(0)	A-2-4(0)
Unified	SC-SM	SC-SM
Weston Swell @ 1 kPa		



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FOUNDATION INDICATOR

Laboratory Number	37	38
Field Number	F37A	F39
Client Reference		
Depth (m)	Channel	0.2-1.0
Position		
Coordinates	X	
	Y	
Description		Weathered Mudrock/ Sandstone
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

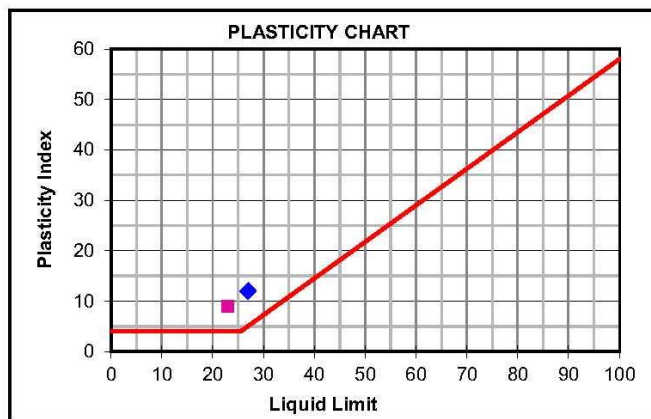
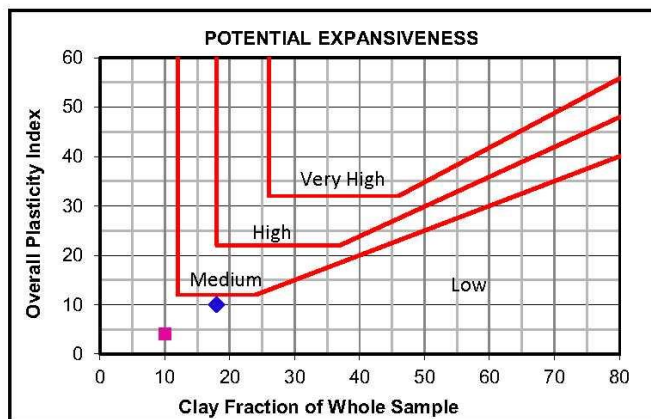
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test Report			
Sieve Size (mm)		Test Results (%)	Specification (%)
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	99	73
	2.00 mm	95	57
	0.425 mm	86	40
0.075 mm	66	29	
Grading Modulus		0.53	1.74

Hydrometer Analysis - ASTM Method D422

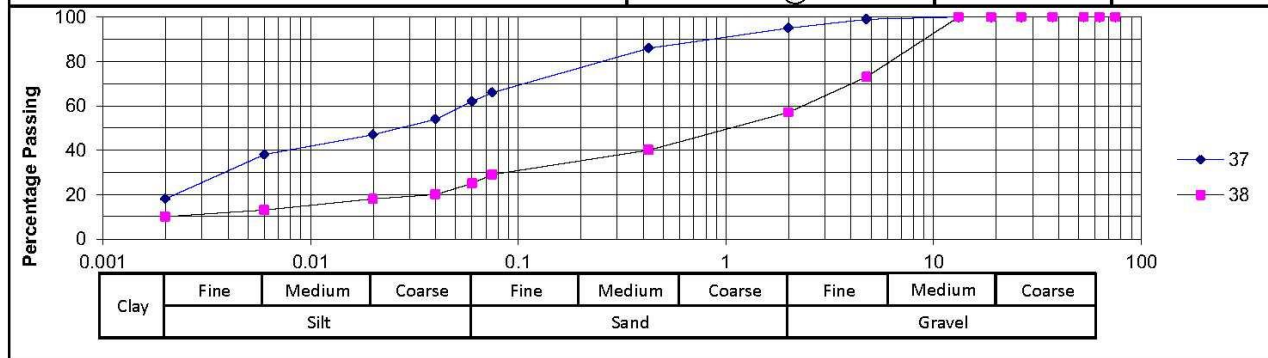
Percentage Passing	0.060 mm	62	25
	0.040 mm	54	20
	0.020 mm	47	18
	0.006 mm	38	13
	0.002 mm	18	10
Gravel	%	5	43
Sand	%	33	32
Silt	%	44	15
Clay	%	18	10



Laboratory Number		37	38
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	27	23
Plasticity Index	%	12	9
Linear Shrinkage	%	6.0	5.5
Overall PI	%	10	4

Classifications

HRB	A-6(5)	A-2-4(0)
Unified	CL	SC
Weston Swell @ 1 kPa		



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Client :	JEFFARES & GREEN CONSULTING ENGINEERS	Date Received:	23/08/2013
Project :	Mzinubu Water Project	Date Reported:	11/11/2013
Project No :	2013-B-2004	Page No. :	21 of 44

FOUNDATION INDICATOR

Laboratory Number	39	
Field Number		
Client Reference		
Depth (m)	-	
Position	Mix F25 + F29 + F34 + F37 + F39	
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

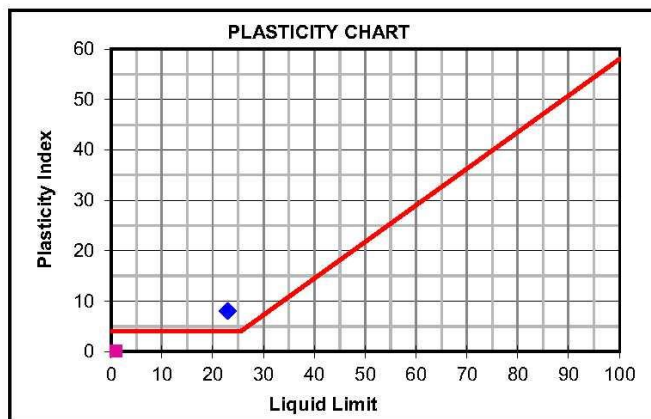
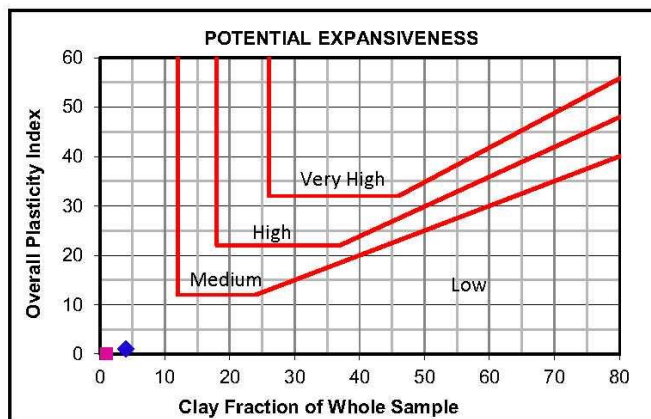
Moisture Content (%)	
Relative Density (S.G.)	2.717

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis (ASTM 1198) - Maximum Allowance (%)		
Percentage Passing	75.0 mm	97
	63.0 mm	95
	53.0 mm	92
	37.5 mm	87
	26.5 mm	80
	19.0 mm	76
	13.2 mm	73
	4.75 mm	44
	2.00 mm	28
	0.425 mm	18
0.075 mm	12	
Grading Modulus		2.42

Hydrometer Analysis - ASTM Method D422

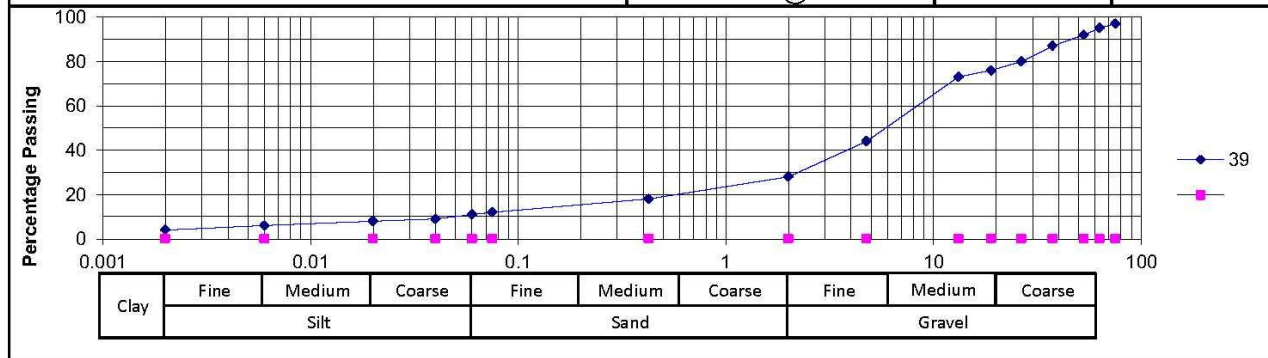
Percentage Passing	0.060 mm	11
	0.040 mm	9
	0.020 mm	8
	0.006 mm	6
	0.002 mm	4
Gravel	%	72
Sand	%	17
Silt	%	7
Clay	%	4



Laboratory Number	39	◆	■
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	23	
Plasticity Index	%	8	
Linear Shrinkage	%	5.5	
Overall PI	%	1	

Classifications

HRB	A-2-4(0)
Unified	GP-GC
Weston Swell @ 1 kPa	



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Project : Mzinvubu Water Project

Date Reported: 11/11/2013

Project No: 2013-B-2004

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MOISTURE DENSITY RELATIONSHIP

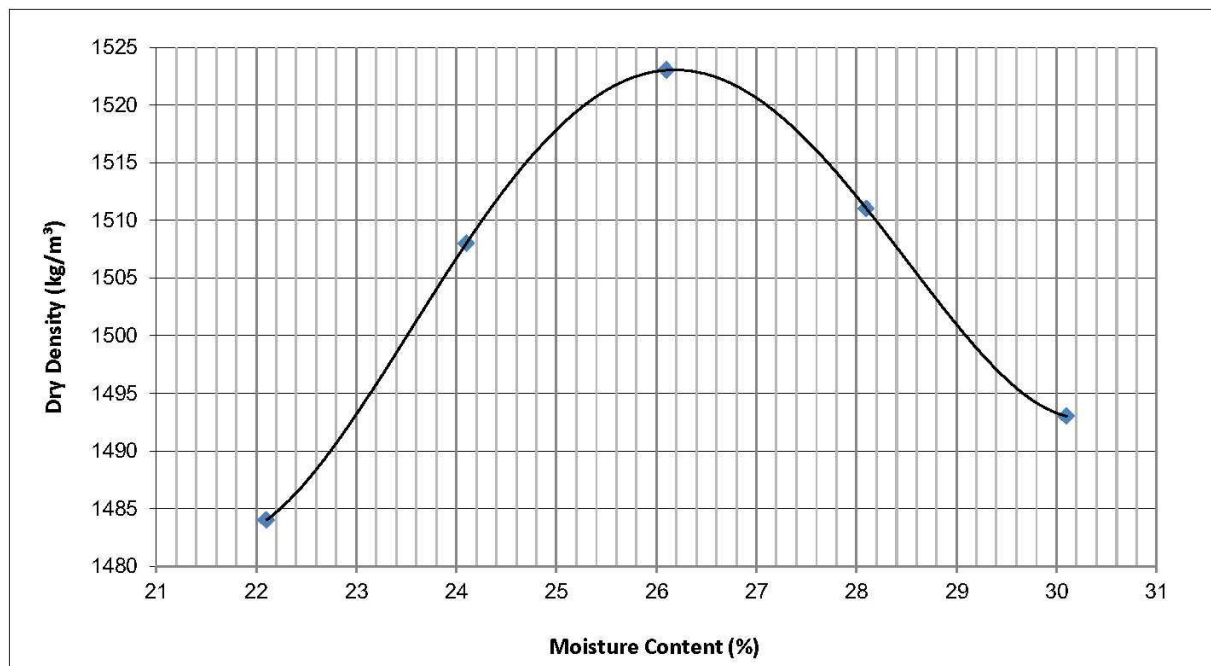
Laboratory Number	11	
Field Number	Mix C2+C4A+C7+C8+C10	
Client Reference		
Depth (m)	0.4-2.5	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - TMH1 Method A7

Compactive Effort:	Standard Proctor	
--------------------	------------------	--

Dry Density	kg/m ³	1484	1508	1523	1511	1493	
Moisture Content	%	22.1	24.1	26.1	28.1	30.1	

Max. Dry Density	kg/m ³	1523
Optimum Moisture	%	26.2



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Project : Mzinvubu Water Project

Project No: 2013-B-2004

Date Received: 23/08/2013

Date Reported: 11/11/2013

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MOISTURE DENSITY RELATIONSHIP

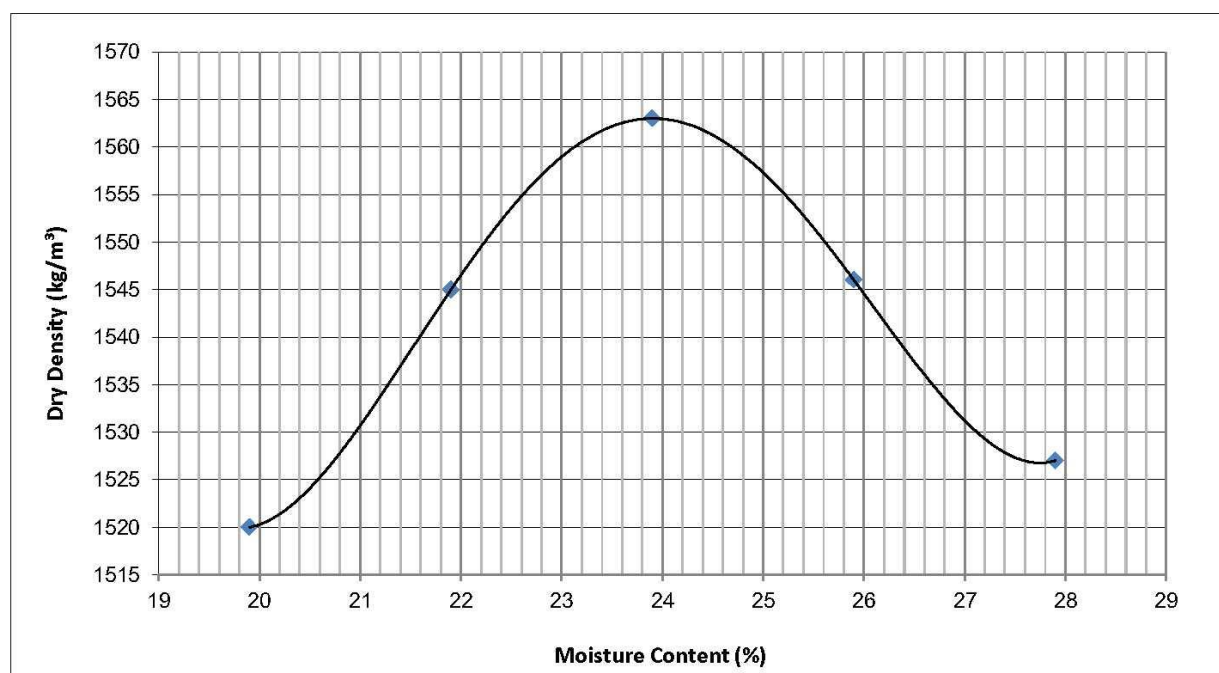
Laboratory Number	22	
Field Number	Mix Sample C12+C18+C22+C28+C30	
Client Reference		
Depth (m)	-	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - TMH1 Method A7

Compactive Effort:	Standard Proctor
--------------------	------------------

Dry Density	kg/m ³	1520	1545	1563	1546	1527	
Moisture Content	%	19.9	21.9	23.9	25.9	27.9	

Max. Dry Density	kg/m ³	1563
Optimum Moisture	%	23.9



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Project : Mzinvubu Water Project

Project No: 2013-B-2004

Date Received: 23/08/2013

Date Reported: 11/11/2013

Page No. : 24 of 44

MOISTURE DENSITY RELATIONSHIP

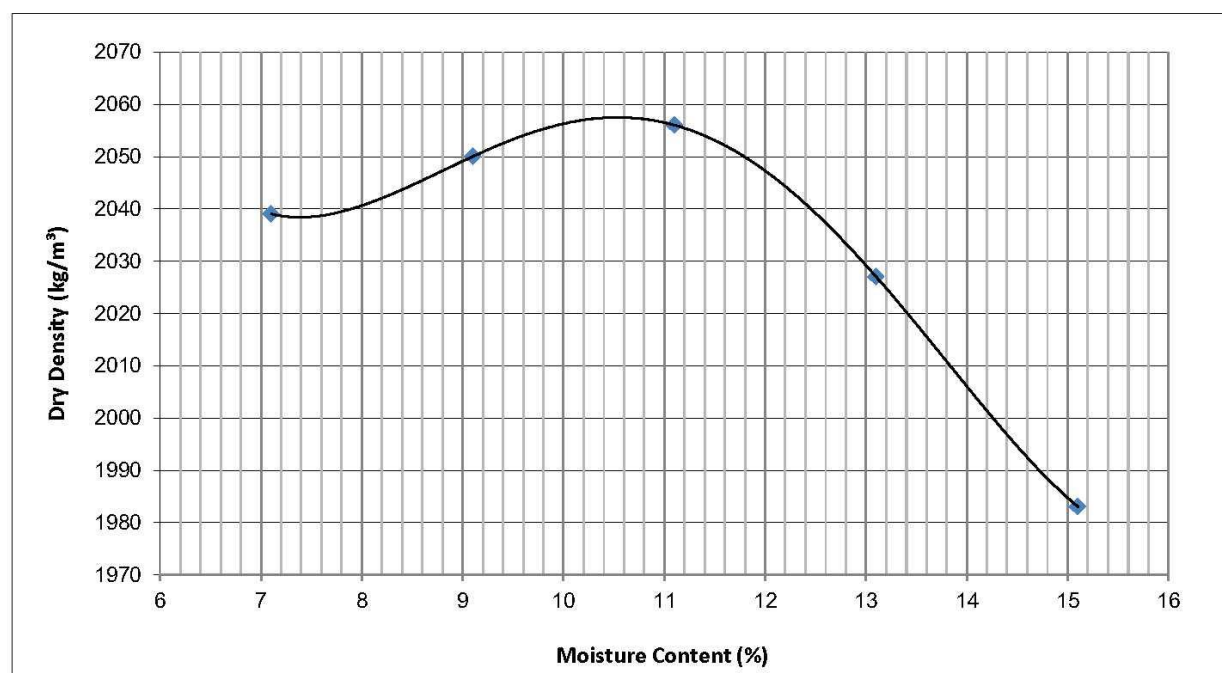
Laboratory Number	29	
Field Number	Mix Sample F5+F8+F10	
Client Reference		
Depth (m)	-	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - TMH1 Method A7

Compactive Effort:	Standard Proctor
--------------------	------------------

Dry Density	kg/m ³	2039	2050	2056	2027	1983	
Moisture Content	%	7.1	9.1	11.1	13.1	15.1	

Max. Dry Density	kg/m ³	2057
Optimum Moisture	%	10.5



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Project : Mzinubu Water Project

Project No: 2013-B-2004

Date Received: 23/08/2013

Date Reported: 11/11/2013

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MOISTURE DENSITY RELATIONSHIP

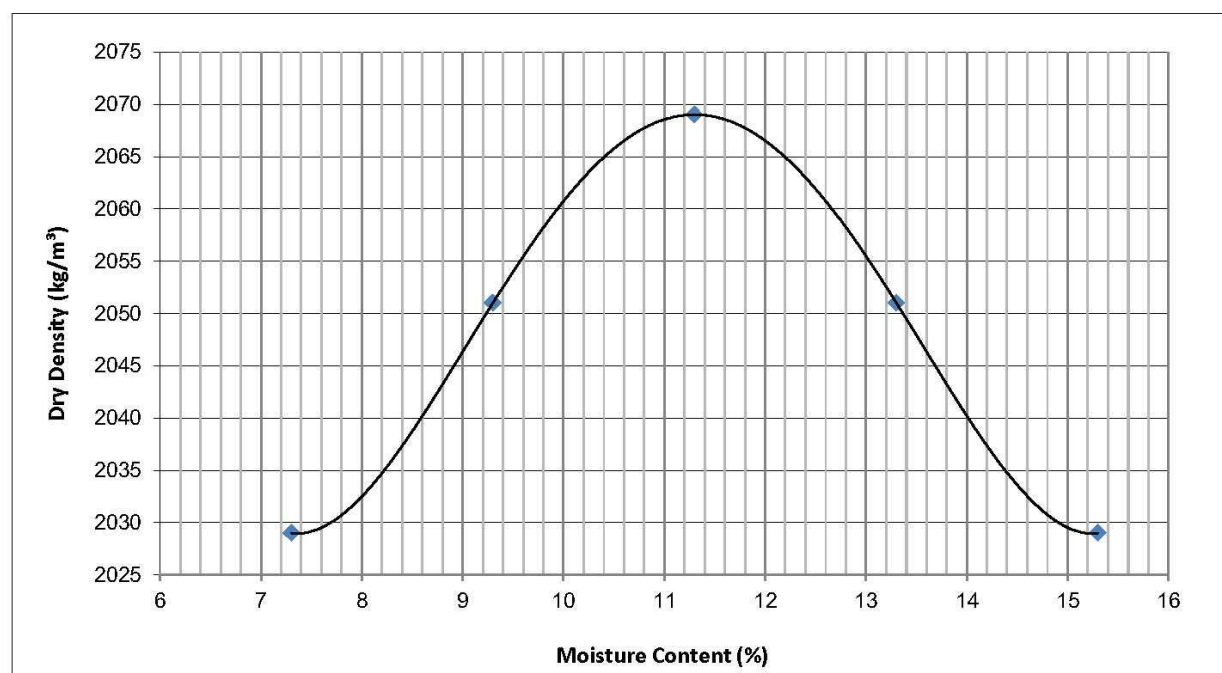
Laboratory Number		39
Field Number		Mix Sample F25+F29+F34+F37+F39
Client Reference		
Depth (m)		-
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - TMH1 Method A7

Compactive Effort:	Standard Proctor
--------------------	------------------

Dry Density	kg/m ³	2029	2051	2069	2051	2029	
Moisture Content	%	7.3	9.3	11.3	13.3	15.3	

Max. Dry Density	kg/m ³	2069
Optimum Moisture	%	11.3



FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Client : JEFFARES & GREEN CONSULTING ENGINEERS
Address : P O BOX 1109
: SUNNINGHILL
: 2157

Client Reference :
Order No. : 2819

Attention :
Facsimile : 011 807 1607
E-mail : chettyn@jgi.co.za

Date Received : 07/10/2013
Date Tested : 07/10/2013 - 29/11/2013
Date Reported : 03/12/2013

Project : Mzimvubu Water Project
Project No. : 2013-B-2246

Page : 1 of 22

Herewith please find the test report(s) pertaining to the above project. All tests were conducted in accordance with prescribed test method(s). Information herein consists of the following:

Test(s) conducted / Item(s) measured	Qty.	Test Method(s)	Authorized By	Page(s)
Atterberg Limits < 0.425mm	6.000	TMH1 A2, A3, A4	J Marques	2-4
Sieve Analysis 0.075mm (Mass Grading)	6.000	TMH1 A1	J Marques	2-4
Hydrometer Analysis	6.000	ASTM D422	J Marques	2-4
Relative Density	2.000	TMH1:A12T	J Marques	Incl. in CU
Consolidated Undrained Triaxial*	2.000	BS 1377 Part 8	J Marques	2 Files, 11 Pages
Oedometer: Standard Consolidation*	2.000	BS 1377 Part 5	J Marques	2 Files, 6 Pages
Permeability: Falling Head*	2.000	KH Head	J Marques	1 File, 1 Page

Any test results contained in this report and marked with * in the table above are "not SANAS accredited" and are not included in the schedule of accreditation for this laboratory.

Any information contained in this test report pertain only to the areas and/or samples tested. Documents may only be reproduced or published in their full context.

While every care is taken to ensure that all tests are carried out in accordance with recognised standards, neither Civilab (Proprietary) Limited nor its employees shall be liable in any way whatsoever for any error made in the execution or reporting of tests or any erroneous conclusions drawn therefrom or for any consequences thereof.

All interpretations, Interpolations, Opinions and/or Classifications contained in this report falls outside our scope of accreditation.

The following parameters, where applicable, were excluded from the classification procedure: Chemical modifications, Additional fines, Fractured Faces, Soluble Salts, pH, Conductivity, Coarse Sand Ratio, Durability (COLTO: G4-G9).

The following parameters, where applicable, were assumed: Rock types were assumed to be of an Arenaceous nature with Siliceous cementing material.

Unless otherwise requested or stated, all samples will be discarded after a period of 3 months.

Deviations in Test Methods:

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

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Client :	JEFFARES & GREEN CONSULTING ENGINEERS	Date Received:	07/10/2013
Project :	Mzimvubu Water Project	Date Reported:	03/12/2013
Project No. :	2013-B-2246	Page No. :	2 of 22

FOUNDATION INDICATOR

Laboratory Number	1	4
Field Number	RF 1	LF 01
Client Reference		
Depth (m)	1.0-1.3	1.0-1.2
Position		
Coordinates	X	
	Y	
Description	Colluvial Reddish Brown	Residual Dolerite
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

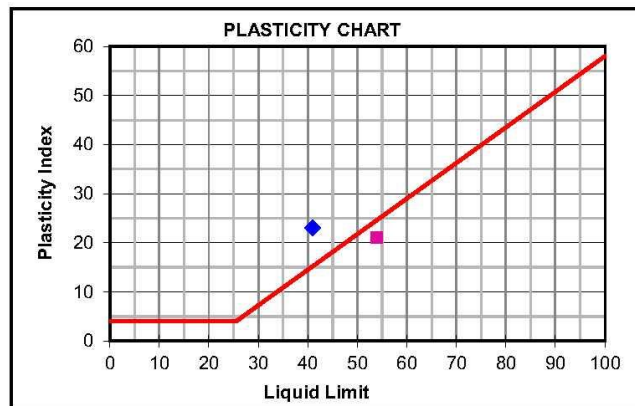
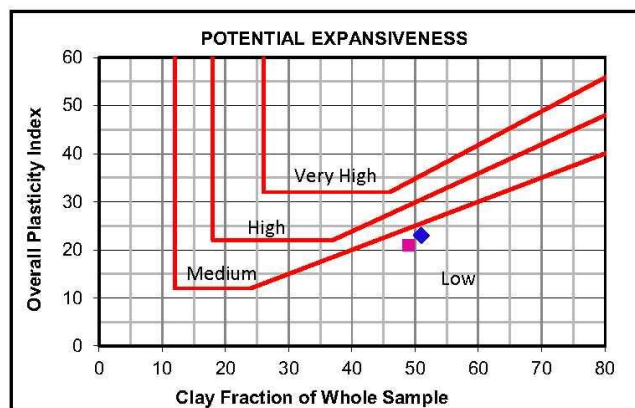
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Percentage Passing	75.0 mm	100	100
	63.0 mm	100	100
	53.0 mm	100	100
	37.5 mm	100	100
	26.5 mm	100	100
	19.0 mm	100	100
	13.2 mm	100	100
	4.75 mm	100	100
	2.00 mm	100	100
	0.425 mm	99	100
	0.075 mm	77	97
Grading Modulus		0.24	0.03

Hydrometer Analysis - ASTM Method D422

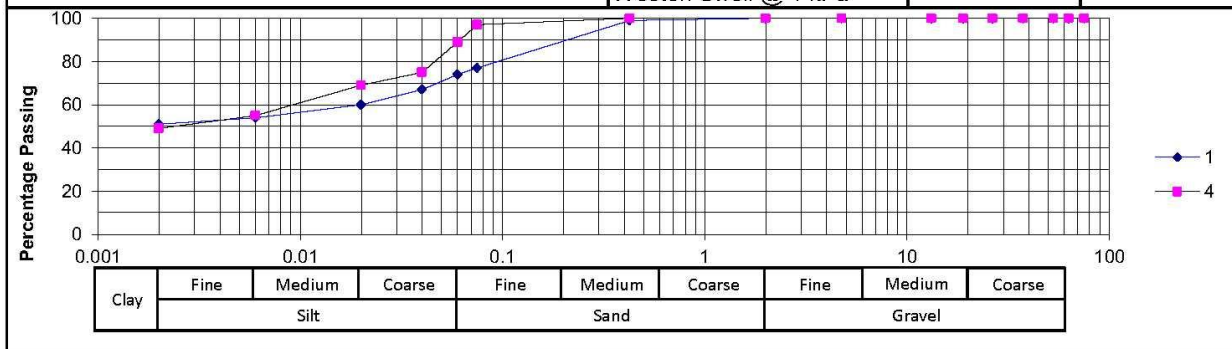
Percentage Passing	0.060 mm	74	89
	0.040 mm	67	75
	0.020 mm	60	69
	0.006 mm	54	55
	0.002 mm	51	49
Gravel	%	0	0
Sand	%	26	11
Silt	%	23	40
Clay	%	51	49



Laboratory Number		1	4
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	41	54
Plasticity Index	%	23	21
Linear Shrinkage	%	10.0	11.5
Overall P	%	23	21

Classifications

HRB	A-7-6(17)	A-7-5(20)
Unified	CL	MH
Weston Swell @ 1 kPa		



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Client :	JEFFARES & GREEN CONSULTING ENGINEERS	Date Received:	07/10/2013
Project :	Mzimvubu Water Project	Date Reported:	03/12/2013
Project No. :	2013-B-2246	Page No. :	3 of 22

FOUNDATION INDICATOR

Laboratory Number	5	6
Field Number	SSP 1	SSP 3
Client Reference		
Depth (m)	1.7-3.5	0.7-4.9
Position		
Coordinates	X	
	Y	
Description	Weathered Dolerite	
Additional Information		
Calcrete / Crushed Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

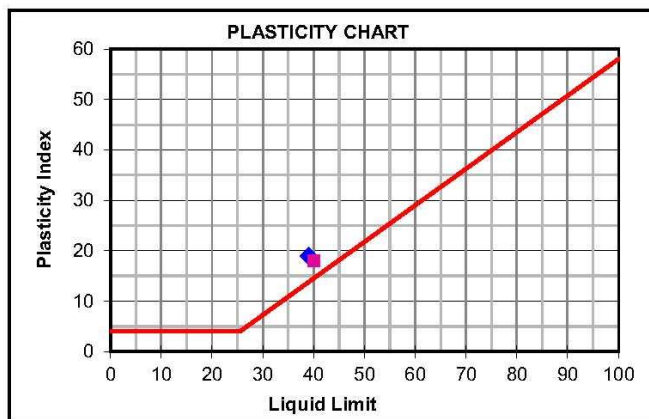
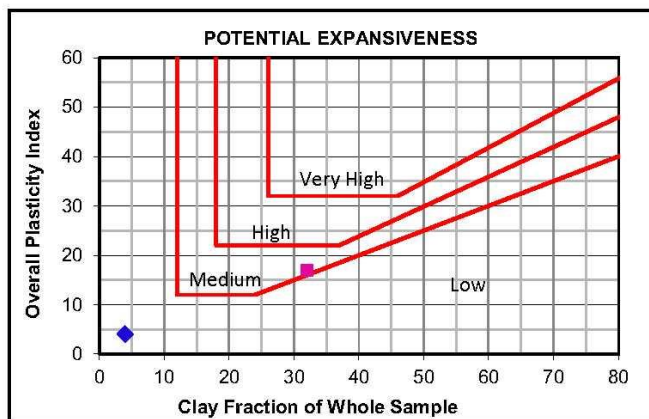
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis (Wet Preparation) - 1mm Method A1a)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	95	100
	53.0 mm	91	100
	37.5 mm	87	100
	26.5 mm	79	100
	19.0 mm	68	100
	13.2 mm	65	100
	4.75 mm	50	99
	2.00 mm	32	99
	0.425 mm	20	97
0.075 mm	13	84	
Grading Modulus		2.35	0.2

Hydrometer Analysis - ASTM Method D422

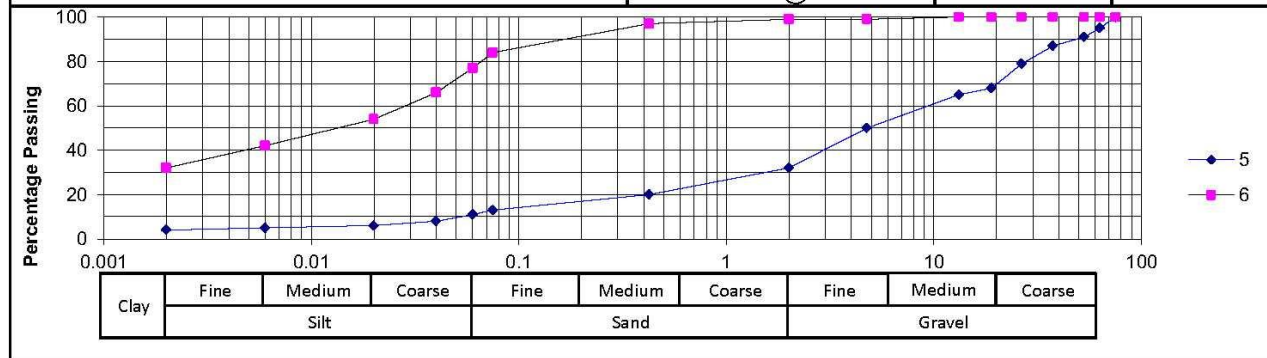
Percentage Passing	0.060 mm	11	77
	0.040 mm	8	66
	0.020 mm	6	54
	0.006 mm	5	42
	0.002 mm	4	32
Gravel	%	68	1
Sand	%	21	22
Silt	%	7	45
Clay	%	4	32



Laboratory Number		5	6
Atterberg Limits - TMH1 Method A2, A3 & A4			
Liquid Limit	%	39	40
Plasticity Index	%	19	18
Linear Shrinkage	%	9.5	10.0
Overall PI	%	4	17

Classifications

HRB	A-2-6(0)	A-6(15)
Unified	GC	CL
Weston Swell @ 1 kPa		



FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Client :	JEFFARES & GREEN CONSULTING ENGINEERS	Date Received:	07/10/2013
Project :	Mzimvubu Water Project	Date Reported:	03/12/2013
Project No :	2013-B-2246	Page No. :	4 of 22

FOUNDATION INDICATOR

Laboratory Number	7	8
Field Number	SP 5	SP 7
Client Reference		
Depth (m)	0.3-2.4	0.15-1.2
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Moisture Content & Relative Density-TMH1 Metod A12T

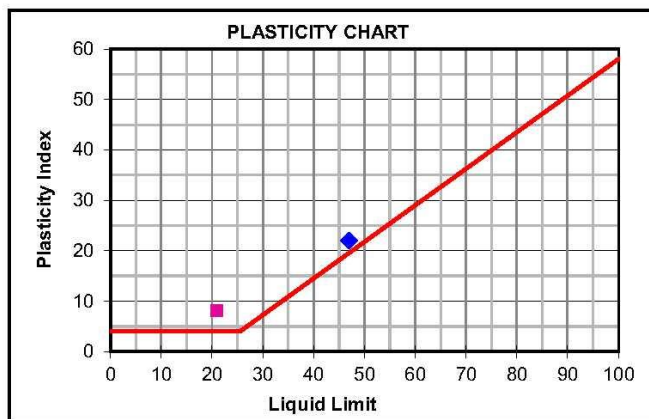
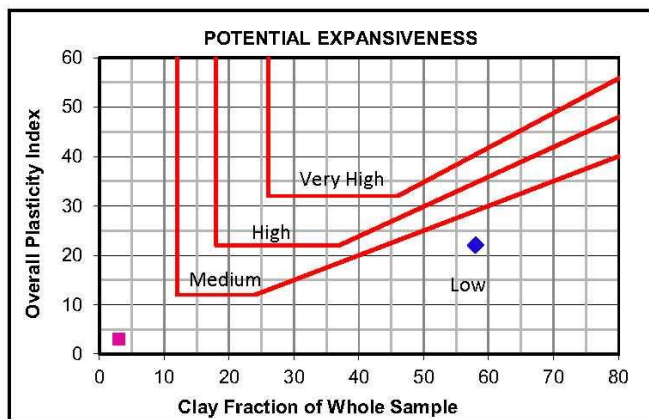
Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Preparation) - TMH1 Method A1(a)

Sieve Analysis Test: Repetition 1 (mm) (Mass %)			
Percentage Passing	75.0 mm	100	100
	63.0 mm	100	94
	53.0 mm	100	84
	37.5 mm	100	75
	26.5 mm	100	67
	19.0 mm	100	57
	13.2 mm	100	56
	4.75 mm	100	44
	2.00 mm	100	40
	0.425 mm	98	35
0.075 mm	88	11	
Grading Modulus		0.14	2.14

Hydrometer Analysis - ASTM Method D422

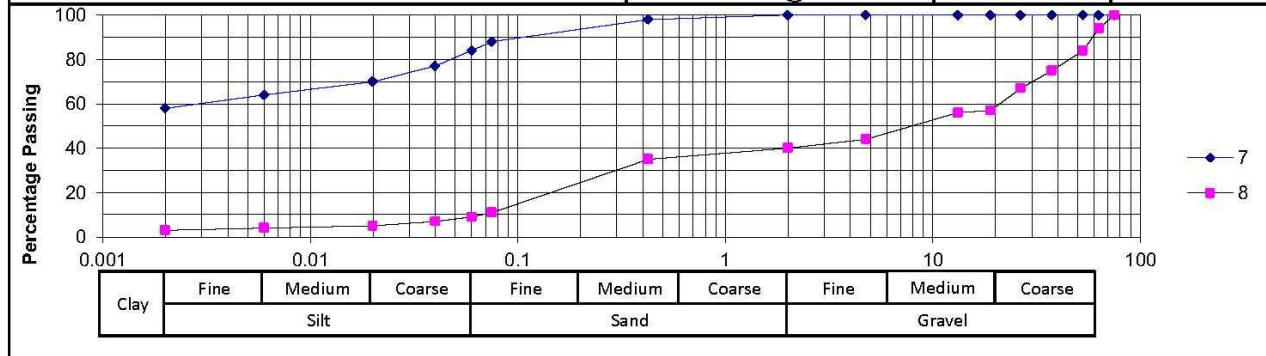
Percentage Passing	0.060 mm	84	9
	0.040 mm	77	7
	0.020 mm	70	5
	0.006 mm	64	4
	0.002 mm	58	3
Gravel	%	0	60
Sand	%	16	31
Silt	%	26	6
Clay	%	58	3



Laboratory Number		7	◆	8	■
Atterberg Limits - TMH1 Method A2, A3 & A4					
Liquid Limit	%	47		21	
Plasticity Index	%	22		8	
Linear Shrinkage	%	11.5		2.5	
Overall PI	%	22		3	

Classifications

HRB	A-7-6(20)	A-2-4(0)
Unified	CL	GP-GC
Weston Swell @ 1 kPa		



H 4:

DISPERSIVENESS

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Analyses on Potentially Dispersive Soils

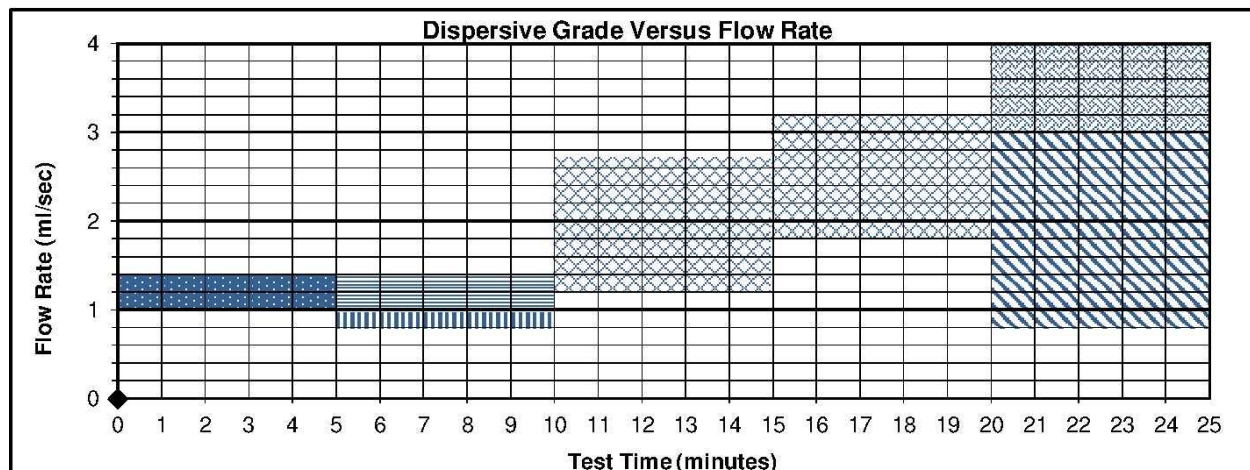
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-2
Job Number	2013-B-2004	Client/Field No.	C2
Date Received	15/10/2013	Depth (m)	0.4 - 2.6

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested		Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%				
Plastic Limit	%				
Plasticity Index	%				

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				



Dispersive Grade Index

Dispersive	Intermediate				Non-dispersive	
D1	D2	ND4	ND3	ND2	ND1	

Classification of test sample

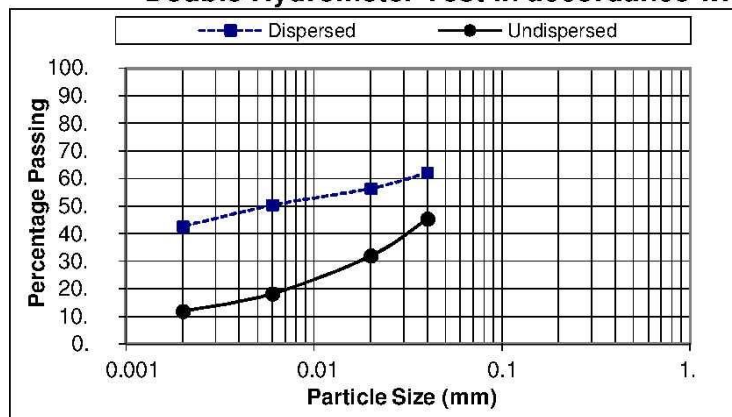
Not tested

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used		Dispersive Grade Index		Classification of test sample
		Non-dispersive	Dispersive	
		1	2	
			3	
			4	

Not tested

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

28 (Non-Dispersive)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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H - 50

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

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Analyses on Potentially Dispersive Soils

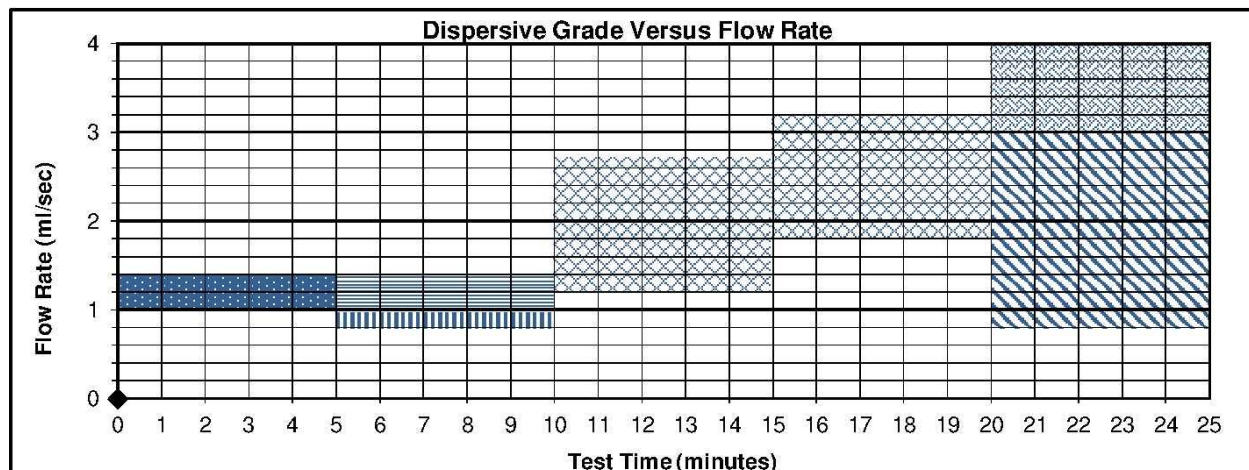
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-4
Job Number	2013-B-2004	Client/Field No.	C4A
Date Received	21/08/2013	Depth (m)	0.4 - 2.1

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested		Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%				
Plastic Limit	%			Moisture Content (%)	
Plasticity Index	%			Hole size after test (mm)	

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				



Dispersive Grade Index

Dispersive	Intermediate	Non-dispersive
D1 D2	ND4 ND3	ND2 ND1

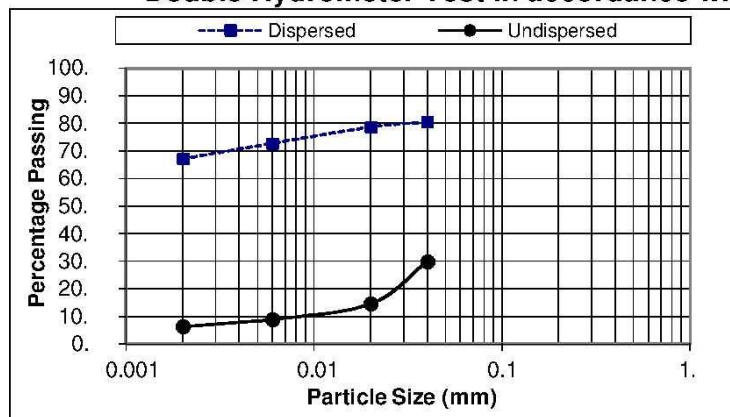
Classification of test sample

Not tested

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used		Dispersive Grade Index		Classification of test sample
		Non-dispersive	Dispersive	
		1 2	3 4	Not tested

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

9 (Non-Dispersive)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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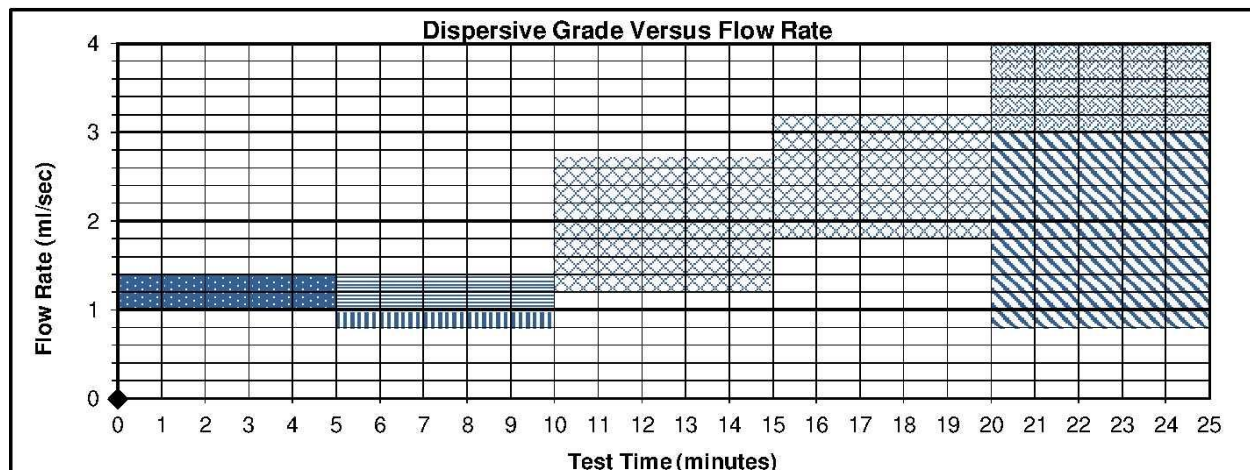
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-8
Job Number	2013-B-2004	Client/Field No.	C8
Date Received	21/08/2013	Depth (m)	0.4 - 2.5

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested	%	Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%	Moisture Content (%)			
Plastic Limit	%	Hole size after test (mm)			
Plasticity Index	%				

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				



Dispersive Grade Index

Classification of test sample

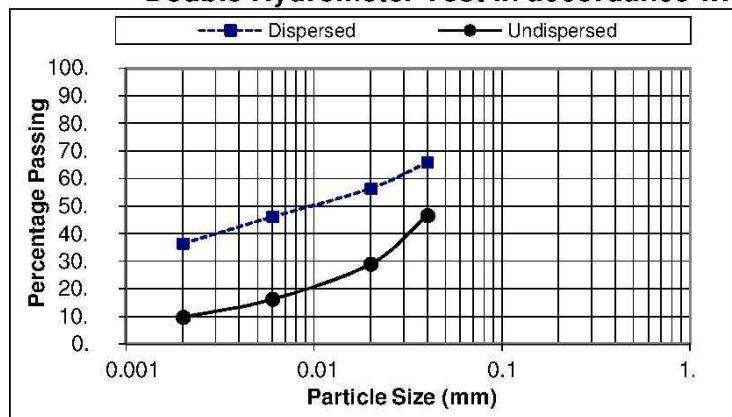
Dispersive	Intermediate	Non-dispersive
D1 D2	ND4 ND3	ND2 ND1

Not tested

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used	Dispersive Grade Index	Classification of test sample
Non-dispersive	Dispersive	Not tested
1 2	3 4	

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

27 (Non-Dispersive)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Analyses on Potentially Dispersive Soils

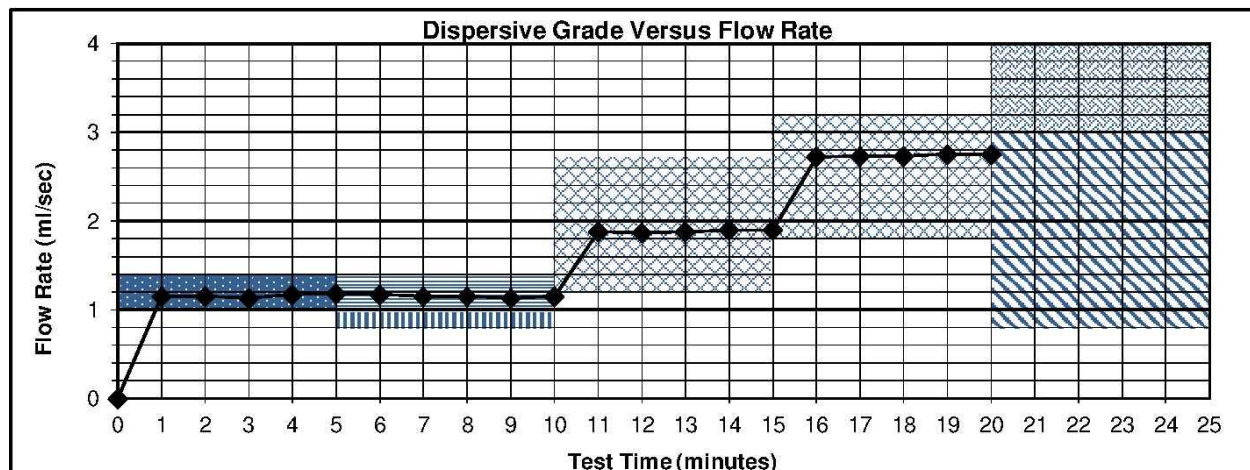
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-11
Job Number	2013-B-2004	Client/Field No.	Mix C2+C4A+C7+C8+C10
Date Received	21/08/2013	Depth (m)	0.4 - 2.5

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested	%	< 2.0 mm	Compacted Density	kg/m ³	Bulk Dry	1961
Liquid Limit	%	Not tested				1556
Plastic Limit	%		Moisture Content (%)			26
Plasticity Index	%		Hole size after test (mm)			0

Head (mm)	50										180					380					860				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20					
Flow Rate (ml/sec)	1.2	1.2	1.1	1.2	1.2	1.2	1.2	1.2	1.1	1.2	1.9	1.9	1.9	1.9	1.9	2.7	2.7	2.7	2.8	2.8					
Effluent Water	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	C	C	C	C	C					
Symbol:	PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				
																					VD-Very Dark				



Dispersive Grade Index

Dispersive	Intermediate	Non-dispersive
D1	D2	ND4
		ND3
		ND2
		ND1

Classification of test sample

ND3 (Intermediate)

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used

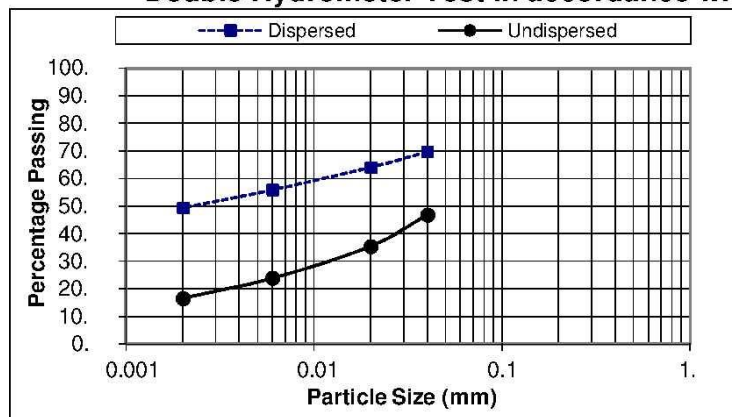
Dispersive Grade Index

Non-dispersive	Dispersive
1	2
	3
	4

Classification of test sample

Not tested

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

34 (Intermediate)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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Analyses on Potentially Dispersive Soils

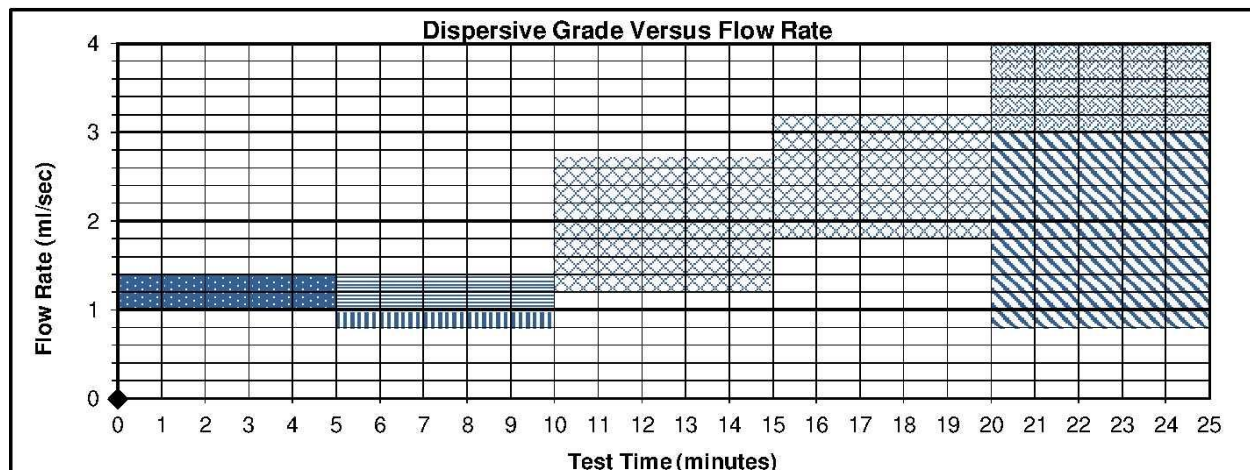
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-12
Job Number	2013-B-2004	Client/Field No.	C12
Date Received	21/08/2013	Depth (m)	0.5 - 2.6

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested		Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%				
Plastic Limit	%			Moisture Content (%)	
Plasticity Index	%			Hole size after test (mm)	

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				



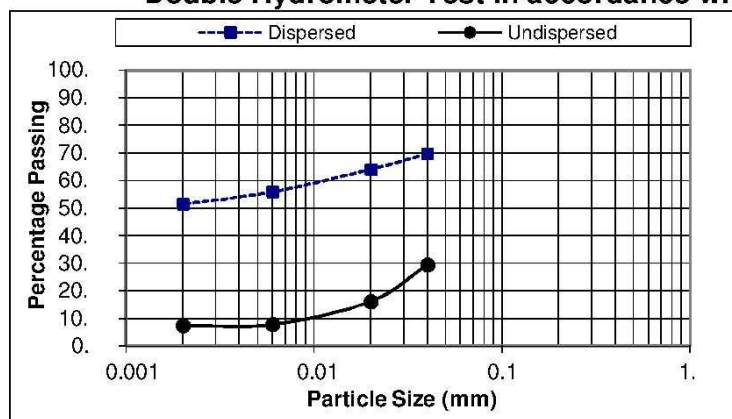
Dispersive Grade Index

Dispersive	Intermediate	Non-dispersive
D1 D2	ND4 ND3	ND2 ND1

Classification of test sample

Not tested**Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990**

Reagent used		Classification of test sample	
Dispersive Grade Index		Not tested	
Non-dispersive	Dispersive		
1 2	3 4		

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990

Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation Service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

14 (Non-Dispersive)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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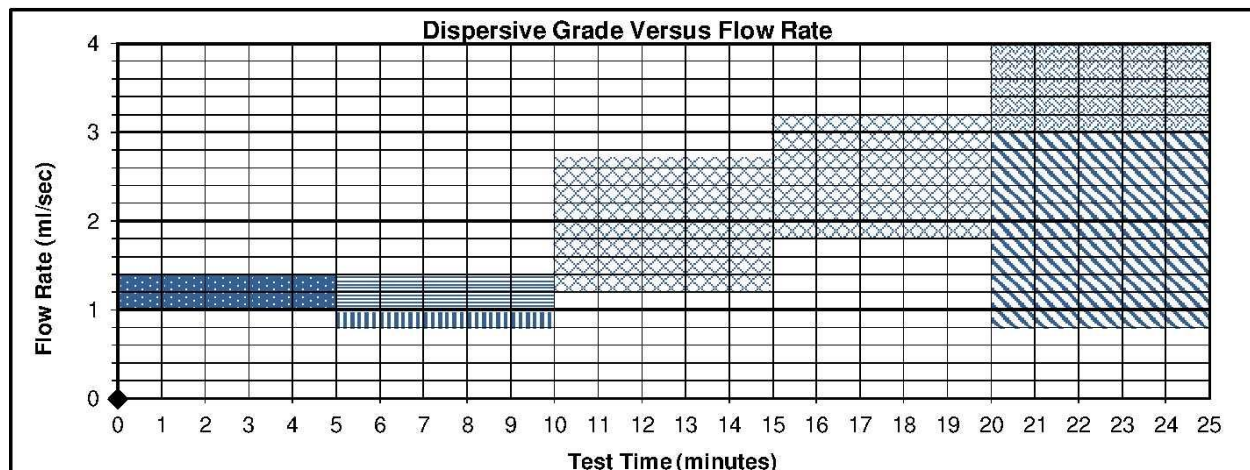
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-15
Job Number	2013-B-2004	Client/Field No.	C18
Date Received	21/08/2013	Depth (m)	0.3 - 2.9

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990







Parameters of Test Sample

Fraction tested		Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%				
Plastic Limit	%				
Plasticity Index	%				

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				



Dispersive Grade Index

Dispersive Grade Index											
Dispersive			Intermediate				Non-dispersive				
	D1		D2		ND4		ND3		ND2		ND1

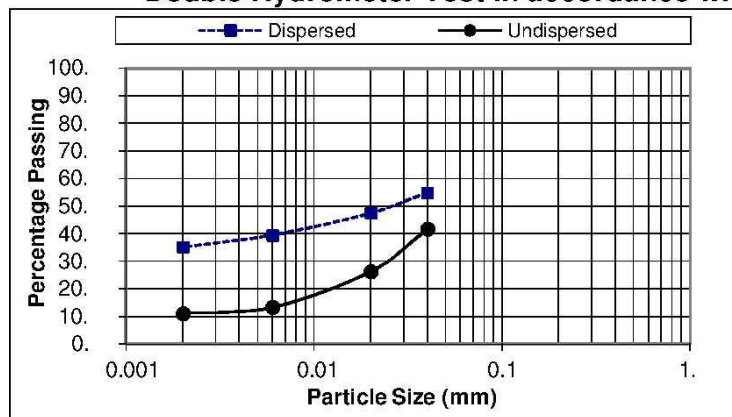
Classification of test sample

Not tested

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used		Dispersive Grade Index		Classification of test sample
		Non-dispersive	Dispersive	
		1	2	
			3	
			4	
				Not tested

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

31 (Intermediate)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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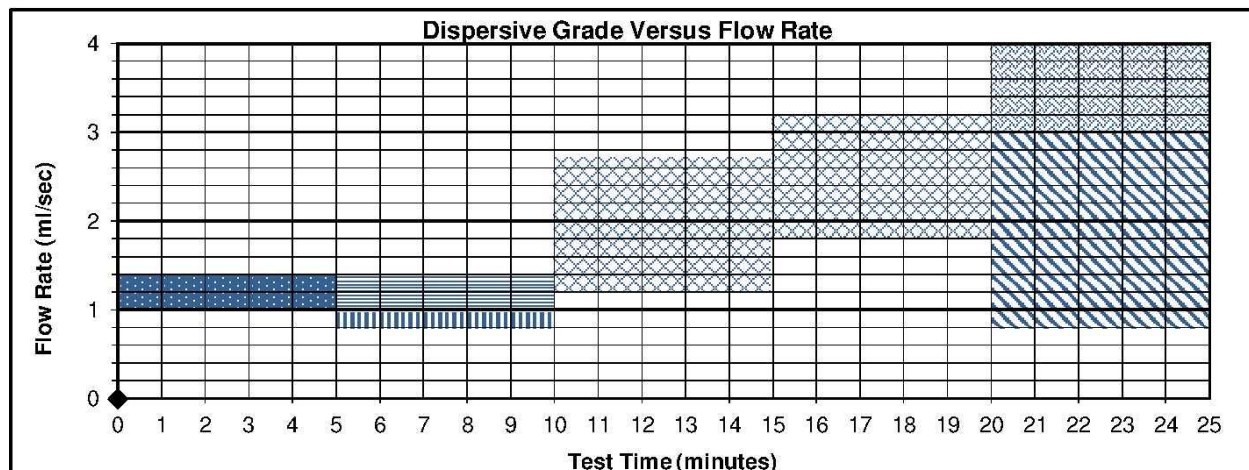
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-20
Job Number	2013-B-2004	Client/Field No.	C28
Date Received	21/08/2013	Depth (m)	0.5 - 2.6

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested	%	Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%	Moisture Content (%)			
Plastic Limit	%	Hole size after test (mm)			
Plasticity Index	%				

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				



Dispersive Grade Index

Classification of test sample

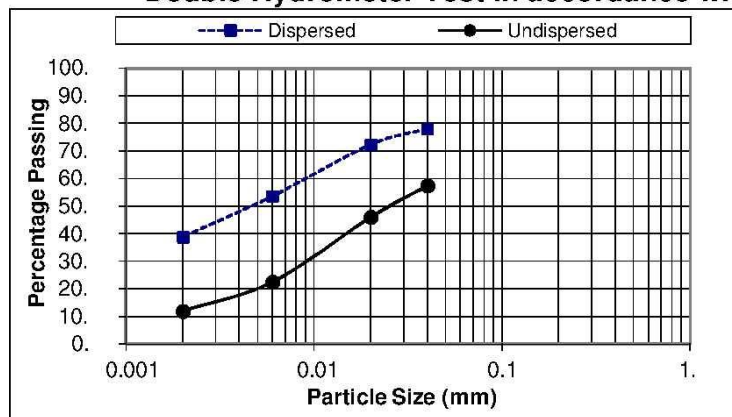
Dispersive	Intermediate	Non-dispersive
D1 D2	ND4 ND3	ND2 ND1

Not tested

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used	Dispersive Grade Index	Classification of test sample
Non-dispersive	Dispersive	Not tested
1 2	3 4	

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

31 (Intermediate)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Analyses on Potentially Dispersive Soils

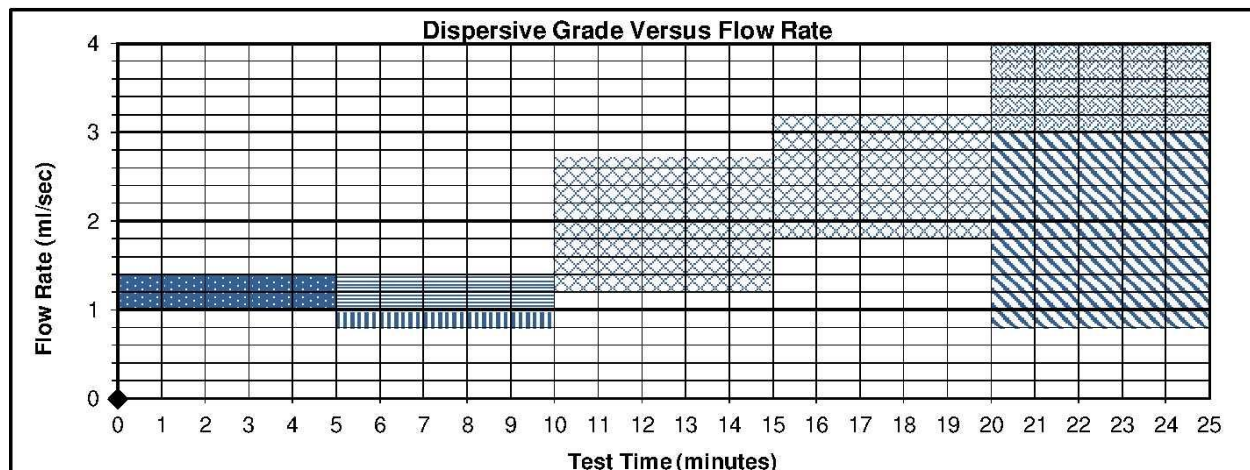
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-21
Job Number	2013-B-2004	Client/Field No.	C30
Date Received	21/08/2013	Depth (m)	0.5 - 2.1

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990







Parameters of Test Sample

Fraction tested		Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%				
Plastic Limit	%				
Plasticity Index	%				

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				



Dispersive Grade Index

Dispersive Grade Index											
Dispersive			Intermediate				Non-dispersive				
	D1		D2		ND4		ND3		ND2		ND1

Classification of test sample

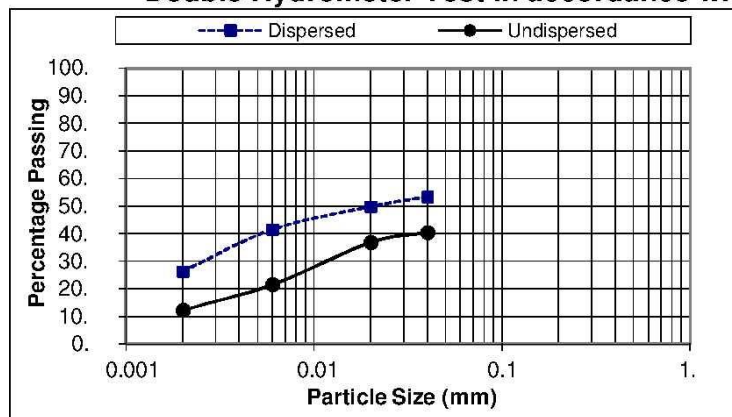
Not tested

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used		Dispersive Grade Index		Classification of test sample	
Non-dispersive					
1	2				

Not tested

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

46 (Intermediate)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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Analyses on Potentially Dispersive Soils

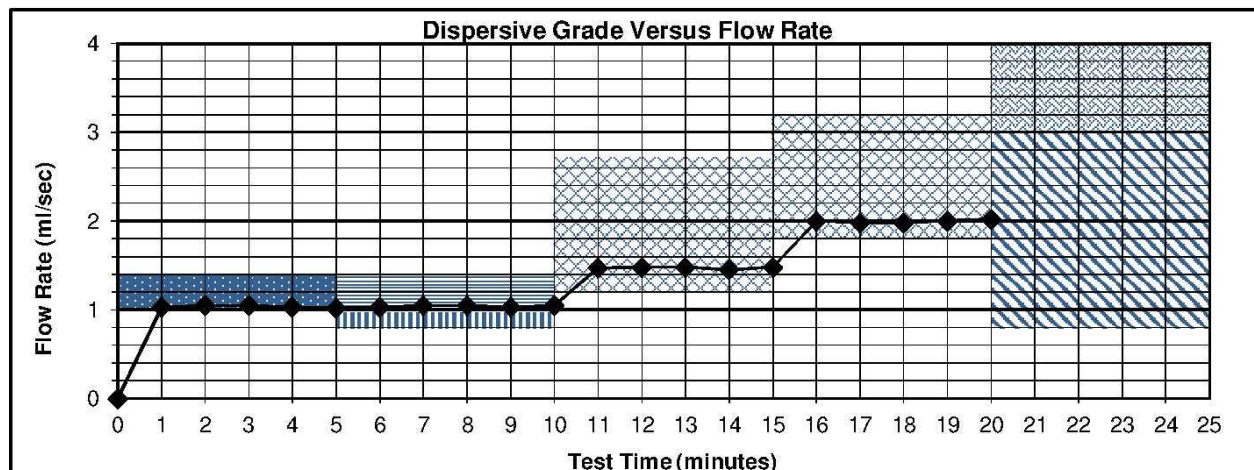
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-22
Job Number	2013-B-2004	Client/Field No.	Mix C12+C18+C22+C28+C30
Date Received	21/08/2013	Depth (m)	-

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested	%	< 2.0 mm	Compacted Density	kg/m ³	Bulk Dry	1989
Liquid Limit	%	Not tested				1608
Plastic Limit	%		Moisture Content (%)			23.7
Plasticity Index	%		Hole size after test (mm)			0

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20					
Flow Rate (ml/sec)	1.0	1.1	1.1	1.0	1.0	1.0	1.1	1.1	1.0	1.1	1.5	1.5	1.5	1.5	1.5	2.0	2.0	2.0	2.0	2.0					
Effluent Water	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	PC	C	C	C	C					
Symbol:	PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				
																					D-Dark				
																					VD-Very Dark				



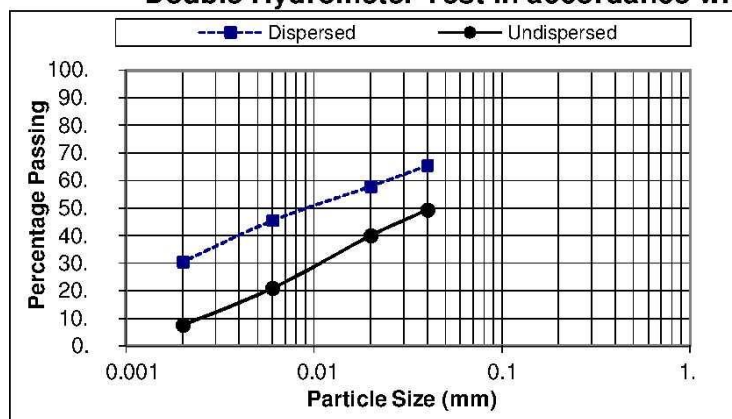
Dispersive Grade Index

Dispersive	Intermediate	Non-dispersive
D1	D2	ND4
		ND3
		ND2
		ND1

Classification of test sample

ND3 (Intermediate)**Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990**

Reagent used	Dispersive Grade Index	Classification of test sample
Non-dispersive	Dispersive	Not tested
1	2	
	3	
	4	

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990

Dispersive Grade Index

Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

25 (Non-Dispersive)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Analyses on Potentially Dispersive Soils

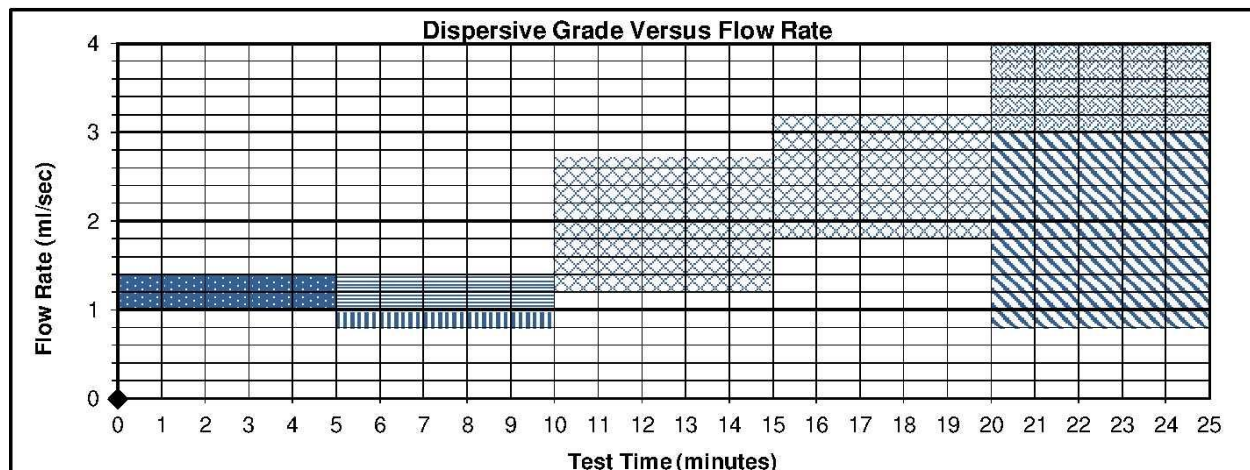
Project Name	MZIMVUBU WATER PROJECT	Lab. No.	2004-37
Job Number	2013-B-2004	Client/Field No.	F37A
Date Received	21/08/2013	Depth (m)	CHANNEL

Pinhole Test in accordance with 6.2 of BS 1377:Part 5:1990

Parameters of Test Sample

Fraction tested		Compacted Density	kg/m ³	Bulk Dry	
Liquid Limit	%				
Plastic Limit	%				
Plasticity Index	%				

Head (mm)	50										180					380					1020				
Time (min)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	20	21	22	23	24	25
Flow Rate (ml/sec)																									
Effluent Water	Symbol: PC-Perfectly Clear										C-Clear					SD-Slightly Dark					MD-Moderately Dark				

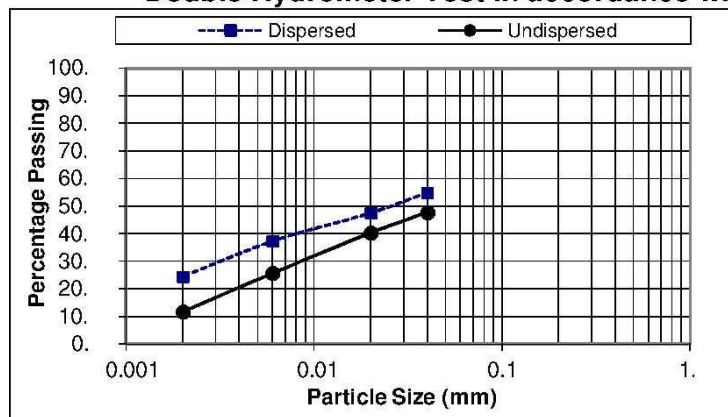


Dispersive Grade Index						Classification of test sample	
Dispersive	Intermediate	Non-dispersive				Not tested	
D1	D2	ND4	ND3	ND2	ND1		

Crumb Test in accordance with 6.3 of BS 1377:Part 5:1990

Reagent used				
Dispersive Grade Index			Classification of test sample	
Non-dispersive		Dispersive		Not tested
1	2	3	4	

Double Hydrometer Test in accordance with 6.4 of BS 1377:Part 5:1990



Dispersive Grade Index
Extract from the U.S. Department of Agriculture: Soil Conservation service: Soil Mechanics Note No. 13 (1991)

Dispersion %	Class
<30	Non-Dispersive
30-60	Intermediate (additional tests recommended)
>60	Dispersive

Classification of test sample

48 (Intermediate)

Remarks: These methods may not be suited to materials where the clay content < 10% and plasticity index ≤ 4. Hydrometer tests are done in accordance with ASTM D422 and interpreted according to BS 1377: Part 5.

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H 5

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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Civil Engineering Testing Laboratory

Triaxial Compression Test Results

Project:	Mzinvu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-11
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed C2, C4A, C7, C8, C10 in equal fractions.
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Test No. 1

SATURATION DATA

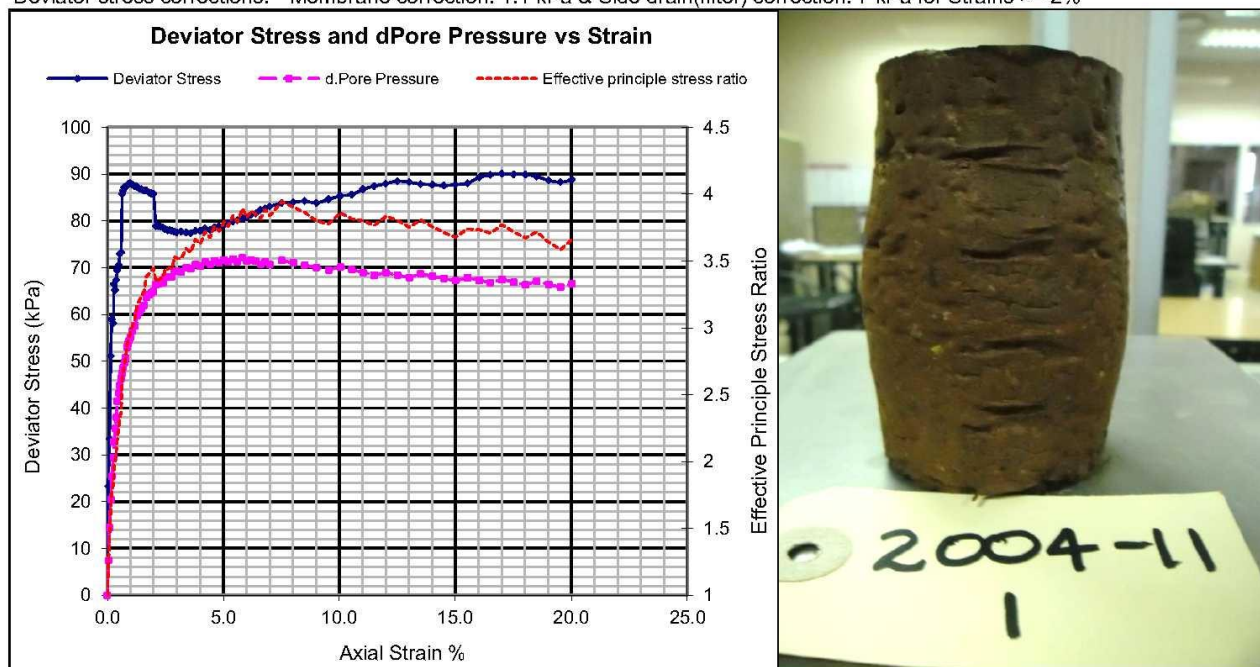
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	343.0	Final back pressure (kPa):	333.0
		Final B parameter:	0.96

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		100.0		t100 (minutes): 9		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.87	*50.1	1971.36	27.1	1457	0.8183	88	2.65 Assumed
CONSOLIDATED	100.06	49.70	1939.68	30.4	1493	0.7745	104	
FINAL (After shear)	80.01	55.57	2425.65	30.4	1493	0.7747	104	
Initial pore pressure (kPa): 442.7		Final pore pressure (kPa): 336.7			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	1.00				
Initial pore pressure (kPa):	336.0	Initial effective stress (kPa): 100.0			
Parameters at failure:					
Failure Criterion:	Max. Effective Principle Stress Ratio				
Axial strain (%):	7.52				
Deviator stress (kPa):	83.8	Principle Stresses (kPa)			
Excess pore pressure (kPa):	71.5	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	3.946	183.8	112.3	100.0	28.5
Deviator stress corrections: Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

36 Fourth Str.,Booyens Reserve,Johannesburg 2091

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Civil Engineering Testing Laboratory

Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-11
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed C2, C4A, C7, C8, C10 in equal fractions.
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SATURATION DATA

Test No. 2

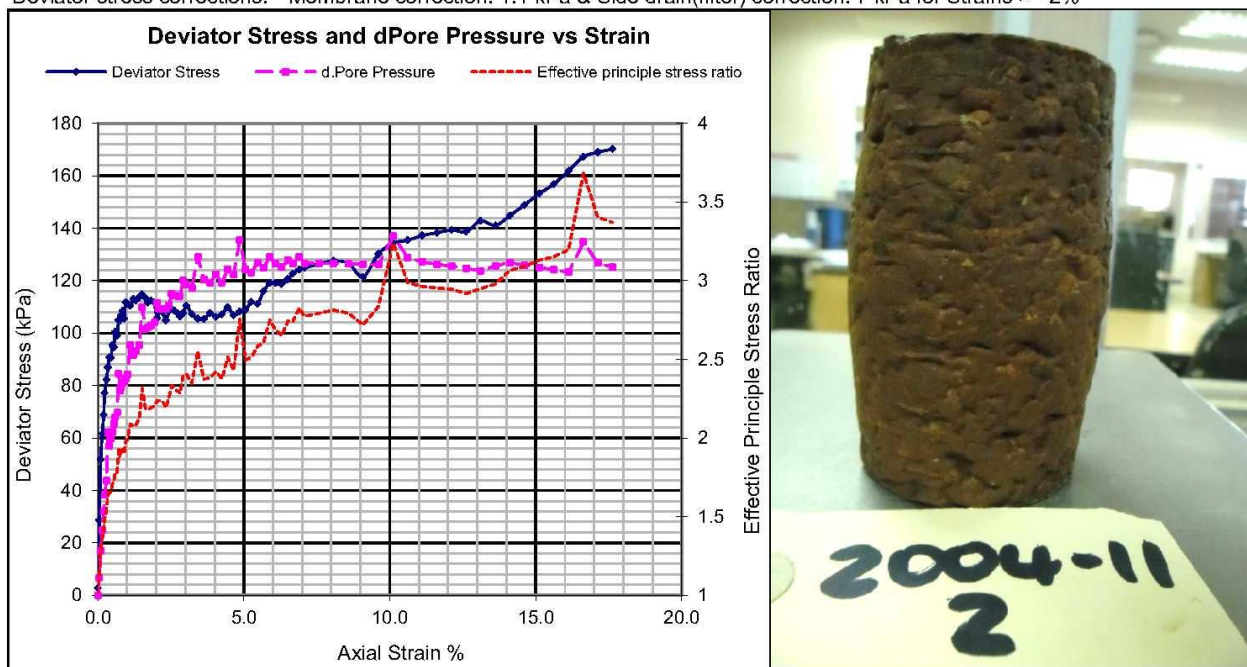
Saturation method: Alternating increments of cell- & back pressure			
Pressure increments applied (kPa): 50,70,100,100,100...		Differential pressure (kPa): 10.0	
Final cell pressure (kPa): 423.0		Final back pressure (kPa): 413.0	Final B parameter: 0.98

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		197.0		t100 (minutes): 4		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*101.09	*50.13	1973.72	25.3	1474	0.7978	84	2.65 Assumed
CONSOLIDATED	99.24	49.21	1901.61	21.9	1559	0.6993	83	
FINAL (After shear)	81.75	54.22	2308.65	21.9	1558	0.7005	83	
Initial pore pressure (kPa): 605.4		Final pore pressure (kPa): 415.5			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	1.25				
Initial pore pressure (kPa):	420.0	Initial effective stress (kPa): 197.0			
Parameters at failure:					
Failure Criterion:	Max. Effective Principle Stress Ratio				
Axial strain (%):	16.63				
Deviator stress (kPa):	167.1	Principle Stresses (kPa)			
Excess pore pressure (kPa):	134.7	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	3.684	364.1	229.4	197.0	62.3
Deviator stress corrections: Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



Civilab (Proprietary) Limited. Registration No.: 1998/019071/07

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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

36 Fourth Str.,Booyens Reserve,Johannesburg 2091

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Civil Engineering Testing Laboratory

Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-11
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed C2, C4A, C7, C8, C10 in equal fractions.
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Test No. 3

SATURATION DATA

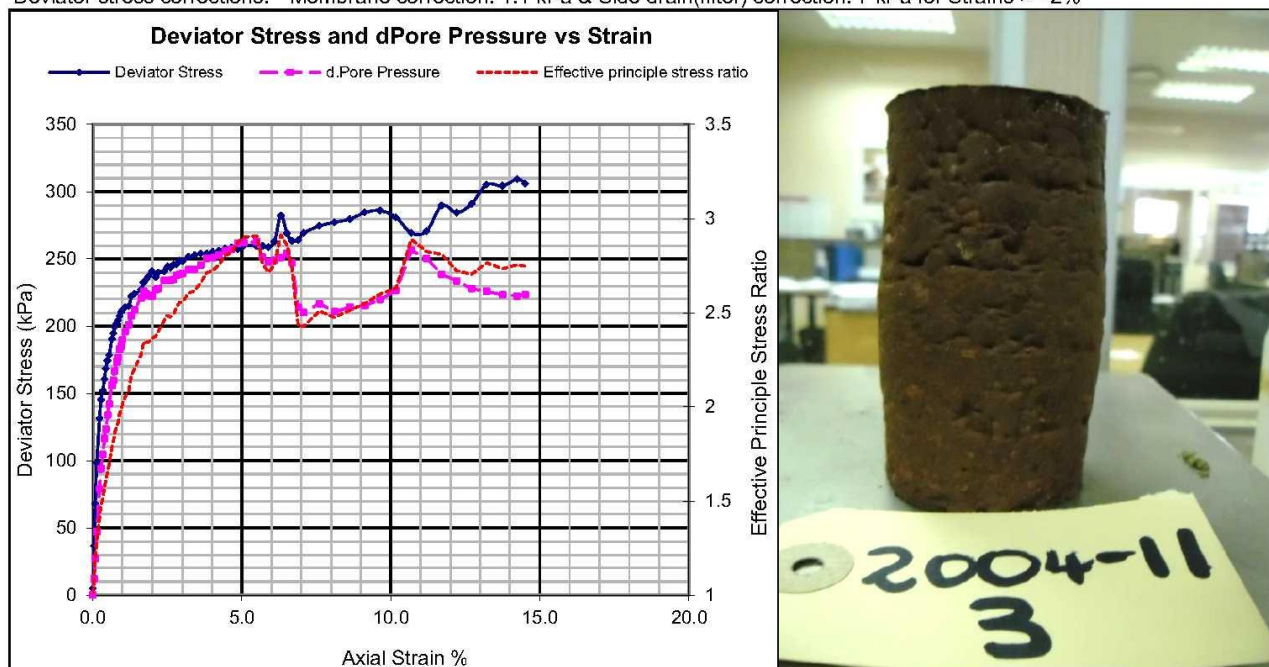
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	323.0	Final back pressure (kPa):	313.0
		Final B parameter:	1.00

CONSOLIDATION DATA

Effective cons. Stress (kPa):		398.7		t100 (minutes): 100		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.97	*50.14	1974.51	25.4	1472	0.8001	84	2.65 Assumed
CONSOLIDATED	97.93	48.60	1855.43	26.3	1619	0.6372	110	
FINAL (After shear)	83.72	52.57	2170.27	26.3	1615	0.6405	109	
Initial pore pressure (kPa): 704.3		Final pore pressure (kPa): 312.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.20			
Initial pore pressure (kPa):	313.3	Initial effective stress (kPa): 398.7		
Parameters at failure:				
Failure Criterion:	Max. Effective Principle Stress Ratio			
Axial strain (%):	6.31			
Deviator stress (kPa):	282.1	Principle Stresses (kPa)		
Excess pore pressure (kPa):	251.1	σ_1	σ_1'	σ_3
Effective principle stress ratio:	2.912	680.7	429.6	σ_3'
Deviator stress corrections:		Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%		



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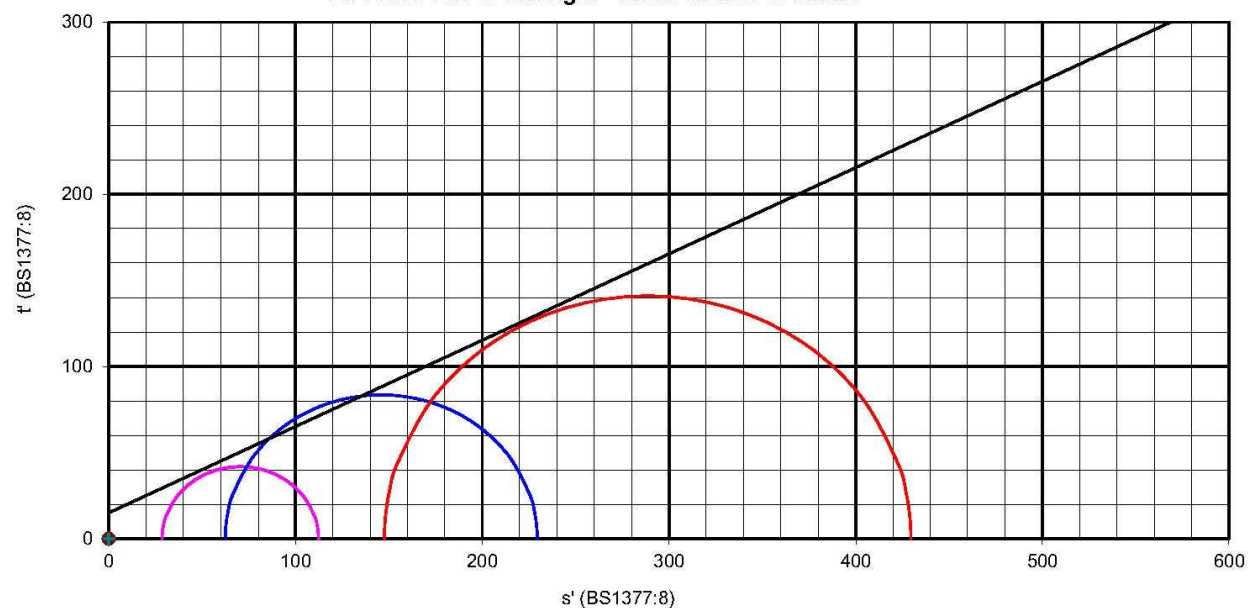
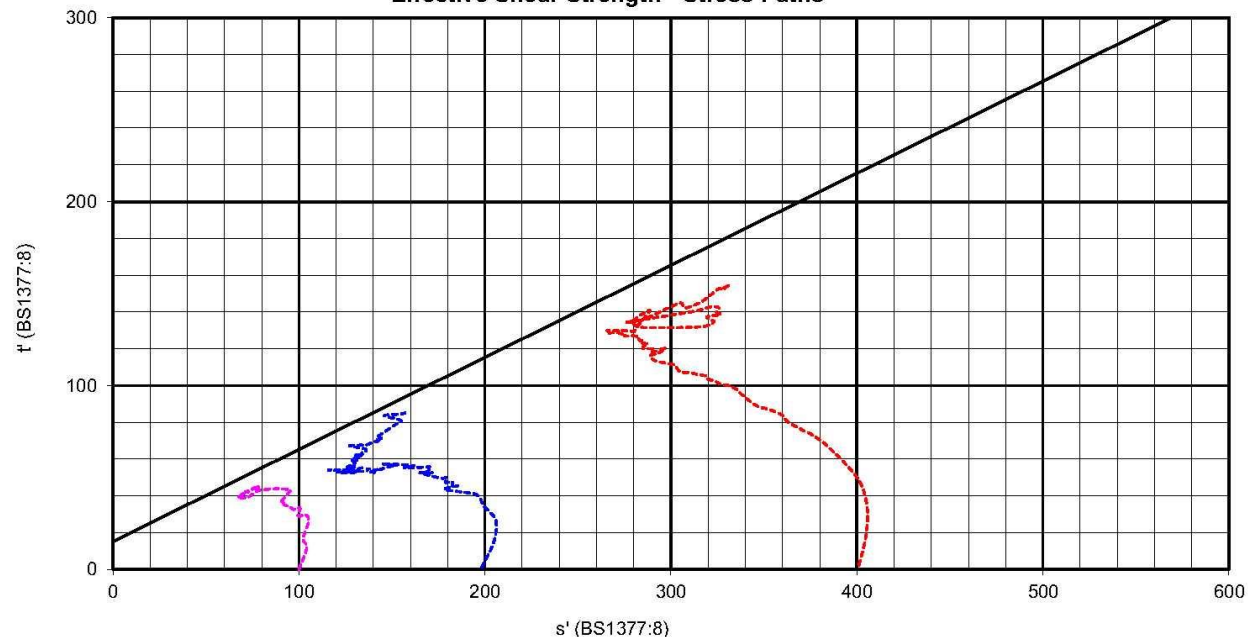
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Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-11
Field Sample Reference:	Refer to Remarks	Depth (m):	-

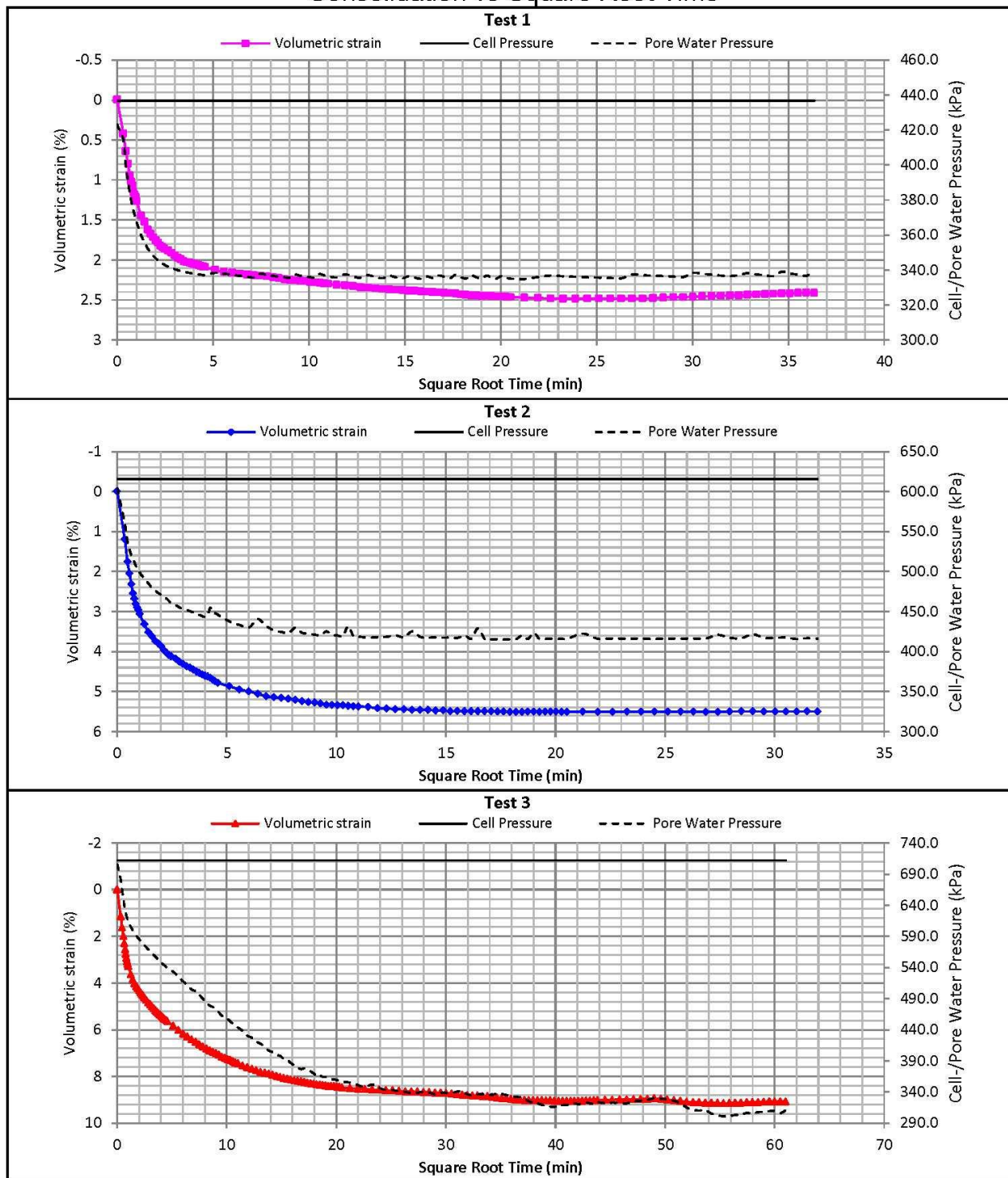
Effective Shear Strength Parameters

Stresses	Cohesion (kPa)	Internal friction (Degrees)
Total	10.4	14.2
Effective	15.1	26.6

Effective Shear Strength - Mohr circles at failure**Effective Shear Strength - Stress Paths**

Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-11
Field Sample Reference:	Refer to Remarks	Depth (m):	-

Consolidation vs Square Root Time

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Civil Engineering Testing Laboratory

Triaxial Compression Test Results

Project:	Mzinvu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	2004-22
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed C12, C18, C22, C28, C30 in equal fractions.
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Test No. 1

SATURATION DATA

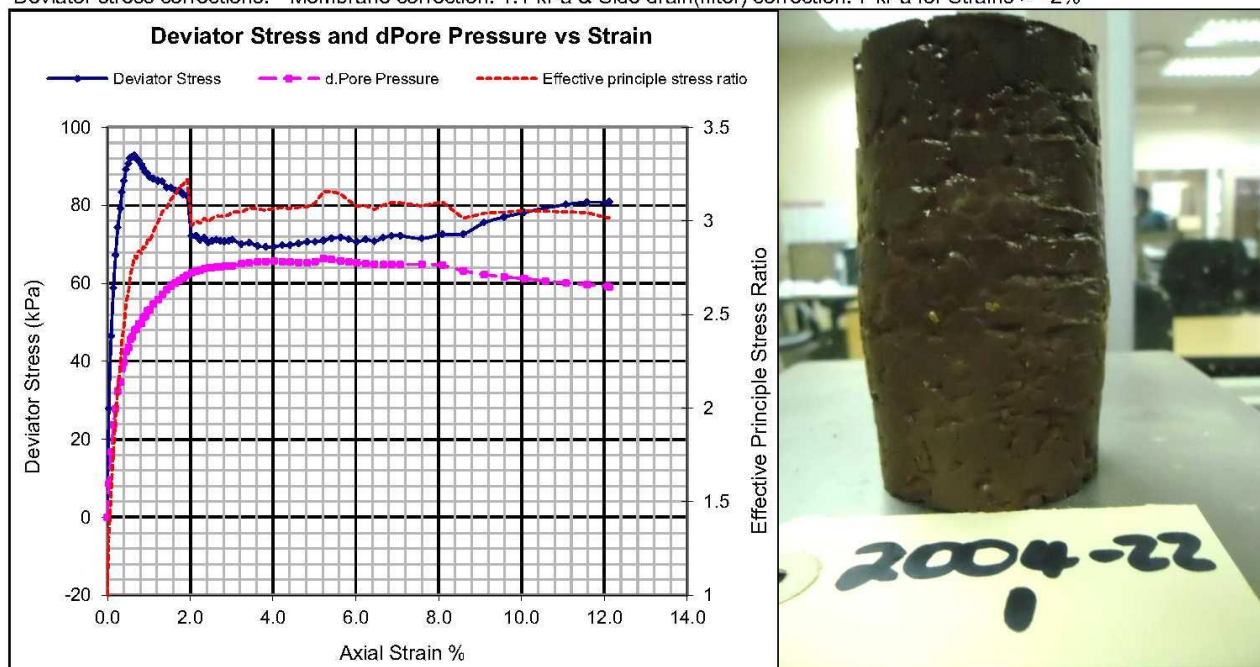
Saturation method:			Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):			50,70,100,100,100...		Differential pressure (kPa): 10.0
Final cell pressure (kPa): 323.0		Final back pressure (kPa): 313.0		Final B parameter: 0.99	

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		99.2		t100 (minutes): 16		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.07	*49.96	1960.36	27.6	1470	0.8079	91	2.657 Determined
CONSOLIDATED	99.33	49.59	1931.46	31.0	1503	0.7680	107	
FINAL (After shear)	87.30	52.90	2197.68	31.0	1503	0.7682	107	
Initial pore pressure (kPa): 406.8		Final pore pressure (kPa): 317.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.25				
Initial pore pressure (kPa):	322.8	Initial effective stress (kPa): 99.2			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	0.65				
Deviator stress (kPa):	92.8	Principle Stresses (kPa)			
Excess pore pressure (kPa):	48.0	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	2.811	192.0	144.0	99.2	51.2
Deviator stress corrections: Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



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Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	2004-22
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed C12, C18, C22, C28, C30 in equal fractions.
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SATURATION DATA**Test No. 2**

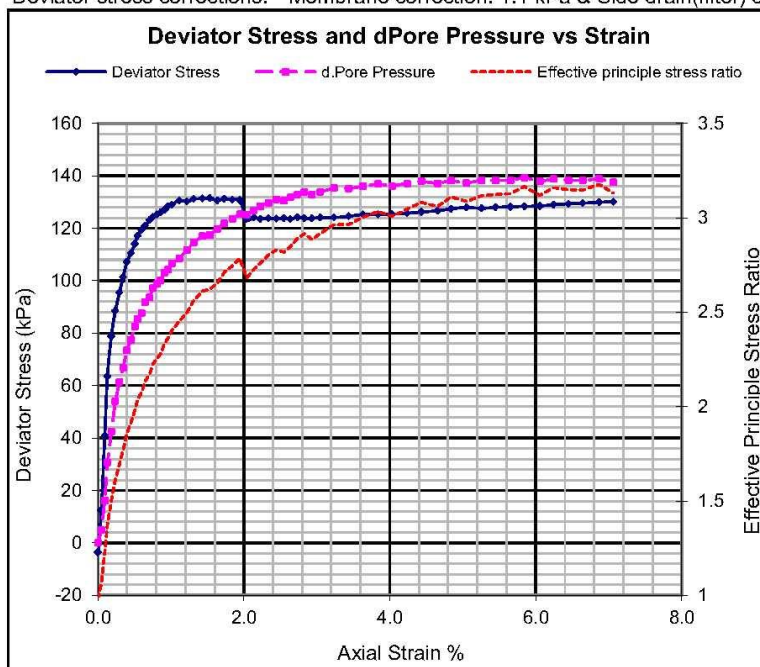
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	353.0	Final back pressure (kPa):	343.0
		Final B parameter:	0.97

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		198.5		t100 (minutes): 100		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.52	*50.01	1964.28	27.5	1464	0.8147	90	2.657 Determined
CONSOLIDATED	99.05	49.27	1906.68	29.7	1532	0.7349	107	
FINAL (After shear)	92.05	51.11	2051.57	29.7	1531	0.7356	107	
Initial pore pressure (kPa): 535.5		Final pore pressure (kPa): 346.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.33				
Initial pore pressure (kPa):	348.5	Initial effective stress (kPa): 198.5			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	1.53				
Deviator stress (kPa):	131.4	Principle Stresses (kPa)			
Excess pore pressure (kPa):	117.4	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	2.620	330.0	212.5	198.5	81.1
Deviator stress corrections: Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

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Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	2004-22
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed C12, C18, C22, C28, C30 in equal fractions.
----------	---

Test No. 3

SATURATION DATA

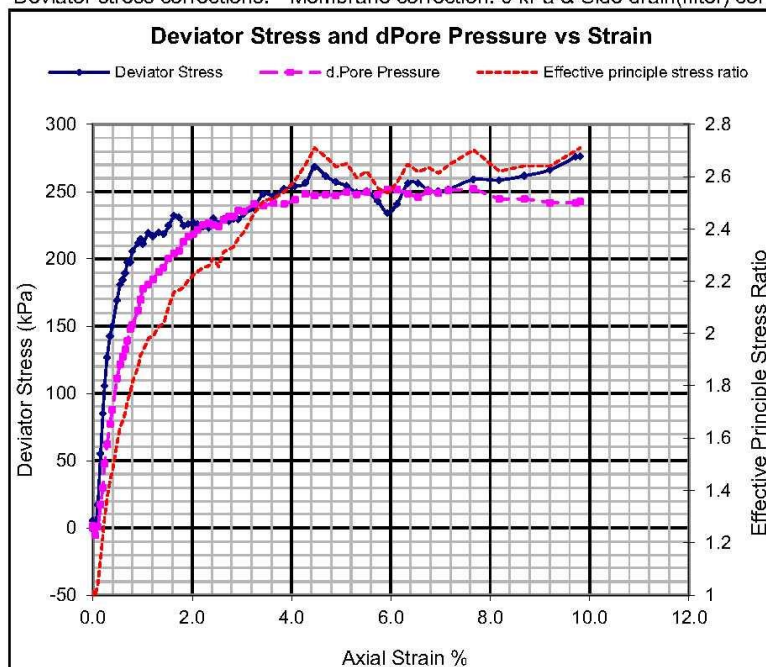
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	333.0	Final back pressure (kPa):	323.0
		Final B parameter:	1.00

CONSOLIDATION DATA

Effective cons. Stress (kPa):		404.0		t100 (minutes): 100		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.08	*50.03	1965.85	27.3	1483	0.7921	92	2.657 Determined
CONSOLIDATED	97.77	48.86	1875.11	27.8	1593	0.6680	110	
FINAL (After shear)	88.18	51.45	2079.16	27.8	1591	0.6699	110	
Initial pore pressure (kPa): 710.4		Final pore pressure (kPa): 313.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.20				
Initial pore pressure (kPa):	322.0	Initial effective stress (kPa): 404.0			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	9.81				
Deviator stress (kPa):	276.0	Principle Stresses (kPa)			
Excess pore pressure (kPa):	242.6	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	2.710	679.9	437.4	404.0	161.4
Deviator stress corrections: Membrane correction: 0 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



Civilab (Proprietary) Limited. Registration No.: 1998/019071/07

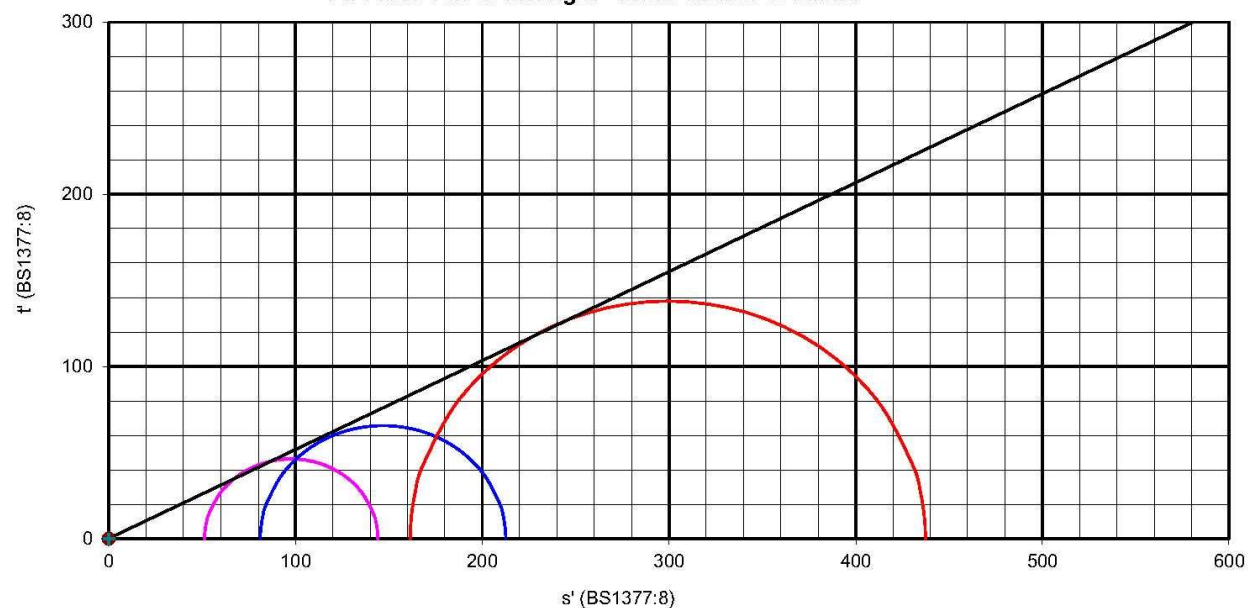
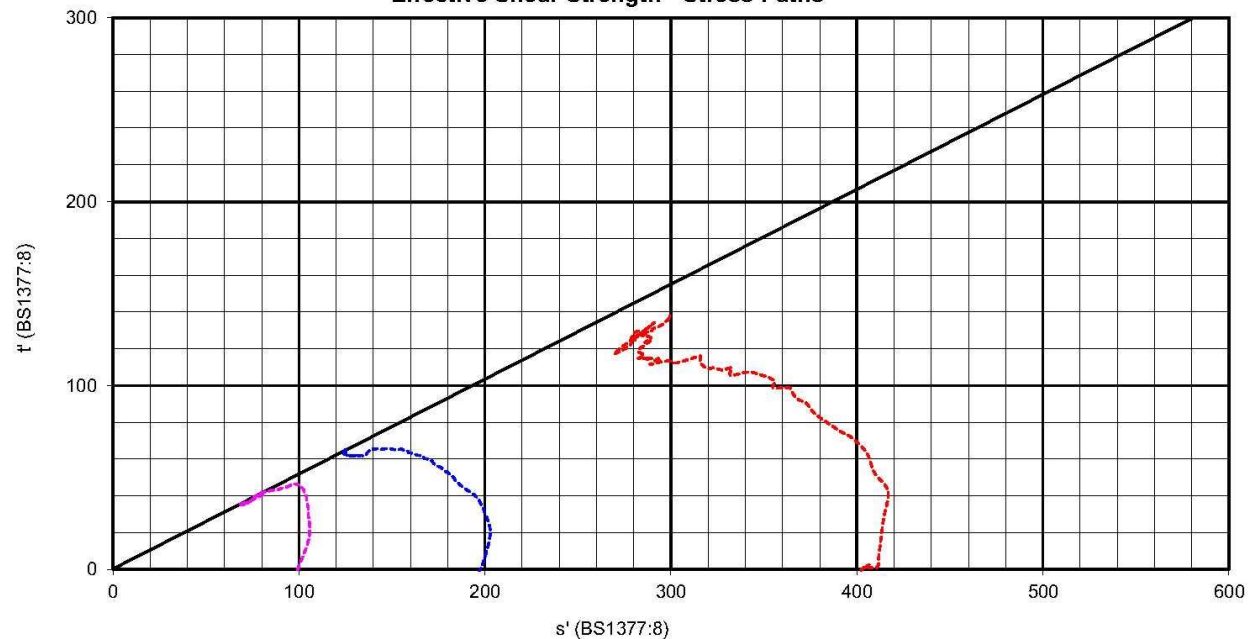
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Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	2004-22
Field Sample Reference:	Refer to Remarks	Depth (m):	-

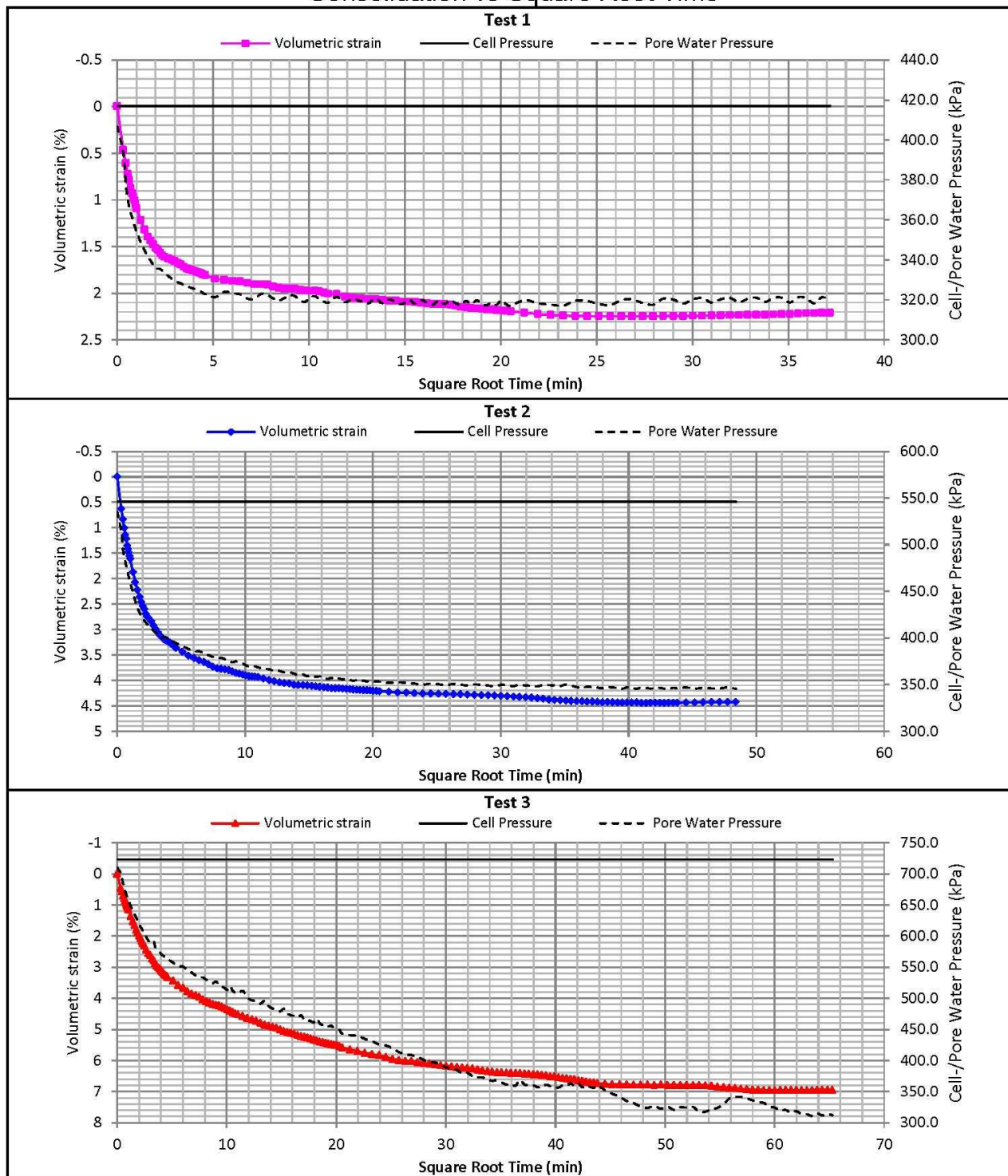
Effective Shear Strength Parameters

Stresses	Cohesion (kPa)	Internal friction (Degrees)
Total	8.6	13.7
Effective	0.2	27.3

Effective Shear Strength - Mohr circles at failure**Effective Shear Strength - Stress Paths**

Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	2004-22
Field Sample Reference:	Refer to Remarks	Depth (m):	-

Consolidation vs Square Root Time

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-29
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed F5, F8, F10 in equal fractions.
----------	---

Test No. 1

SATURATION DATA

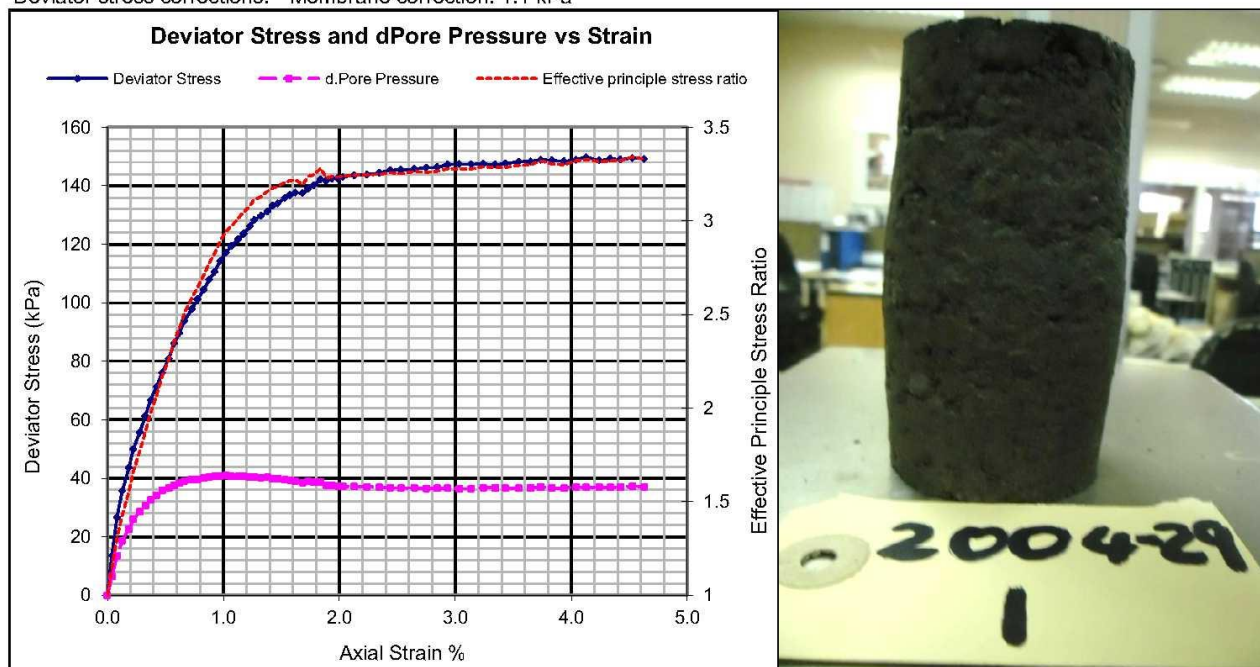
Saturation method: Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa): 10.0
Final cell pressure (kPa):	353.0	Final back pressure (kPa): 343.0
		Final B parameter: 0.96

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		101.1		t100 (minutes): 60		Side drains fitted: No		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.29	*50.18	1977.66	10.3	1932	0.3281	80	2.566 Determined
CONSOLIDATED	99.36	49.71	1940.91	15.4	1987	0.2911	136	
FINAL (After shear)	94.76	50.90	2035.13	15.4	1987	0.2913	136	
Initial pore pressure (kPa): 339.1		Final pore pressure (kPa): 339.6			PWP dissipation (%): No build-up			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.30				
Initial pore pressure (kPa):	336.9	Initial effective stress (kPa): 101.1			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	4.13				
Deviator stress (kPa):	149.7	Principle Stresses (kPa)			
Excess pore pressure (kPa):	36.8	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	3.328	250.8	214.0	101.1	64.3
Deviator stress corrections: Membrane correction: 1.1 kPa					



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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

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Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-29
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed F5, F8, F10 in equal fractions.
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Test No. 3

SATURATION DATA

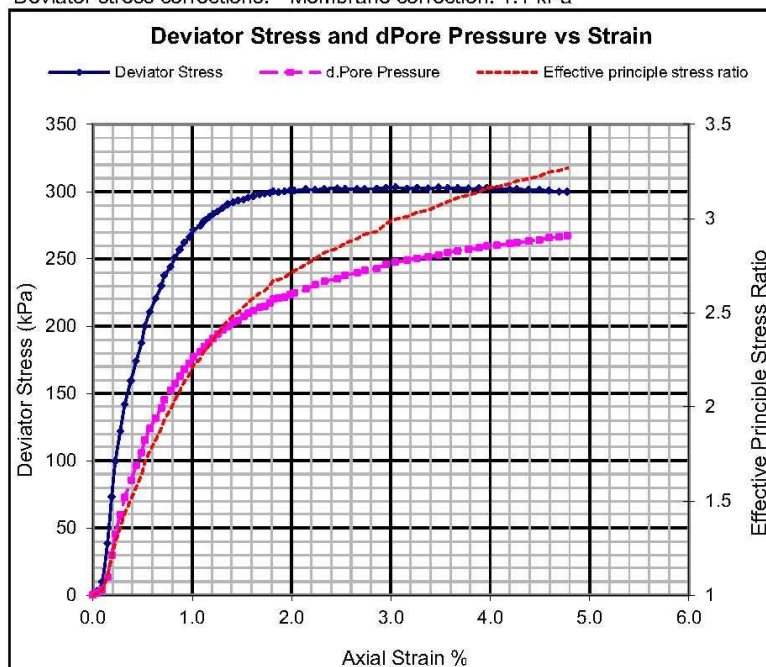
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	353.0	Final back pressure (kPa):	343.0
		Final B parameter:	0.97

CONSOLIDATION DATA

Effective cons. Stress (kPa):		399.4		t100 (minutes): 120		Side drains fitted: No		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.35	*50.17	1976.87	10.3	1931	0.3287	80	2.566 Determined
CONSOLIDATED	98.59	49.28	1907.50	14.0	2038	0.2588	139	
FINAL (After shear)	93.88	50.50	2003.17	14.0	2037	0.2596	139	
Initial pore pressure (kPa): 339.1		Final pore pressure (kPa): 339.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.30				
Initial pore pressure (kPa):	338.6	Initial effective stress (kPa): 399.4			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	3.05				
Deviator stress (kPa):	303.0	Principle Stresses (kPa)			
Excess pore pressure (kPa):	247.5	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	2.996	702.4	454.9	399.4	151.8
Deviator stress corrections: Membrane correction: 1.1 kPa					



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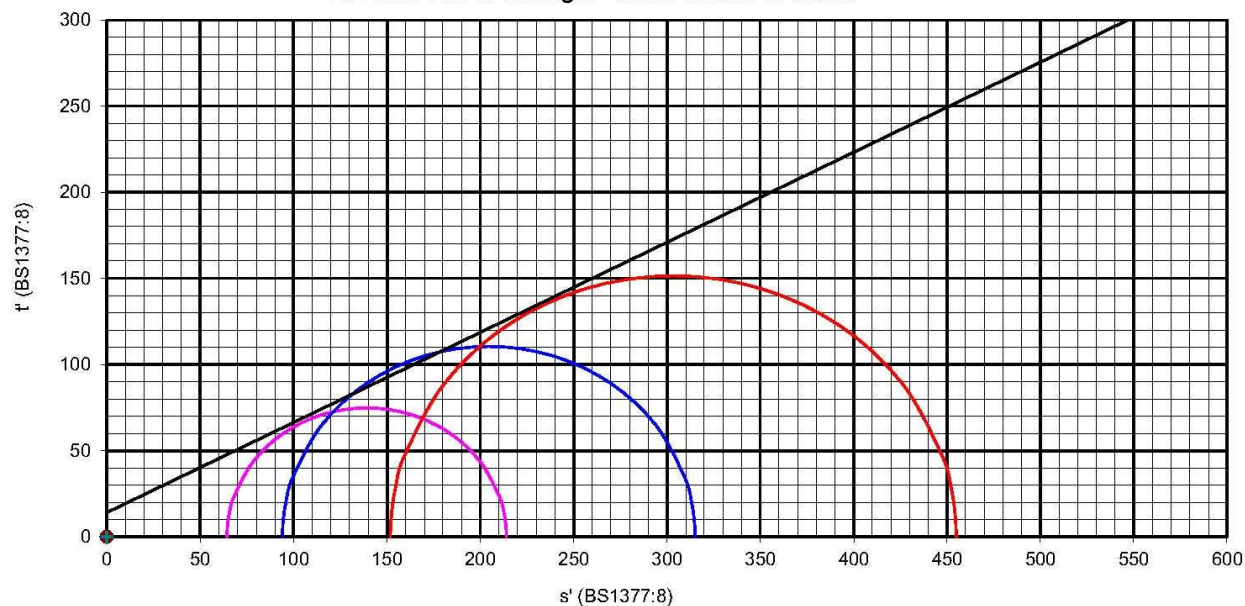
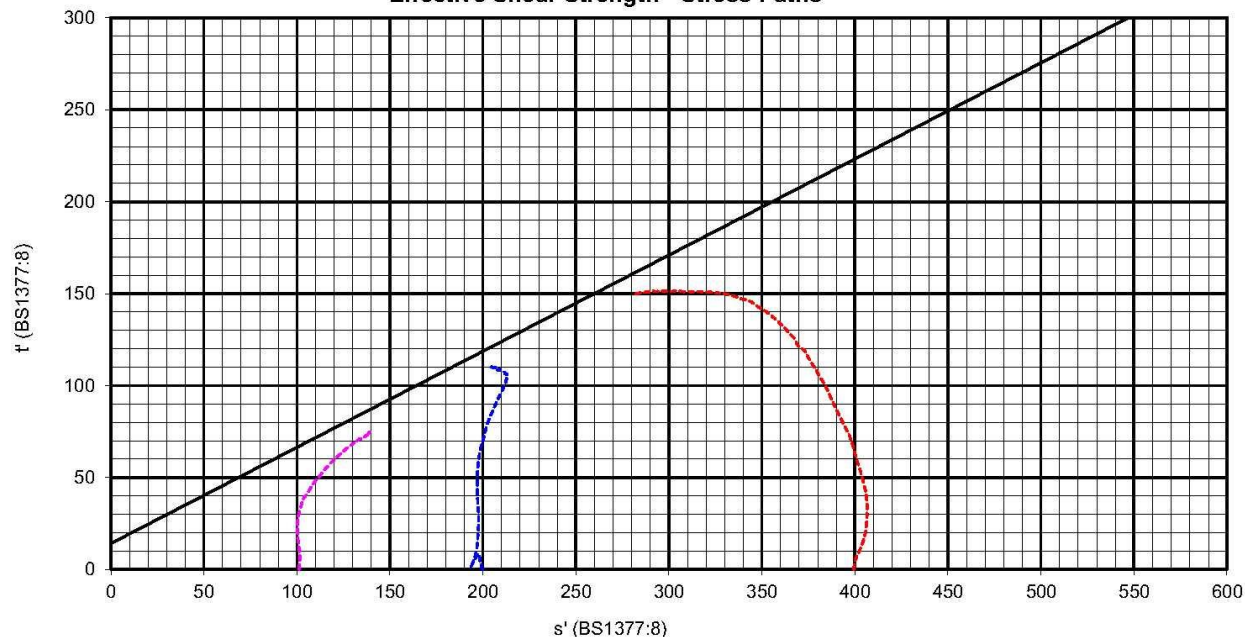
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Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-29
Field Sample Reference:	Refer to Remarks	Depth (m):	-

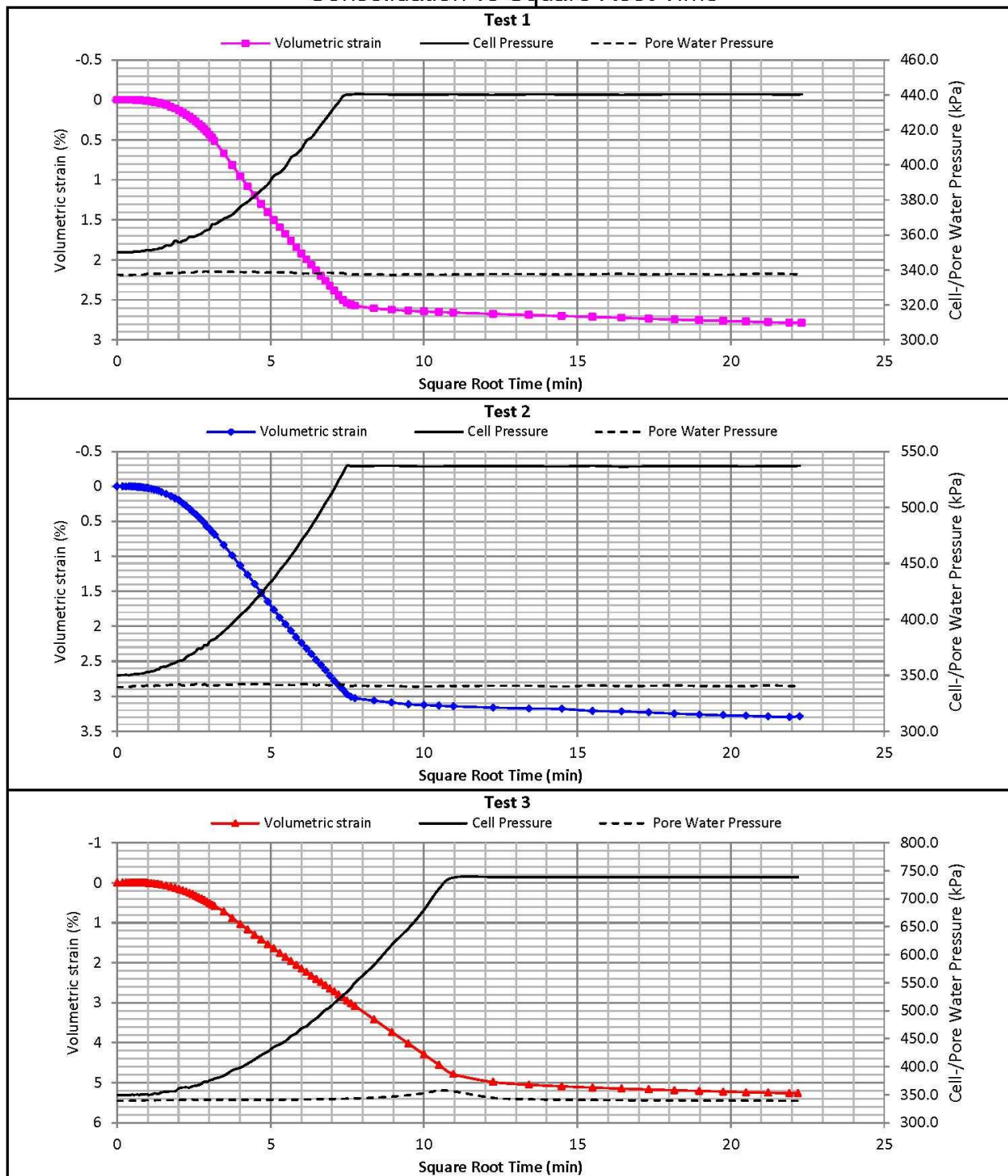
Effective Shear Strength Parameters

Stresses	Cohesion (kPa)	Internal friction (Degrees)
Total	43.9	11.6
Effective	14.1	27.6

Effective Shear Strength - Mohr circles at failure**Effective Shear Strength - Stress Paths**

Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-29
Field Sample Reference:	Refer to Remarks	Depth (m):	-

Consolidation vs Square Root Time

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-39
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed F25, F29, F34, F37 and F39 in equal fractions.
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Test No. 1

SATURATION DATA

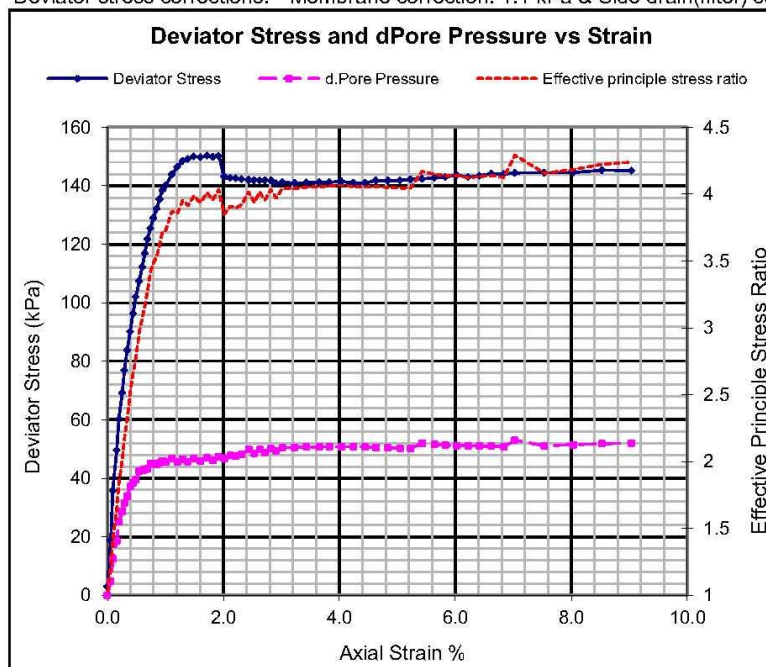
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	383.0	Final back pressure (kPa):	373.0
		Final B parameter:	0.96

CONSOLIDATION DATA

Effective cons. Stress (kPa):		96.9		t100 (minutes): 64		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.3	*50.06	1968.21	11.4	1946	0.3964	78	2.717 Determined
CONSOLIDATED	99.66	49.74	1942.95	14.1	1984	0.3695	104	
FINAL (After shear)	90.65	52.15	2135.91	14.1	1984	0.3697	104	
Initial pore pressure (kPa): 464.2		Final pore pressure (kPa): 368.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.50				
Initial pore pressure (kPa):	371.1	Initial effective stress (kPa): 96.9			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	1.72				
Deviator stress (kPa):	150.3	Principle Stresses (kPa)			
Excess pore pressure (kPa):	46.9	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	4.009	247.2	200.2	96.9	49.9
Deviator stress corrections: Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



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FEASIBILITY STUDY FOR THE MZINVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-39
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed F25, F29, F34, F37 and F39 in equal fractions.
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SATURATION DATA

Test No. 2

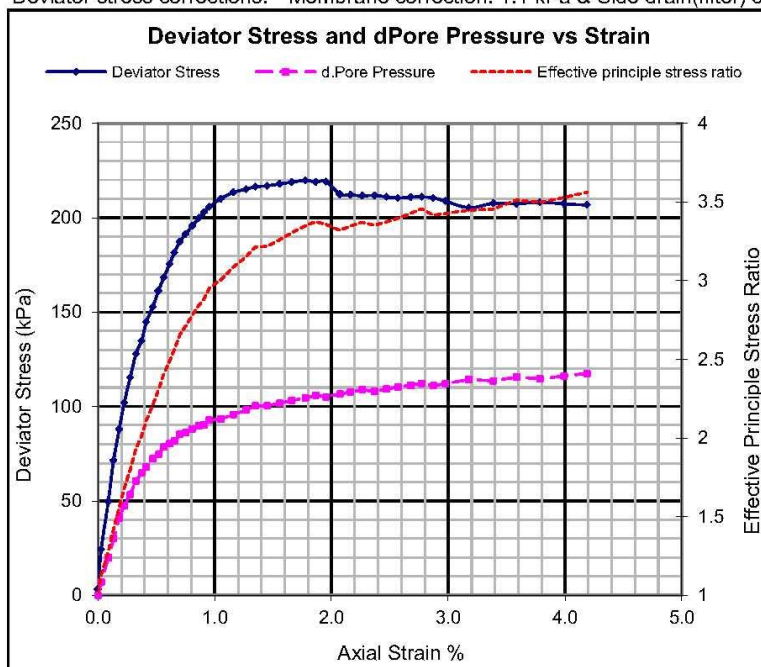
Saturation method:			Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):			50,70,100,100,100...		Differential pressure (kPa): 10.0
Final cell pressure (kPa): 343.0		Final back pressure (kPa): 333.0		Final B parameter: 0.96	

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		198.1		t100 (minutes): 25		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100.62	*50.01	1964.28	11.4	1943	0.3984	78	2.717 Determined
CONSOLIDATED	99.46	49.43	1918.84	13.7	2013	0.3499	107	
FINAL (After shear)	95.29	50.50	2002.72	13.7	2012	0.3503	106	
Initial pore pressure (kPa): 527.1		Final pore pressure (kPa): 339.5			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.30				
Initial pore pressure (kPa):	340.9	Initial effective stress (kPa): 198.1			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	1.78				
Deviator stress (kPa):	219.7	Principle Stresses (kPa)			
Excess pore pressure (kPa):	104.5	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	3.349	417.8	313.3	198.1	93.5
Deviator stress corrections: Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-39
Field Sample Number:	Refer to Remarks	Depth (m):	-

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on a remoulded sample tested saturated. Mixed F25, F29, F34, F37 and F39 in equal fractions.
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Test No. 3

SATURATION DATA

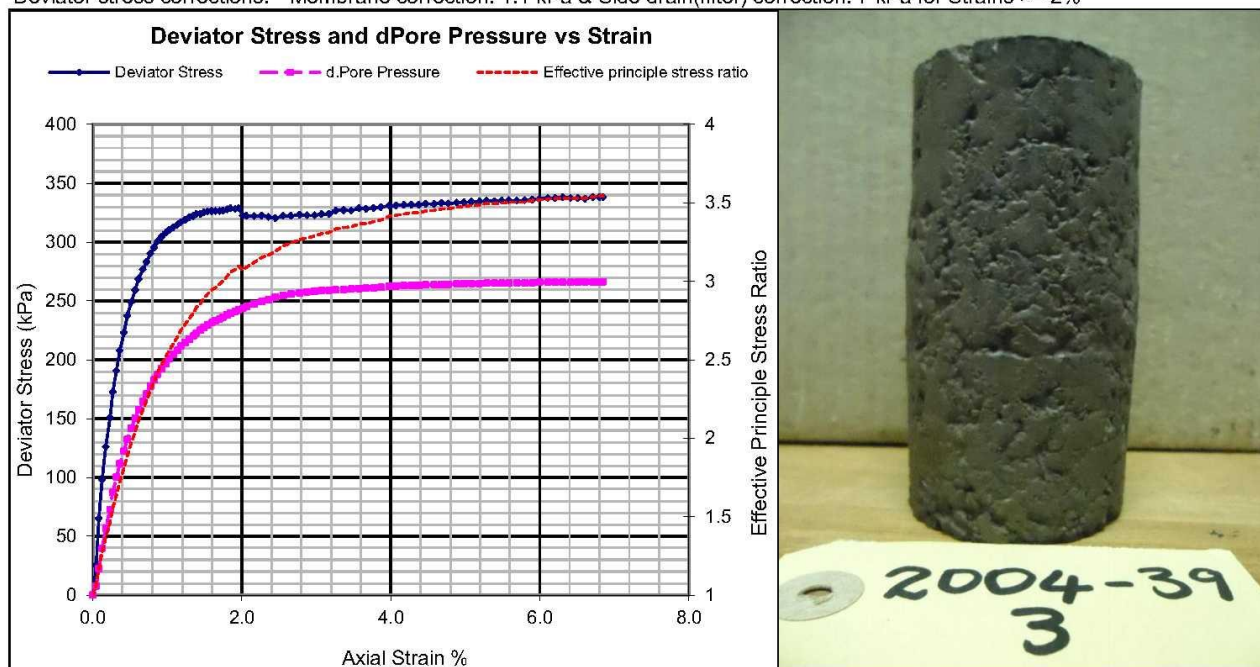
Saturation method:			Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):			50,70,100,100,100...		Differential pressure (kPa): 10.0
Final cell pressure (kPa): 353.0		Final back pressure (kPa): 343.0		Final B parameter: 0.97	

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		399.3		t100 (minutes): 120		Side drains fitted: Yes		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*99.8	*50.06	1968.21	11.7	1952	0.3920	81	2.717 Determined
CONSOLIDATED	98.33	49.32	1910.31	14.7	2042	0.3306	121	
FINAL (After shear)	91.60	51.10	2050.74	14.7	2041	0.3312	121	
Initial pore pressure (kPa): 339.5		Final pore pressure (kPa): 336.9			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.28				
Initial pore pressure (kPa):	335.7	Initial effective stress (kPa): 399.3			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	6.80				
Deviator stress (kPa):	338.2	Principle Stresses (kPa)			
Excess pore pressure (kPa):	266.3	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	3.544	737.5	471.2	399.3	132.9
Deviator stress corrections: Membrane correction: 1.1 kPa & Side drain(filter) correction: 7 kPa for Strains >= 2%					



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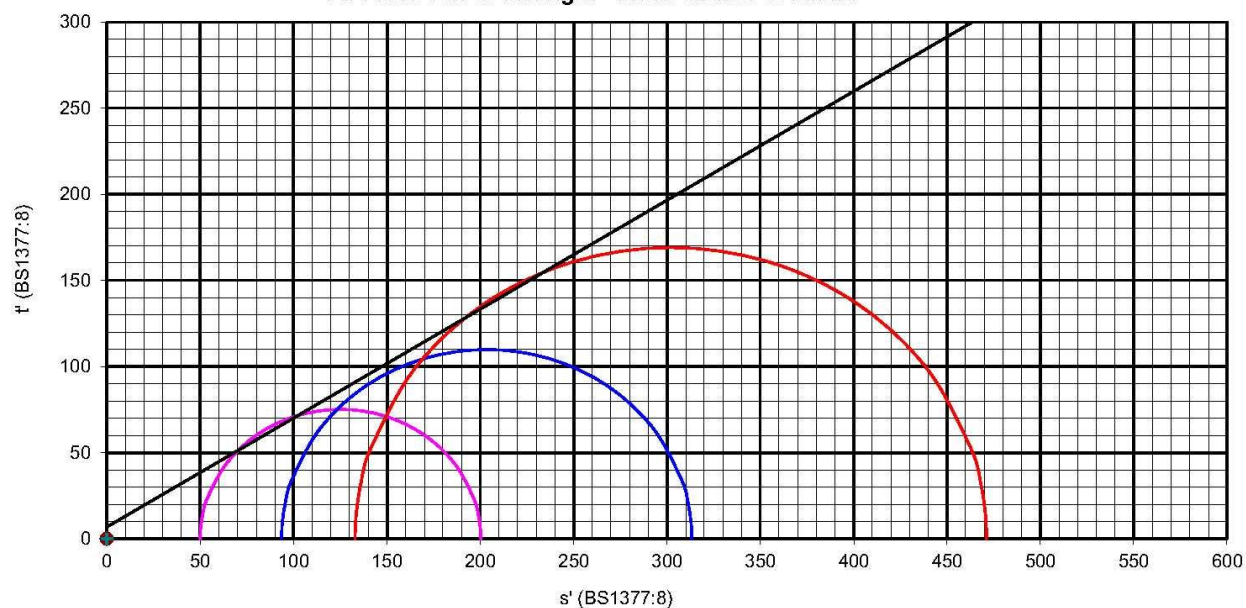
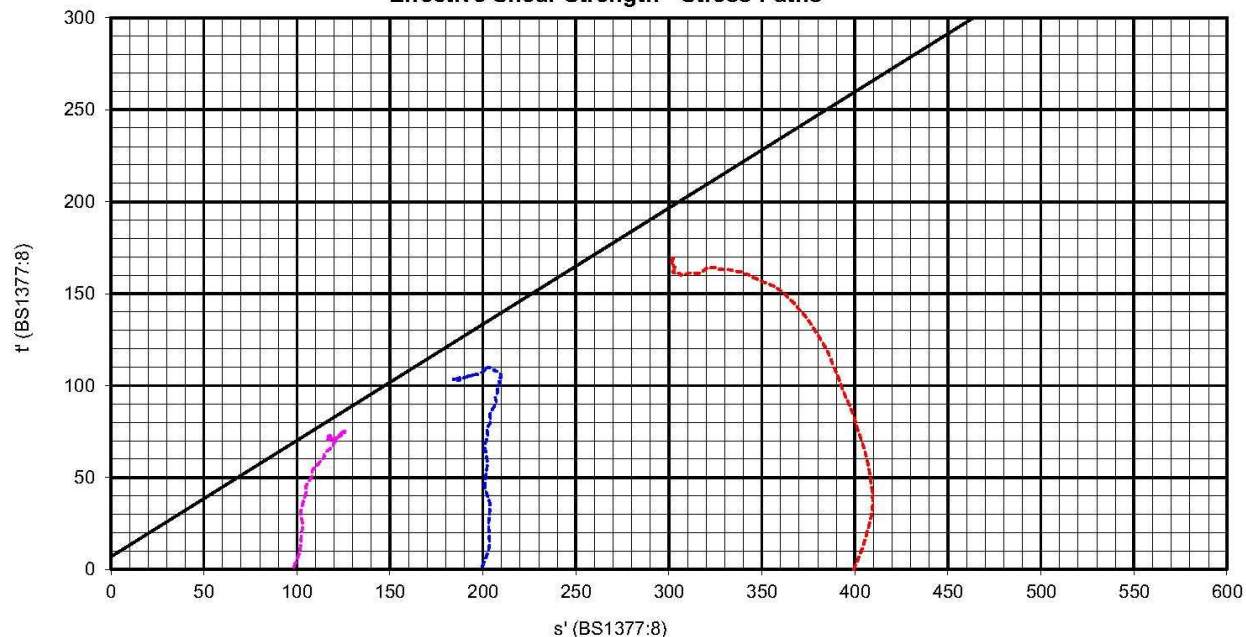
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Triaxial Compression Test Results

Project:	Mzinubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-39
Field Sample Reference:	Refer to Remarks	Depth (m):	-

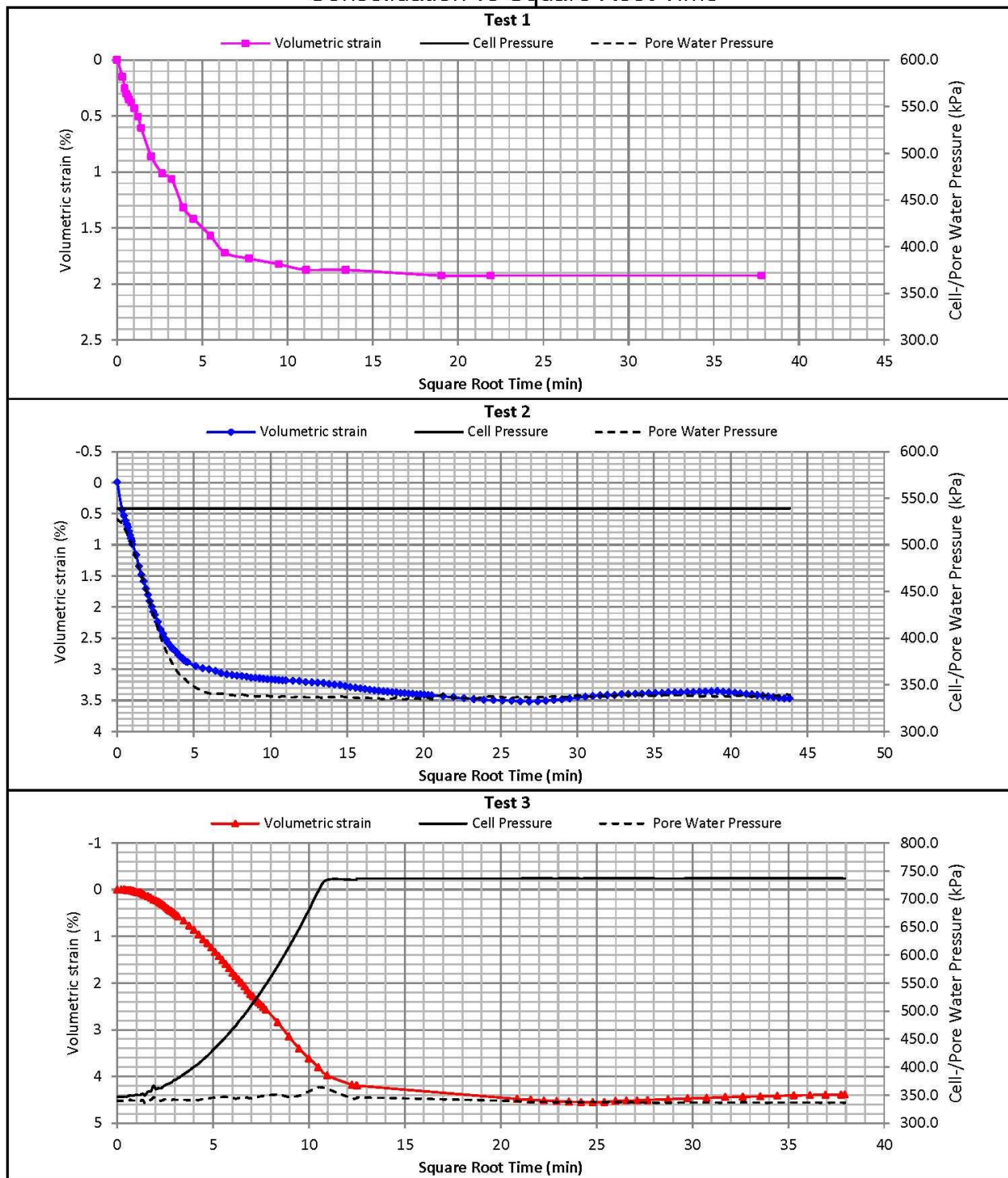
Effective Shear Strength Parameters

Stresses	Cohesion (kPa)	Internal friction (Degrees)
Total	36.7	13.6
Effective	6.9	32.3

Effective Shear Strength - Mohr circles at failure**Effective Shear Strength - Stress Paths**

Triaxial Compression Test Results

Project:	Mzinvubu Water Project	Date Received:	2013/08/23
Job Number:	2013-B-2004	Laboratory Number:	B-2004-39
Field Sample Reference:	Refer to Remarks	Depth (m):	-

Consolidation vs Square Root Time

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-2
Field Sample Number:	RF 1	Depth (m):	1.0 - 1.3

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on an undisturbed sample tested saturated.
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SATURATION DATA

Test No. 1

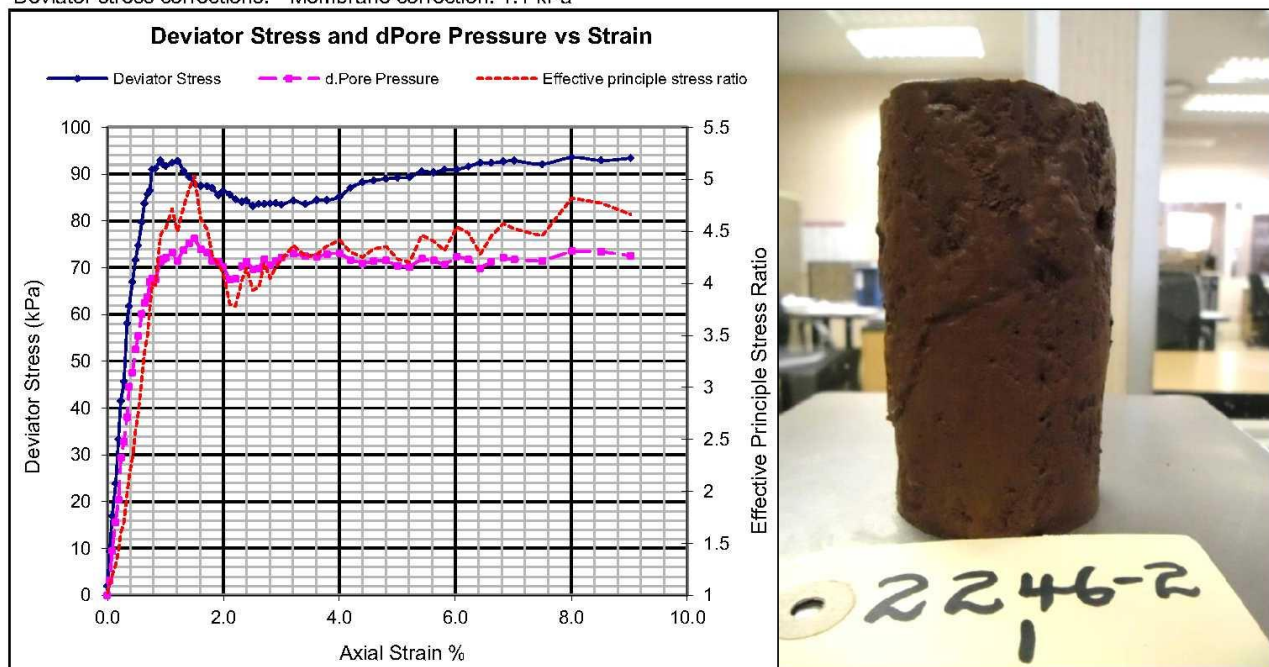
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	353.0	Final back pressure (kPa):	343.0
		Final B parameter:	1.00

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		98.1		t100 (minutes): 1		Side drains fitted: No		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*100	*50	1963.50	25.5	1433	0.8420	80	2.639 Determined
CONSOLIDATED	99.53	49.77	1945.11	30.7	1453	0.8162	99	
FINAL (After shear)	90.55	52.17	2137.95	30.7	1453	0.8162	99	
Initial pore pressure (kPa): 435.5		Final pore pressure (kPa): 347.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.40				
Initial pore pressure (kPa):	348.9	Initial effective stress (kPa): 98.1			
Parameters at failure:					
Failure Criterion:	Max. Effective Principle Stress Ratio				
Axial strain (%):	1.51				
Deviator stress (kPa):	88.0	Principle Stresses (kPa)			
Excess pore pressure (kPa):	76.2	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	5.028	186.1	109.9	98.1	21.9
Deviator stress corrections: Membrane correction: 1.1 kPa					



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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-2
Field Sample Number:	RF 1	Depth (m):	1.0 - 1.3

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on an undisturbed sample tested saturated.
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SATURATION DATA

Test No. 2

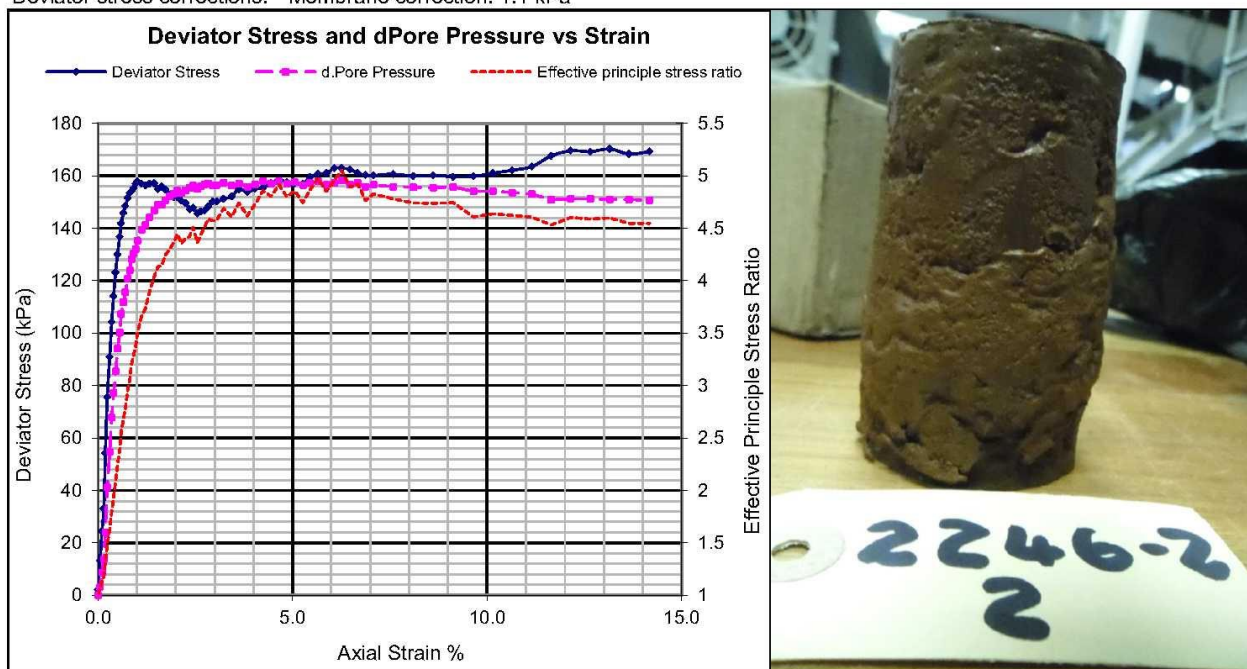
Saturation method: Alternating increments of cell- & back pressure			
Pressure increments applied (kPa): 50,70,100,100,100...		Differential pressure (kPa): 10.0	
Final cell pressure (kPa): 353.0	Final back pressure (kPa): 343.0	Final B parameter: 0.99	

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		198.3		t100 (minutes): 1		Side drains fitted: No		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*99.84	*50.07	1969.00	21.4	1561	0.6910	82	2.639 Determined
CONSOLIDATED	98.91	49.60	1932.32	24.5	1606	0.6437	100	
FINAL (After shear)	84.89	53.54	2251.42	24.5	1605	0.6440	100	
Initial pore pressure (kPa): 535.7		Final pore pressure (kPa): 349.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.30				
Initial pore pressure (kPa):	350.7	Initial effective stress (kPa): 198.3			
Parameters at failure:					
Failure Criterion:	Max. Effective Principle Stress Ratio				
Axial strain (%):	6.26				
Deviator stress (kPa):	162.9	Principle Stresses (kPa)			
Excess pore pressure (kPa):	158.1	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	5.051	361.2	203.1	198.3	40.2
Deviator stress corrections: Membrane correction: 1.1 kPa					



Civilab (Proprietary) Limited. Registration No.: 1998/019071/07

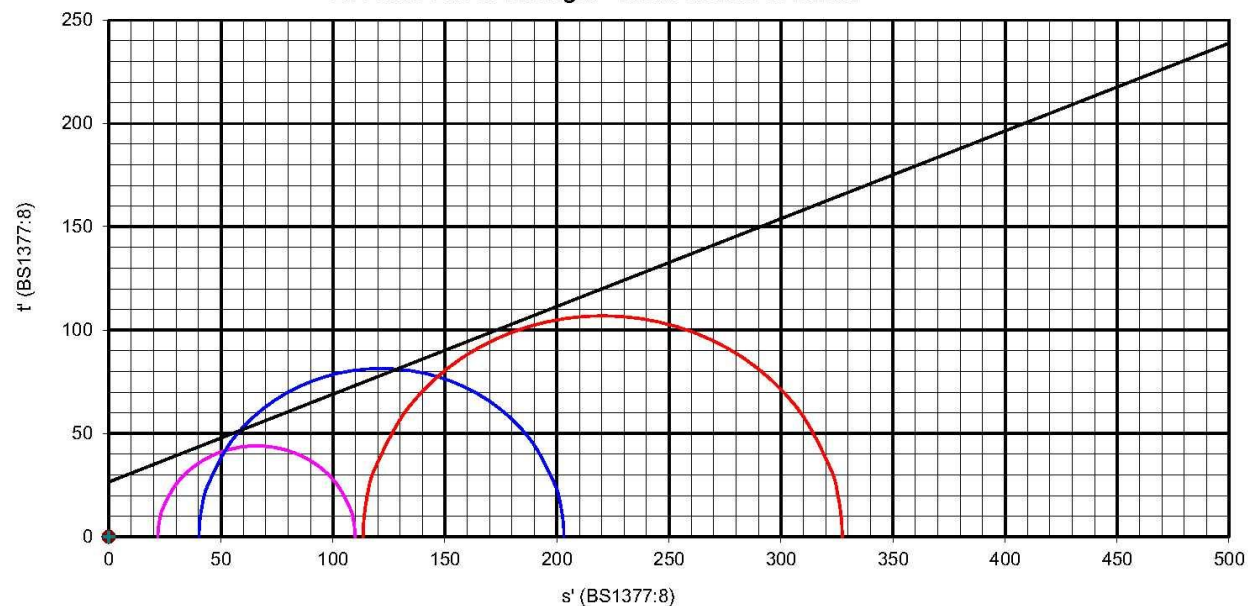
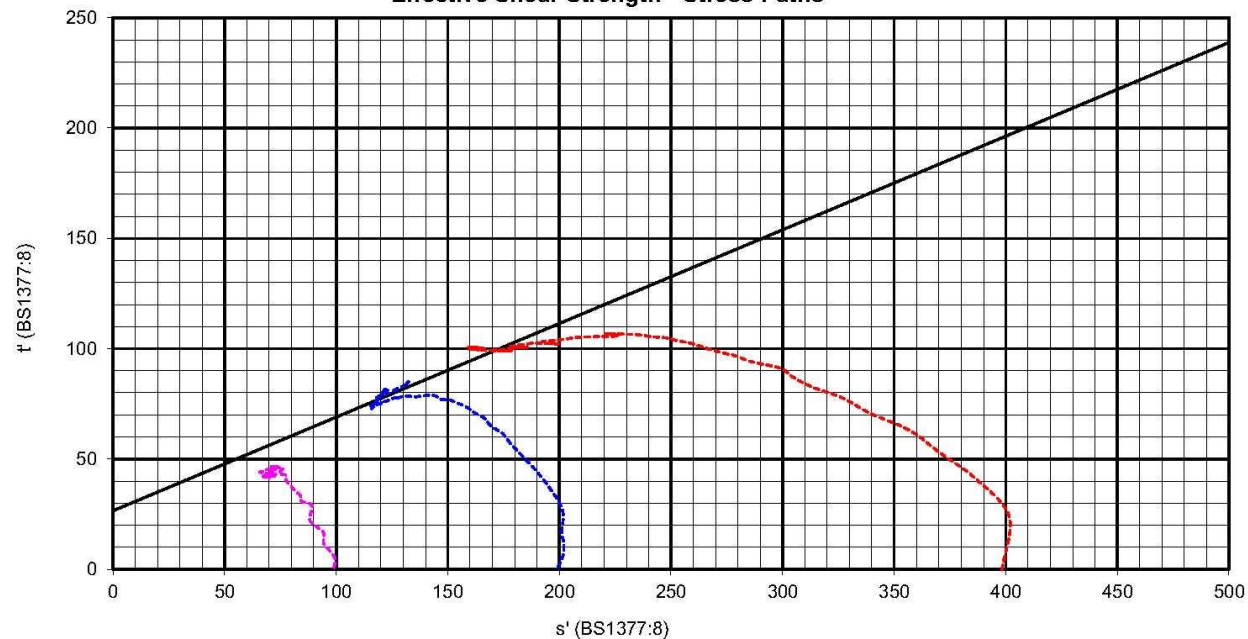
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Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-2
Field Sample Reference:	RF 1	Depth (m):	1.0 - 1.3

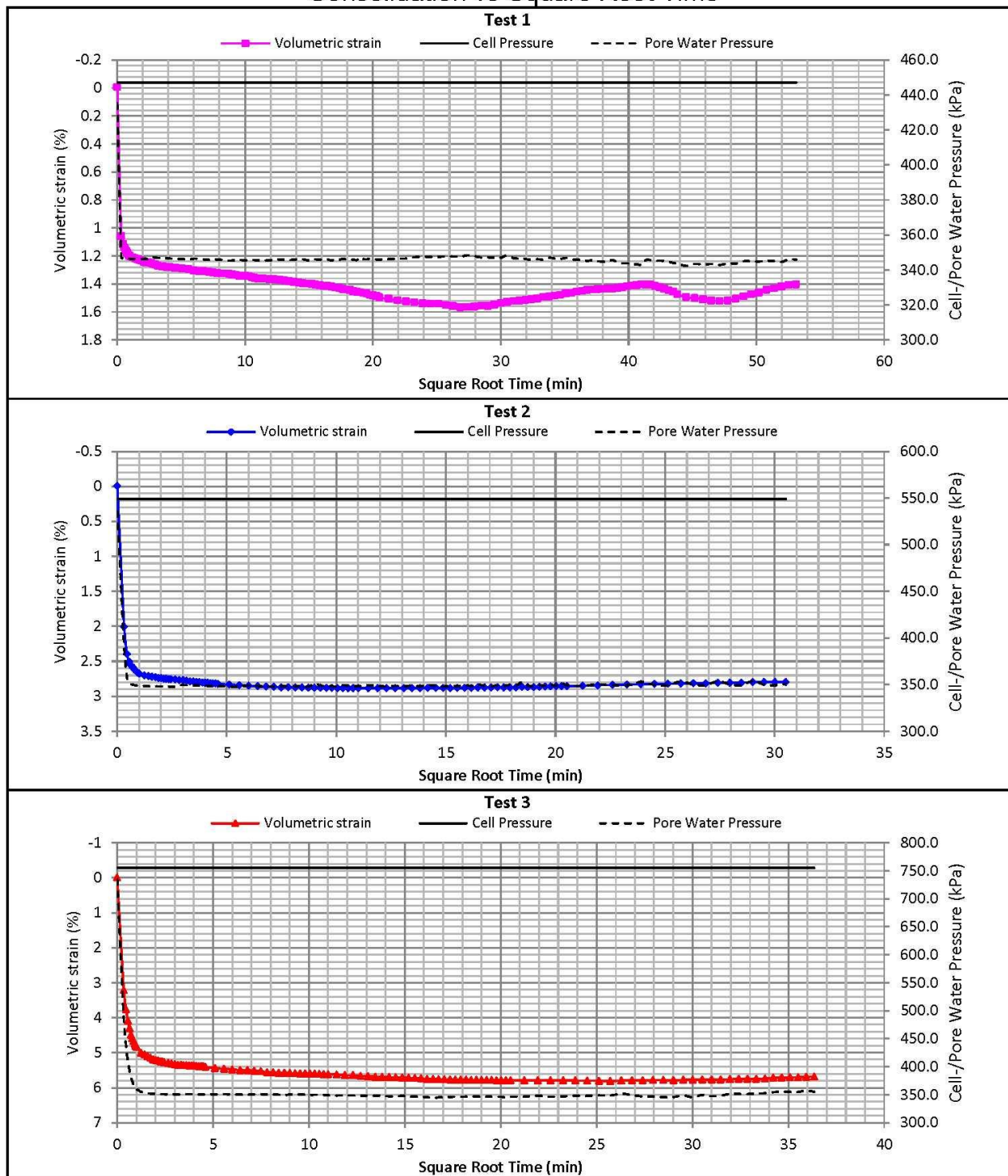
Effective Shear Strength Parameters

Stresses	Cohesion (kPa)	Internal friction (Degrees)
Total	26.1	9.6
Effective	26.5	23.0

Effective Shear Strength - Mohr circles at failure**Effective Shear Strength - Stress Paths**

Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-2
Field Sample Reference:	RF 1	Depth (m):	1.0 - 1.3

Consolidation vs Square Root Time

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-3
Field Sample Number:	LF 1 Top	Depth (m):	1.0 - 1.2

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on an undisturbed sample tested saturated.
----------	--

Test No. 1

SATURATION DATA

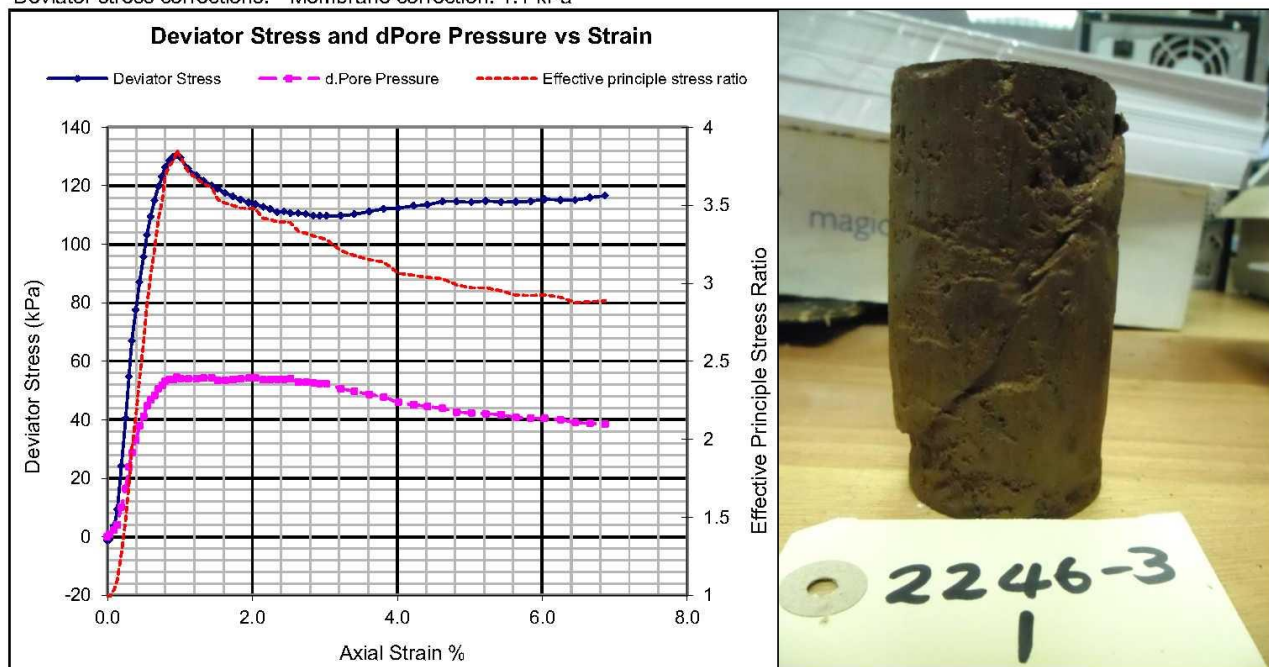
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	353.0	Final back pressure (kPa):	343.0
		Final B parameter:	0.97

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		100.3		t100 (minutes): 4		Side drains fitted: No		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*99.62	*49.99	1962.71	38.9	1118	1.2165	79	2.477 Determined
CONSOLIDATED	99.23	49.79	1947.26	52.7	1131	1.1904	110	
FINAL (After shear)	92.41	51.60	2090.83	52.7	1131	1.1904	110	
Initial pore pressure (kPa): 432.4		Final pore pressure (kPa): 346.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.30				
Initial pore pressure (kPa):	345.7	Initial effective stress (kPa): 100.3			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	0.96				
Deviator stress (kPa):	130.4	Principle Stresses (kPa)			
Excess pore pressure (kPa):	54.6	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	3.851	230.8	176.2	100.3	45.8
Deviator stress corrections: Membrane correction: 1.1 kPa					



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FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-3
Field Sample Number:	LF 1 Top	Depth (m):	1.0 - 1.2

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks:	A Consolidated Undrained test on an undisturbed sample tested saturated.
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SATURATION DATA

Test No. 2

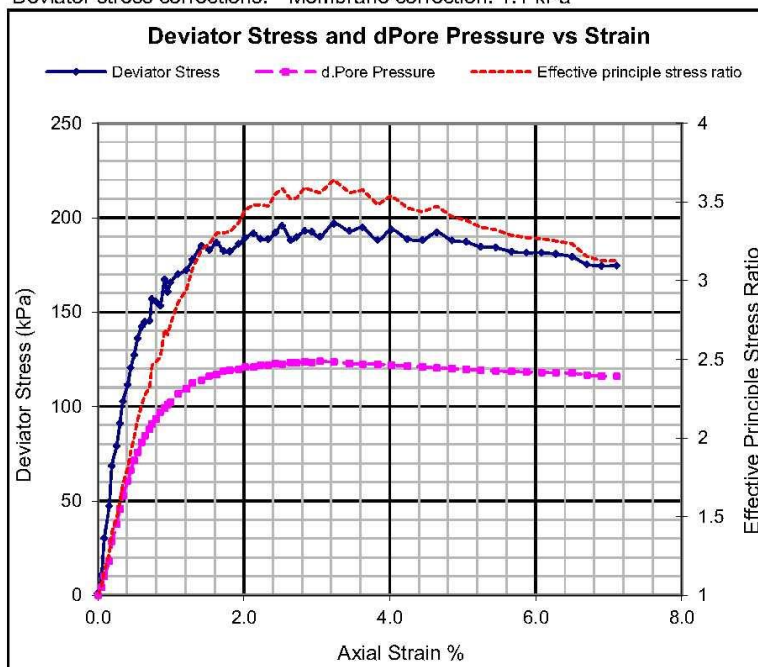
Saturation method: Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa): 10.0
Final cell pressure (kPa): 353.0	Final back pressure (kPa): 343.0	Final B parameter: 1.00

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		198.1		t100 (minutes): 4		Side drains fitted: No		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*99.74	*49.71	1940.78	38.7	1121	1.2096	79	2.477 Determined
CONSOLIDATED	98.42	49.05	1889.27	50.5	1168	1.1216	111	
FINAL (After shear)	91.41	50.89	2033.96	50.5	1167	1.1224	111	
Initial pore pressure (kPa): 533.9		Final pore pressure (kPa): 347.0			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour): 0.50					
Initial pore pressure (kPa): 347.9		Initial effective stress (kPa): 198.1			
Parameters at failure:					
Failure Criterion:		Max. Deviator Stress			
Axial strain (%): 3.23					
Deviator stress (kPa): 196.7		Principle Stresses (kPa)			
Excess pore pressure (kPa): 123.6		σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio: 3.641		394.8	271.2	198.1	74.5
Deviator stress corrections: Membrane correction: 1.1 kPa					



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Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-3
Field Sample Number:	LF 1 Top	Depth (m):	1.0 - 1.2

This test was carried out in accordance with BS 1377:Part 8:1990 Clause 4,5,6,7

Remarks: A Consolidated Undrained test on an undisturbed sample tested saturated.

Test No. 3**SATURATION DATA**

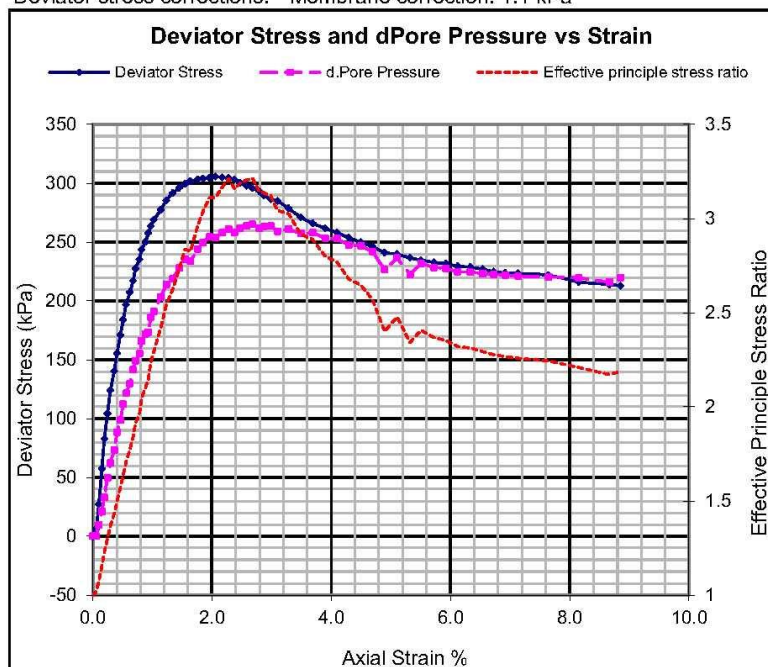
Saturation method:	Alternating increments of cell- & back pressure		
Pressure increments applied (kPa):	50,70,100,100,100...	Differential pressure (kPa):	10.0
Final cell pressure (kPa):	353.0	Final back pressure (kPa):	343.0
		Final B parameter:	0.96

CONSOLIDATION DATA

CONSOLIDATION DATA								
Effective cons. Stress (kPa):		398.6		t100 (minutes): 16		Side drains fitted: No		
	Height mm	Diameter mm	Area mm ²	Moisture Content %	Dry Density kg/m ³	Void Ratio	Saturation %	Specific Gravity
INITIAL (Before saturation)	*99.58	*50.14	1974.51	34.7	1136	1.1801	73	2.477 Determined
CONSOLIDATED	98.14	49.41	1917.55	47.1	1188	1.0858	107	
FINAL (After shear)	89.45	51.76	2103.89	47.1	1187	1.0867	107	
Initial pore pressure (kPa): 730.1		Final pore pressure (kPa): 349.5			PWP dissipation (%): 100			
*: Measured dimensions; all other dimensions are calculated.								

SHEAR DATA

Rate of strain (%/hour):	0.35				
Initial pore pressure (kPa):	349.4	Initial effective stress (kPa): 398.6			
Parameters at failure:					
Failure Criterion:	Max. Deviator Stress				
Axial strain (%):	2.06				
Deviator stress (kPa):	305.6	Principle Stresses (kPa)			
Excess pore pressure (kPa):	253.9	σ_1	σ_1'	σ_3	σ_3'
Effective principle stress ratio:	3.111	704.2	450.3	398.6	144.8
Deviator stress corrections: Membrane correction: 1.1 kPa					

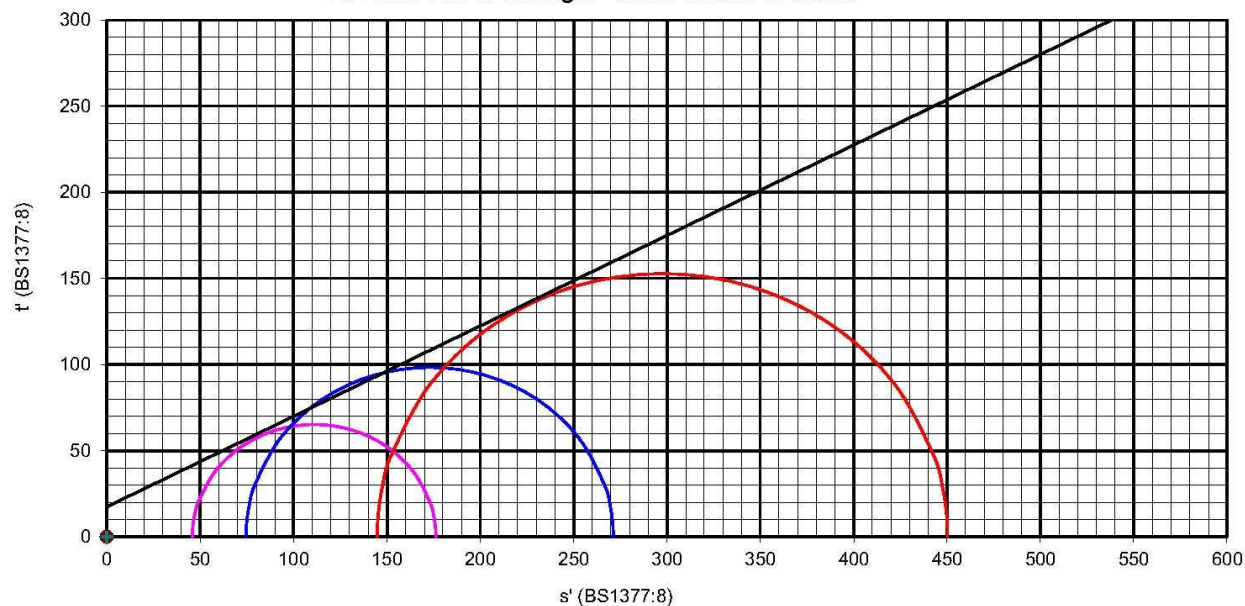
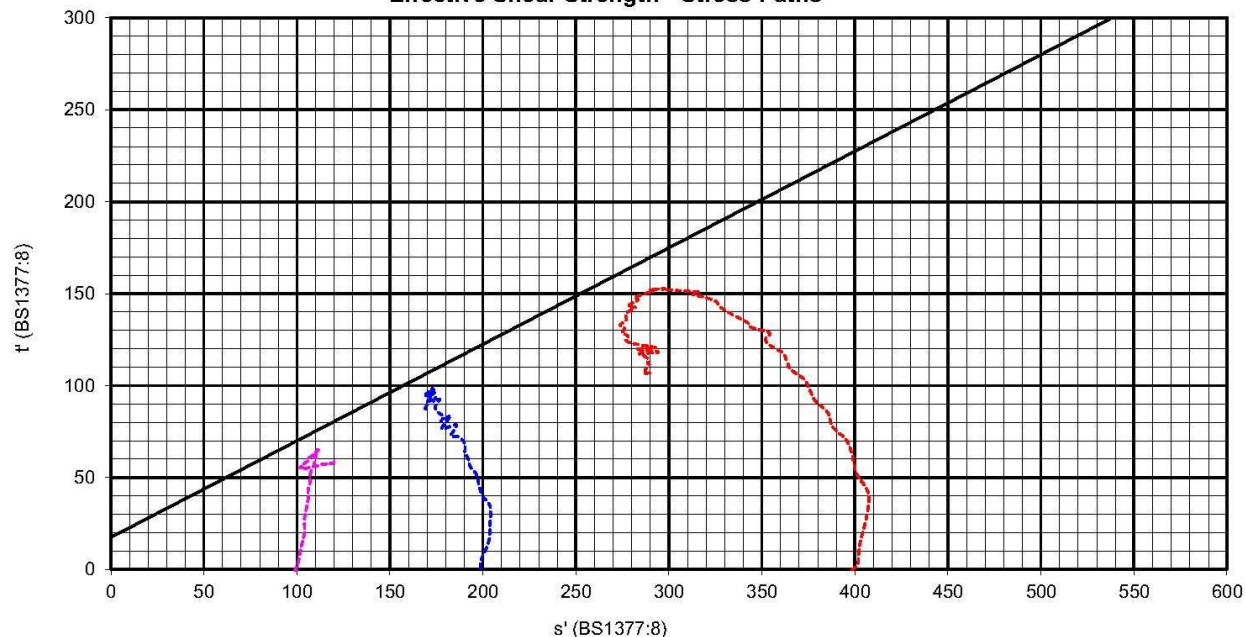


Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-3
Field Sample Reference:	LF 1 Top	Depth (m):	1.0 - 1.2

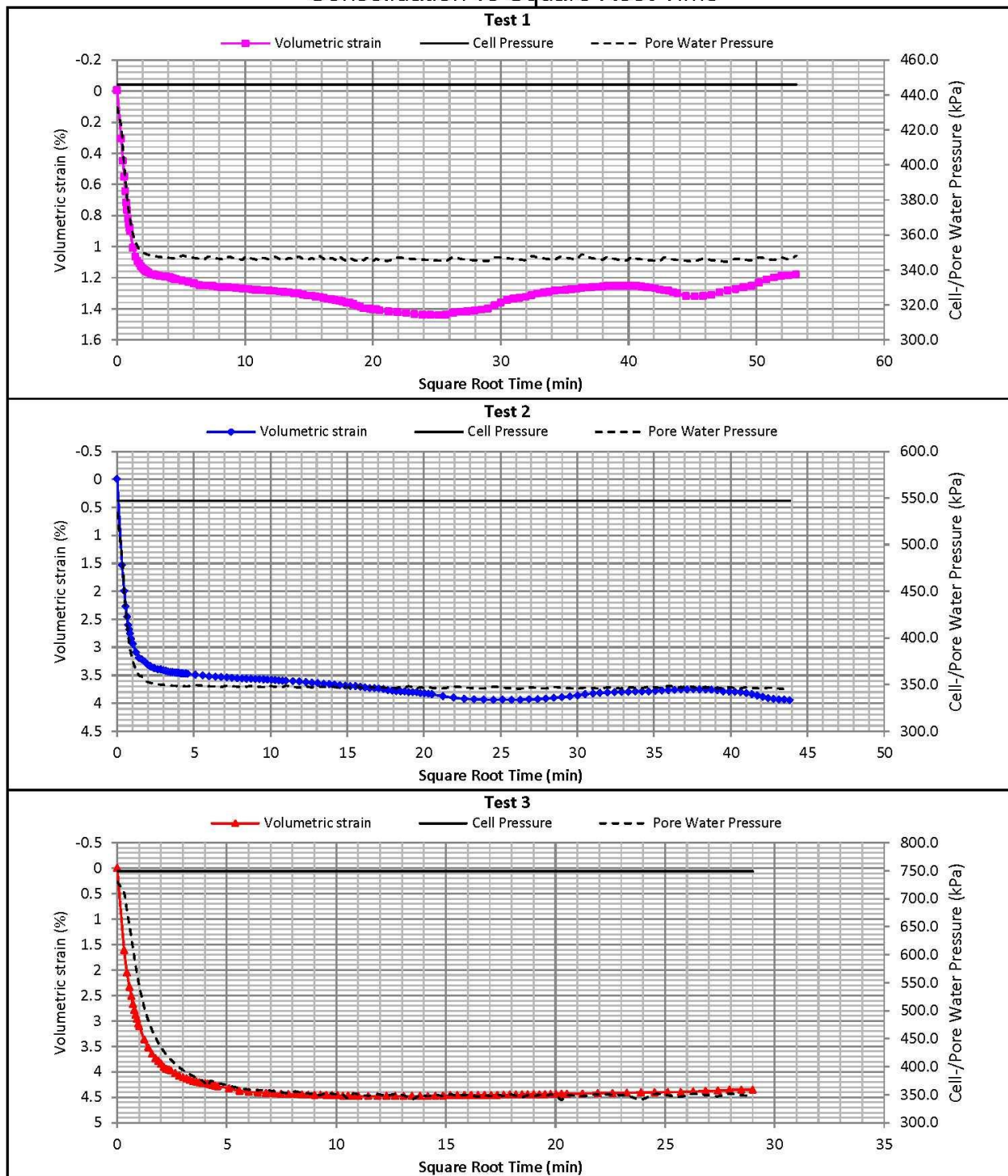
Effective Shear Strength Parameters

Stresses	Cohesion (kPa)	Internal friction (Degrees)
Total	30.2	13.0
Effective	17.4	27.7

Effective Shear Strength - Mohr circles at failure**Effective Shear Strength - Stress Paths**

Triaxial Compression Test Results

Project:	Mzimvubu Water Project	Date Received:	2013/10/07
Job Number:	2013-B-2246	Laboratory Number:	B-2246-3
Field Sample Reference:	LF 1 Top	Depth (m):	1.0 - 1.2

Consolidation vs Square Root Time

H 6

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Consolidation Tests

Project:				MZIMVUBU WATER PROJECT				Test 1	
Project No.:		2013-B-2246		Sample No.:		2246-3A			
Borehole No:		LF 1 TOP		Depth:		1.0 - 1.2			
Date Received:		07/10/2013		Date Tested:		02/12/2013			
Remarks:		An undisturbed sample tested soaked.							
Machine No.		5	Ring No.	16	Height (mm)	19.95	Diameter (mm)	75.95	

Masses for Water Content Determination (g)

Wet Sample and Ring		Dry Sample and Ring	Ring Only	Water Content	
Before Test	After Test			Before Test	After Test
244.6	253.6	206.7	106.78	37.9%	46.9%

Pre-Determined Particle Specific Gravity 2.477

Initial Parameters

Void Ratio	1.2406	Degree of Saturation (%)	75.7	Dry Density (Kg/m3)	1106
------------	--------	--------------------------	------	---------------------	------

Effect. Stress (kPa)		10	50	100	200	400	800	1600	400	100	10	0
Dial Correction (u)		0	37	68	101	170	220	321	196	112	45	0
HH:MM:SS	√Minutes	Dial Readings in Microns								Initial Dial Reading		13504
00:00:00	0.00	13504		13388		13123		11934				
00:00:06	0.32			13384		12914		11370				
00:00:12	0.45			13383		12902		11340				
00:00:18	0.55			13381		12893		11316				
00:00:24	0.63			13381		12888		11296				
00:00:30	0.71			13380		12886		11278				
00:00:42	0.84			13378		12880		11252				
00:01:00	1.00			13377		12873		11218				
00:01:30	1.22			13375		12866		11178				
00:02:00	1.41			13373		12861		11148				
00:04:00	2.00			13369		12850		11071				
00:07:00	2.65			13367		12838		10992				
00:10:00	3.16			13364		12834		10974				
00:15:00	3.87			13362		12824		10946				
00:20:00	4.47			13361		12820		10920				
00:30:00	5.48			13359		12819		10895				
00:40:00	6.32			13357		12814		10868				
01:00:00	7.75			13353		12807						
01:30:00	9.49			13350		12800		10837				
02:00:00	10.95			13349		12794		10824	11031	11374		
03:00:00	13.42			13345		12784		10807			11790	
04:00:00	15.49			13342		12778		10790				
06:00:00	18.97			13336		12769		10780				
08:00:00	21.91	13619				12764		10770				
16:00:00	30.98		13471									
24:00:00	37.95				13123	12755	11934	10745				
72:00:00	65.73			13328								
End of Primary Cons		13619	13471	13328	13123	12755	11934	10745	11031	11374	11790	
Number of Readings:		2	1	24	1	25	1	24	1	1	1	0

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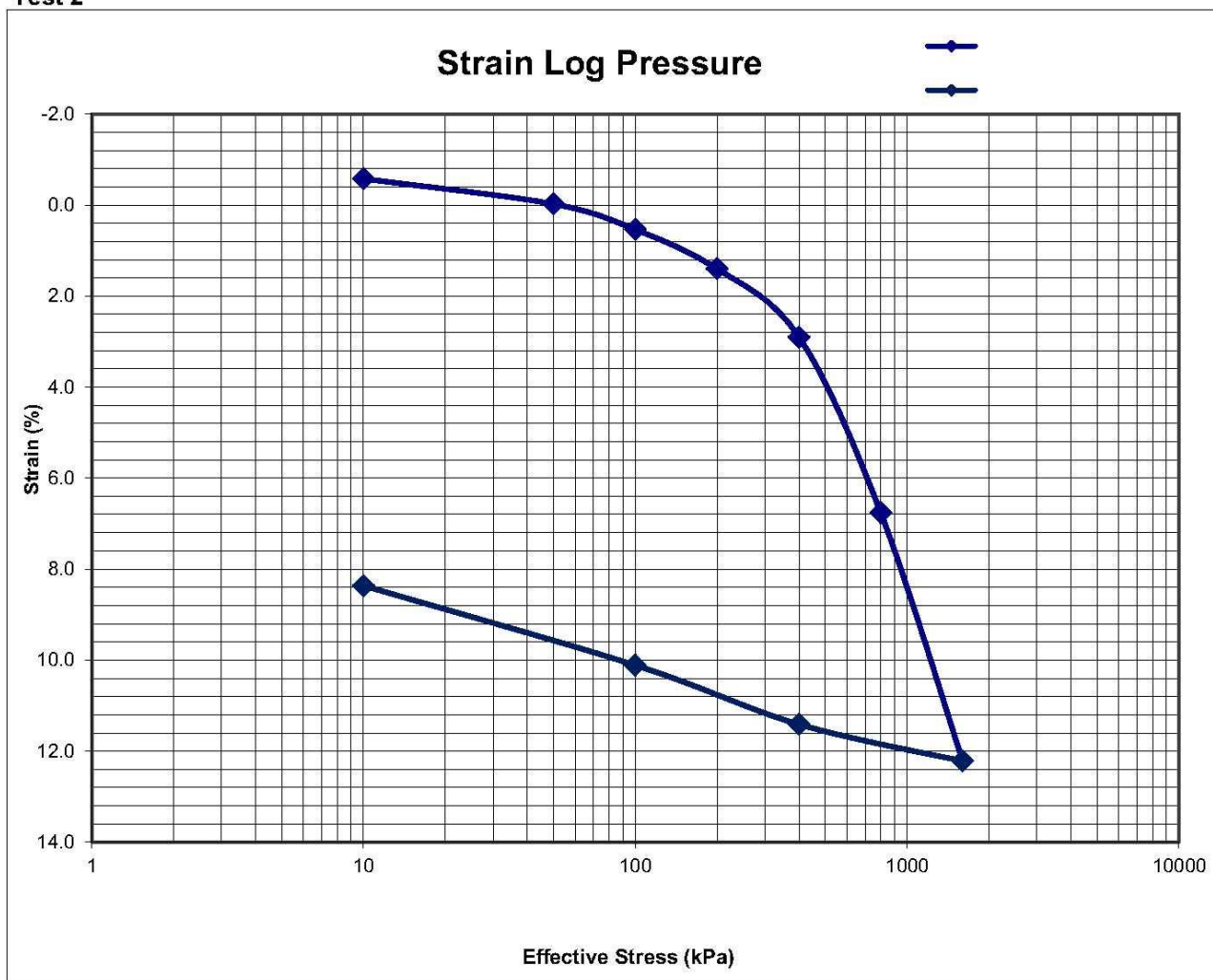
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2246	Sample No.:		2246-3A						
Borehole No:	LF 1 TOP	Depth:		1.0 - 1.2						
Date Received:	07/10/2013	Date Tested:		02/12/2013						

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.58	-0.02	0.54	1.40	2.90	6.77	12.22	11.41	10.12	8.37	
Mv (1/MPa)		0.1391	0.1123	0.0862	0.0749	0.0966	0.0682	0.0067	0.0433	0.1944	
Void Ratio	1.2535	1.241	1.2285	1.2091	1.1756	1.089	0.9668	0.9849	1.0139	1.0531	

Test 2



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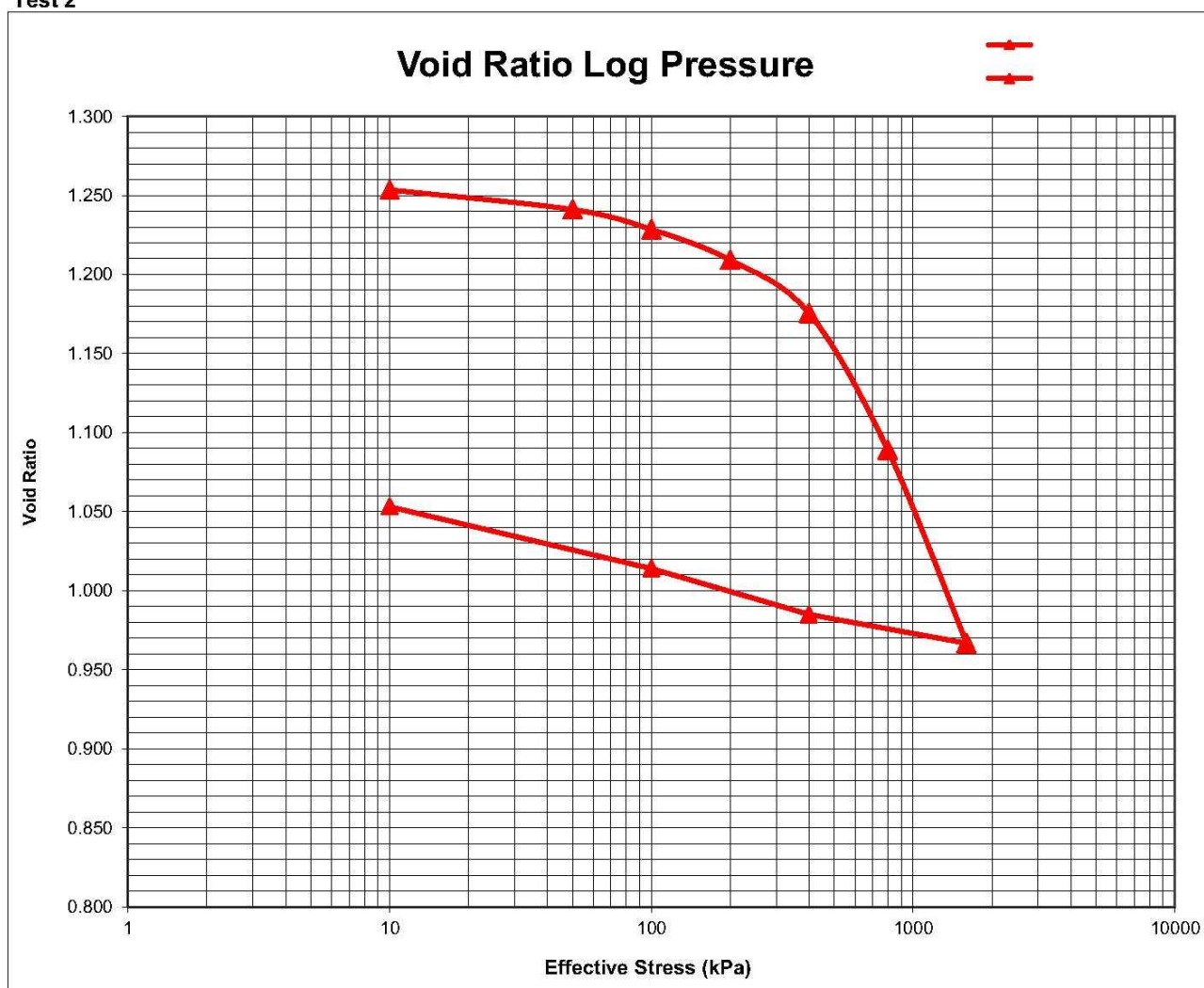
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2246					Sample No.:	2246-3A			
Borehole No:	LF 1 TOP					Depth:	1.0 - 1.2			
Date Received:	07/10/2013					Date Tested:	02/12/2013			

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.58	-0.02	0.54	1.40	2.90	6.77	12.22	11.41	10.12	8.37	
Mv (1/MPa)		0.1391	0.1123	0.0862	0.0749	0.0966	0.0682	0.0067	0.0433	0.1944	
Void Ratio	1.2535	1.241	1.2285	1.2091	1.1756	1.089	0.9668	0.9849	1.0139	1.0531	

Test 2



Falling Head Permeability Test Results

Project:	MZINVUBU WATER PROJECT		
Project No:	2013-B-2004	Date:	17/10/2013

[illegible]

Remarks:	<p>Samples remoulded to 98% Proctor.</p> <p>* = Samples remoulded to 95% Proctor.</p> <p>Saturated and tested under a load of 100kPa.</p> <p>Densities reported are under a load of 100kPa.</p>
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Interim results

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Consolidation Tests

Project:				MZIMVUBU WATER PROJECT				Test 1	
Project No.:		2013-B-2246		Sample No.:		2246-2A			
Borehole No:		RF 1		Depth:		1.0 - 1.3			
Date Received:		07/10/2013		Date Tested:		02/12/2013			
Remarks:		An undisturbed sample tested soaked.							
Machine No.		6	Ring No.	26	Height (mm)	18.7	Diameter (mm)	75.6	

Masses for Water Content Determination (g)

Wet Sample and Ring		Dry Sample and Ring	Ring Only	Water Content	
Before Test	After Test			Before Test	After Test
243.2	242.7	214.2	93.08	23.9%	23.5%

Pre-Determined Particle Specific Gravity 2.639

Initial Parameters

Void Ratio	0.8289	Degree of Saturation (%)	76.2	Dry Density (Kg/m ³)	1443
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Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	0
Dial Correction (u)	0	50	82	122	189	299	417	231	117	42	0
HH:MM:SS	√Minutes	Dial Readings in Microns						Initial Dial Reading			
00:00:00	0.00	13794		13611		12883		11171			13794
00:00:06	0.32			13460		12387		10478			
00:00:12	0.45			13450		12365		10446			
00:00:18	0.55			13444		12346		10423			
00:00:24	0.63			13441		12335		10407			
00:00:30	0.71			13438		12324		10397			
00:00:40	0.82					12312					
00:00:42	0.84			13433				10376			
00:01:00	1.00			13429		12297		10356			
00:01:30	1.22			13423		12281		10338			
00:02:00	1.41			13418		12271		10324			
00:04:00	2.00			13411		12256		10296			
00:07:00	2.65			13400		12228		10273			
00:10:00	3.16			13399		12221		10264			
00:15:00	3.87			13394		12210		10254			
00:20:00	4.47			13390		12203		10246			
00:30:00	5.48			13388		12193		10237			
00:40:00	6.32			13385		12185		10227			
01:00:00	7.75			13378		12180					
01:30:00	9.49			13373		12175		10214			
02:00:00	10.95			13371		12160		10209	10458	10703	
03:00:00	13.42			13367		12148		10200			10962
04:00:00	15.49			13362		12143		10193			
06:00:00	18.97			13355		12135		10188			
08:00:00	21.91	13791				12130		10183			
16:00:00	30.98		13611								
24:00:00	37.95				12883	12122	11171	10173			
72:00:00	65.73			13340							
End of Primary Cons		13791	13611	13340	12883	12122	11171	10173	10458	10703	10962
Number of Readings:		2	1	24	1	25	1	24	1	1	1

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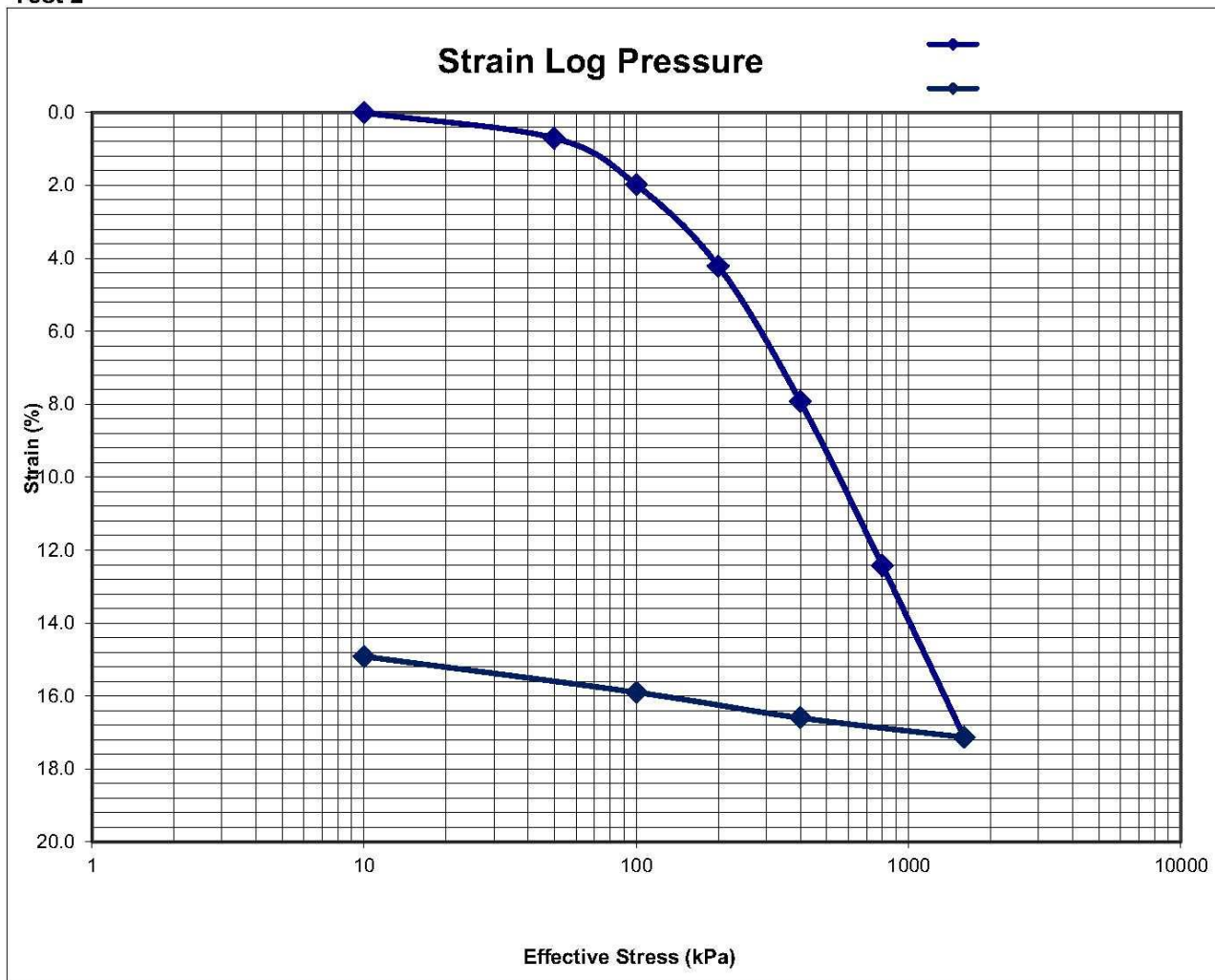
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2246	Sample No.:		2246-2A						
Borehole No:	RF 1	Depth:		1.0 - 1.3						
Date Received:	07/10/2013	Date Tested:		02/12/2013						

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	0.02	0.71	1.99	4.22	7.93	12.43	17.13	16.60	15.90	14.92	
Mv (1/MPa)		0.1738	0.2556	0.2230	0.1856	0.1124	0.0588	0.0044	0.0234	0.1093	
Void Ratio	0.8286	0.8159	0.7926	0.7518	0.6839	0.6016	0.5156	0.5253	0.5381	0.5561	

Test 2



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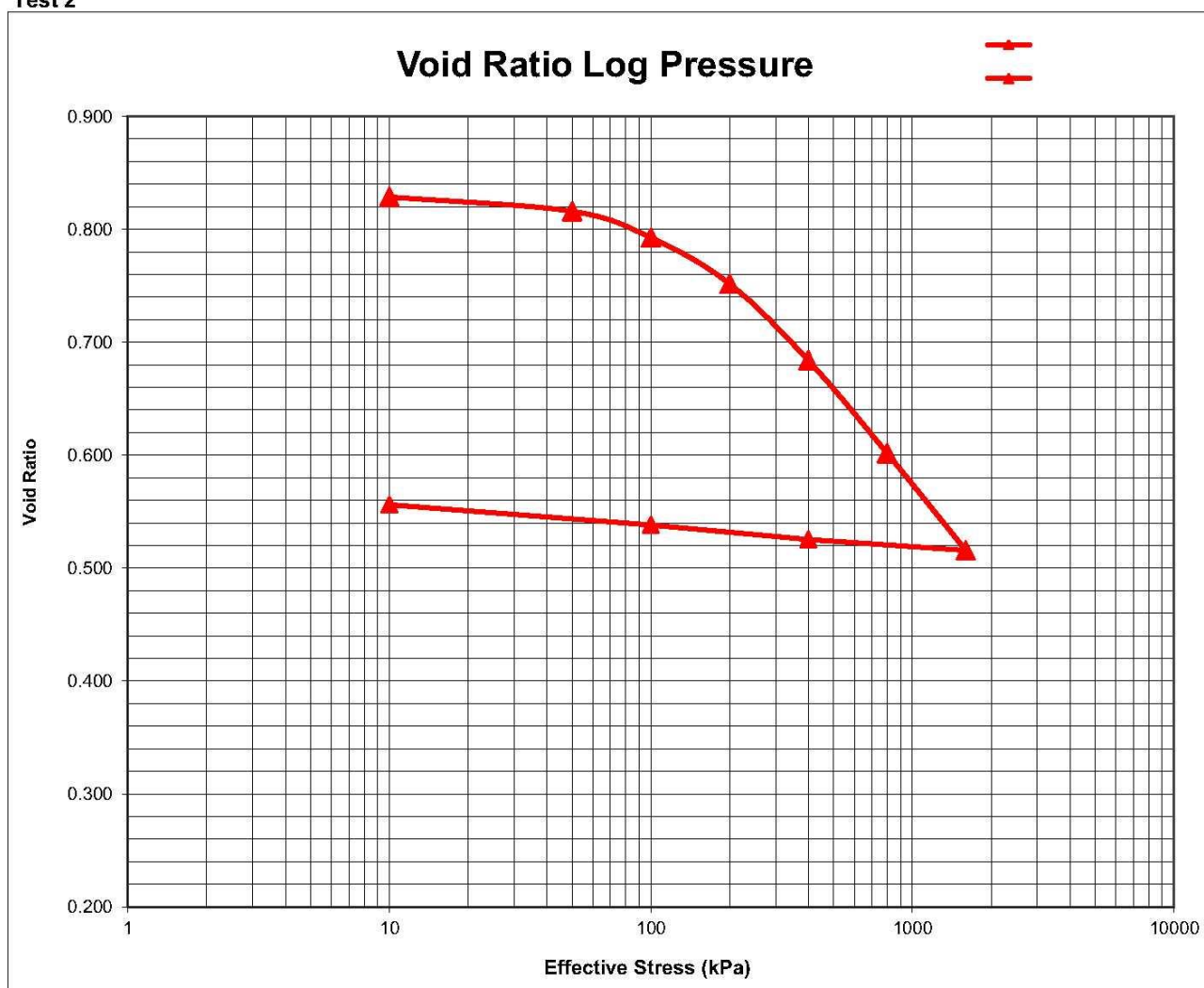
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2246					Sample No.:	2246-2A			
Borehole No:	RF 1					Depth:	1.0 - 1.3			
Date Received:	07/10/2013					Date Tested:	02/12/2013			

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	0.02	0.71	1.99	4.22	7.93	12.43	17.13	16.60	15.90	14.92	
Mv (1/MPa)		0.1738	0.2556	0.2230	0.1856	0.1124	0.0588	0.0044	0.0234	0.1093	
Void Ratio	0.8286	0.8159	0.7926	0.7518	0.6839	0.6016	0.5156	0.5253	0.5381	0.5561	

Test 2



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Consolidation Tests

Project:		MZIMVUBU WATER PROJECT						Test 1			
Project No.:		2013-B-2004			Sample No.:		2004-11				
Borehole No:		Mix C2+C4A+C7+C8+C10			Depth:		0.4 - 2.5				
Date Received:		23/08/2013			Date Tested:		21/10/2013				
Remarks:		A remoulded sample tested soaked.									
Machine No.		1	Ring No.		4	Height (mm)		19.45	Diameter (mm)		75.55

Masses for Water Content Determination (g)

Wet Sample and Ring		Dry Sample and Ring	Ring Only	Water Content	
Before Test	After Test			Before Test	After Test
250.9	241.0	210.7	87.13	32.5%	24.5%

Pre-Determined Particle Specific Gravity 2.506

Initial Parameters

Void Ratio	0.7683	Degree of Saturation (%)	106.1	Dry Density (Kg/m ³)	1417
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Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	0
Dial Correction (u)	0	39	65	96	137	194	284	182	123	65	0
HH:MM:SS	√Minutes	Dial Readings in Microns								Initial Dial Reading	
00:00:00	0.00	12824									12824
02:00:00	10.95							9028	9240		
03:00:00	13.42									9489	
18:00:00	32.86	12766									
24:00:00	37.95		12107		11096	10206	9491	8814			
72:00:00	65.73			11641							
End of Primary Cons		12766	12107	11641	11096	10206	9491	8814	9028	9240	9489
Number of Readings:		2	1	1	1	1	1	1	1	1	0

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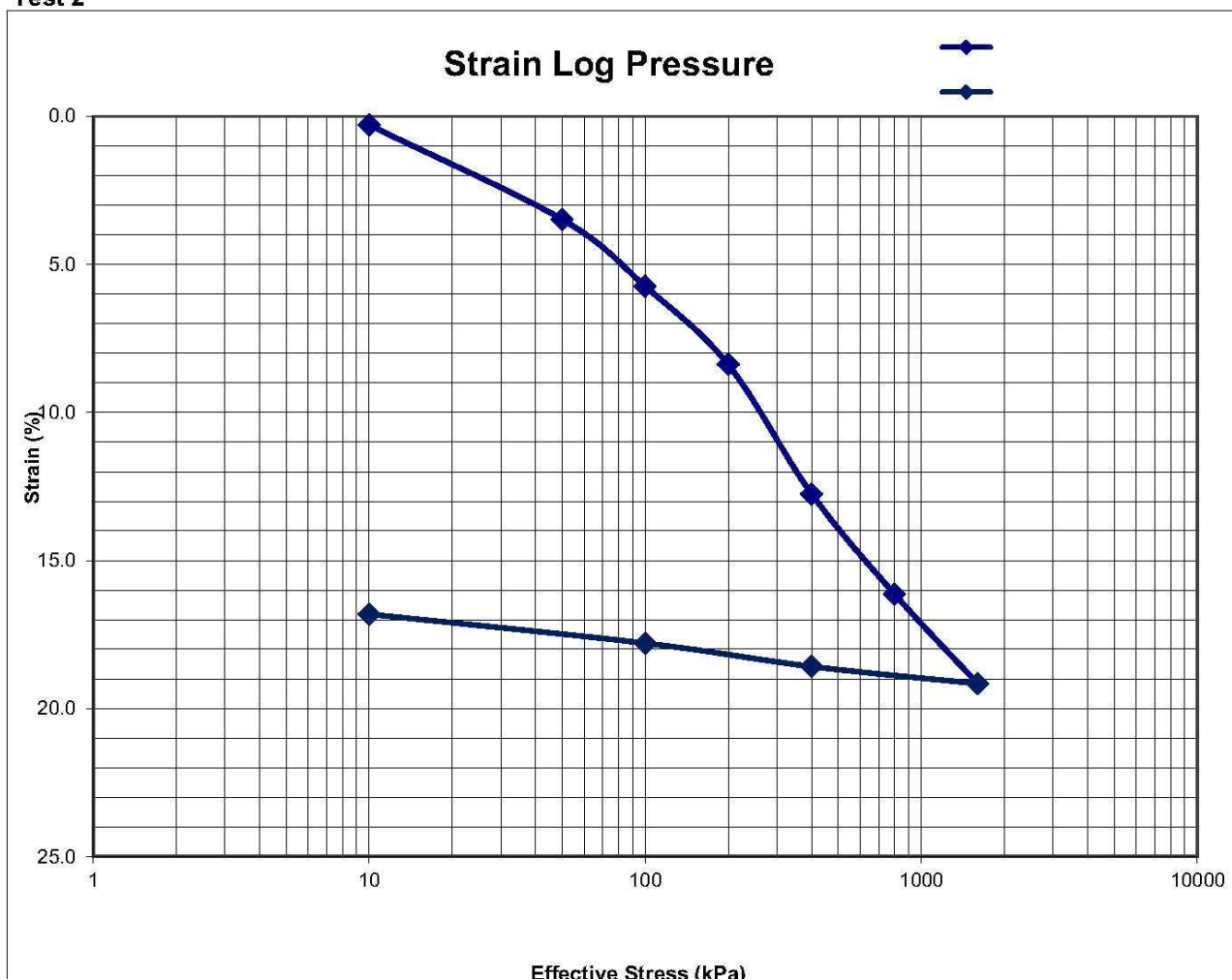
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2004	Sample No.:		2004-11						
Borehole No:	Mix C2+C4A+C7+C8+C10	Depth:		0.4 - 2.5						
Date Received:	23/08/2013	Date Tested:		21/10/2013						

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	0.30	3.49	5.75	8.39	12.76	16.14	19.16	18.58	17.79	16.81	
Mv (1/MPa)		0.7969	0.4524	0.2643	0.2183	0.0846	0.0377	0.0048	0.0262	0.1091	
Void Ratio	0.763	0.7066	0.6666	0.6199	0.5427	0.4829	0.4295	0.4397	0.4536	0.471	

Test 2



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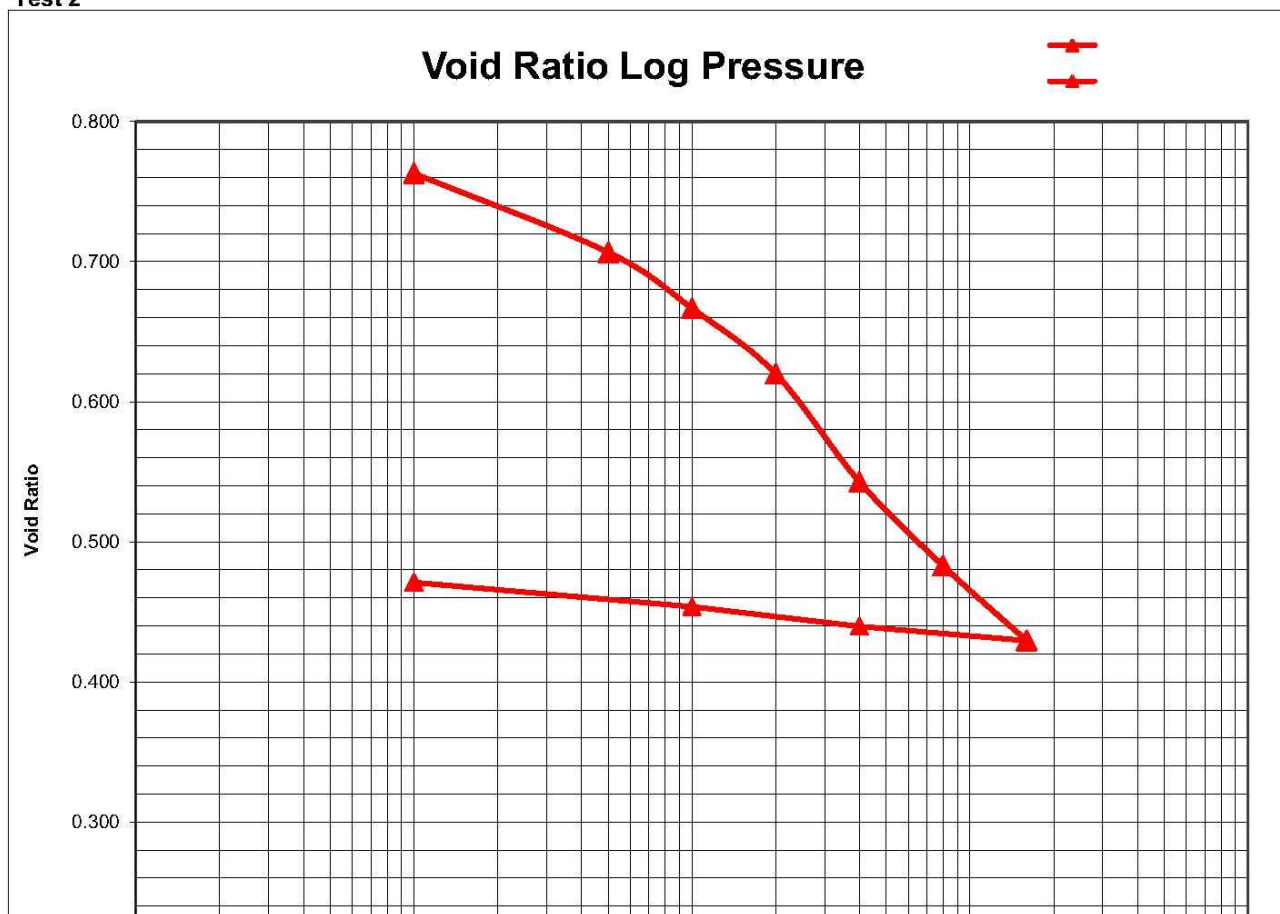
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2004					Sample No.:	2004-11			
Borehole No:	Mix C2+C4A+C7+C8+C10					Depth:	0.4 - 2.5			
Date Received:	23/08/2013					Date Tested:	21/10/2013			

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	0.30	3.49	5.75	8.39	12.76	16.14	19.16	18.58	17.79	16.81	
Mv (1/MPa)		0.7969	0.4524	0.2643	0.2183	0.0846	0.0377	0.0048	0.0262	0.1091	
Void Ratio	0.763	0.7066	0.6666	0.6199	0.5427	0.4829	0.4295	0.4397	0.4536	0.471	

Test 2



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Consolidation Tests

Project:		MZIMVUBU WATER PROJECT						Test 1			
Project No.:		2013-B-2004			Sample No.:		2004-22				
Borehole No:		Mix C12+C18+C22+C28+C30			Depth:		-				
Date Received:		23/08/2013			Date Tested:		21/10/2013				
Remarks:		A remoulded sample tested soaked.									
Machine No.		2	Ring No.		19	Height (mm)		18.5	Diameter (mm)		76.1

Masses for Water Content Determination (g)

Wet Sample and Ring		Dry Sample and Ring	Ring Only	Water Content	
Before Test	After Test			Before Test	After Test
249.9	248.7	219.1	90.64	24.0%	23.0%

Pre-Determined Particle Specific Gravity 2.657

Initial Parameters

Void Ratio	0.7404	Degree of Saturation (%)	86.0	Dry Density (Kg/m ³)	1527
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Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	0
Dial Correction (u)	0	56	78	112	151	208	280	226	177	117	0
HH:MM:SS	√Minutes	Dial Readings in Microns								Initial Dial Reading	
00:00:00	0.00	11984									11984
02:00:00	10.95							8332	8662		
03:00:00	13.42									9162	
18:00:00	32.86	12151									
24:00:00	37.95		11445		10687	9797	8950	8090			
72:00:00	65.73			11171							
End of Primary Cons		12151	11445	11171	10687	9797	8950	8090	8332	8662	9162
Number of Readings:		2	1	1	1	1	1	1	1	1	0

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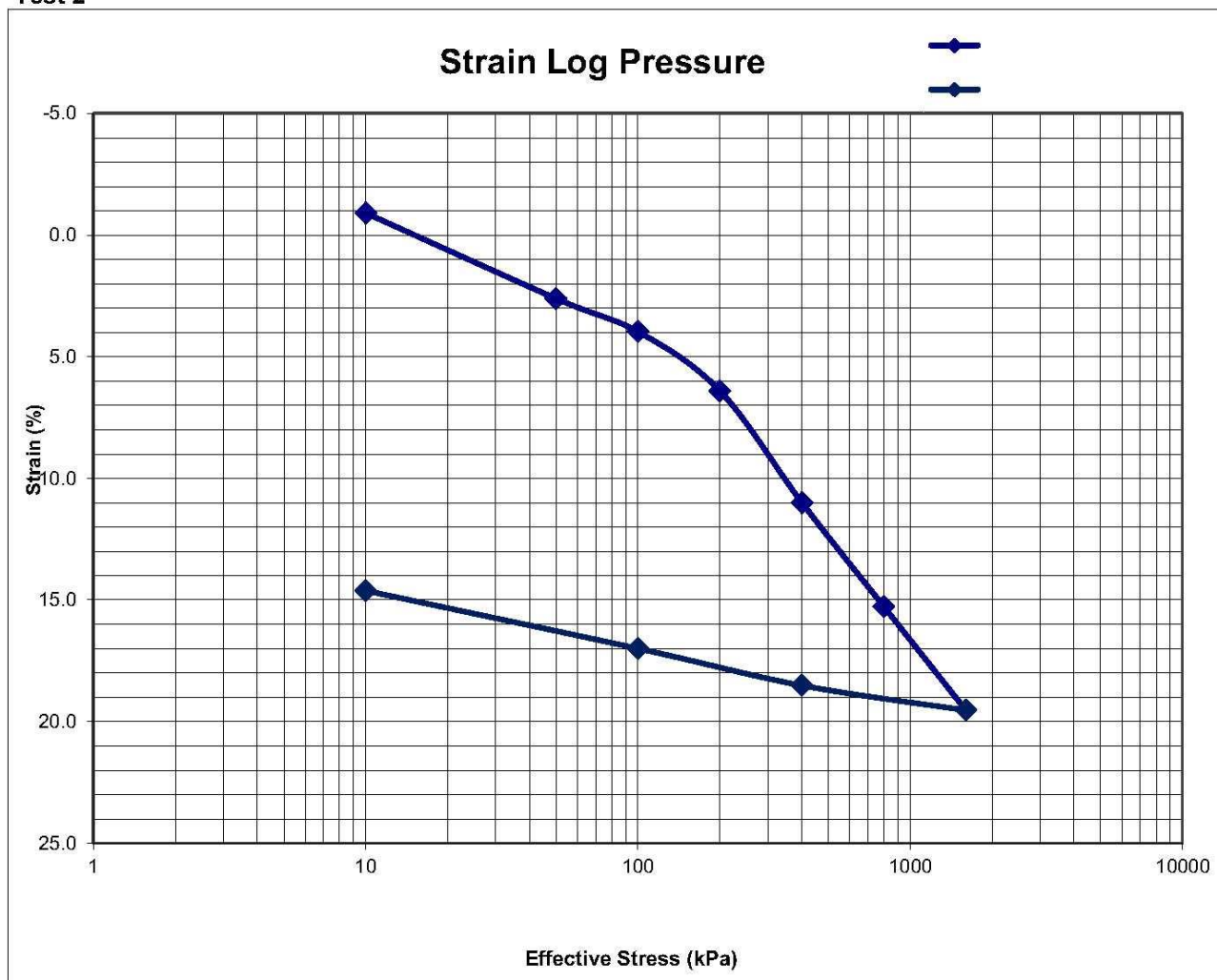
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2004					Sample No.:	2004-22			
Borehole No:	Mix C12+C18+C22+C28+C30					Depth:	-			
Date Received:	23/08/2013					Date Tested:	21/10/2013			

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.90	2.61	3.97	6.41	11.01	15.28	19.54	18.52	17.00	14.62	
Mv (1/MPa)		0.8784	0.2724	0.2432	0.2300	0.1068	0.0532	0.0085	0.0506	0.2643	
Void Ratio	0.7561	0.695	0.6713	0.6289	0.5489	0.4746	0.4004	0.4181	0.4446	0.4859	

Test 2



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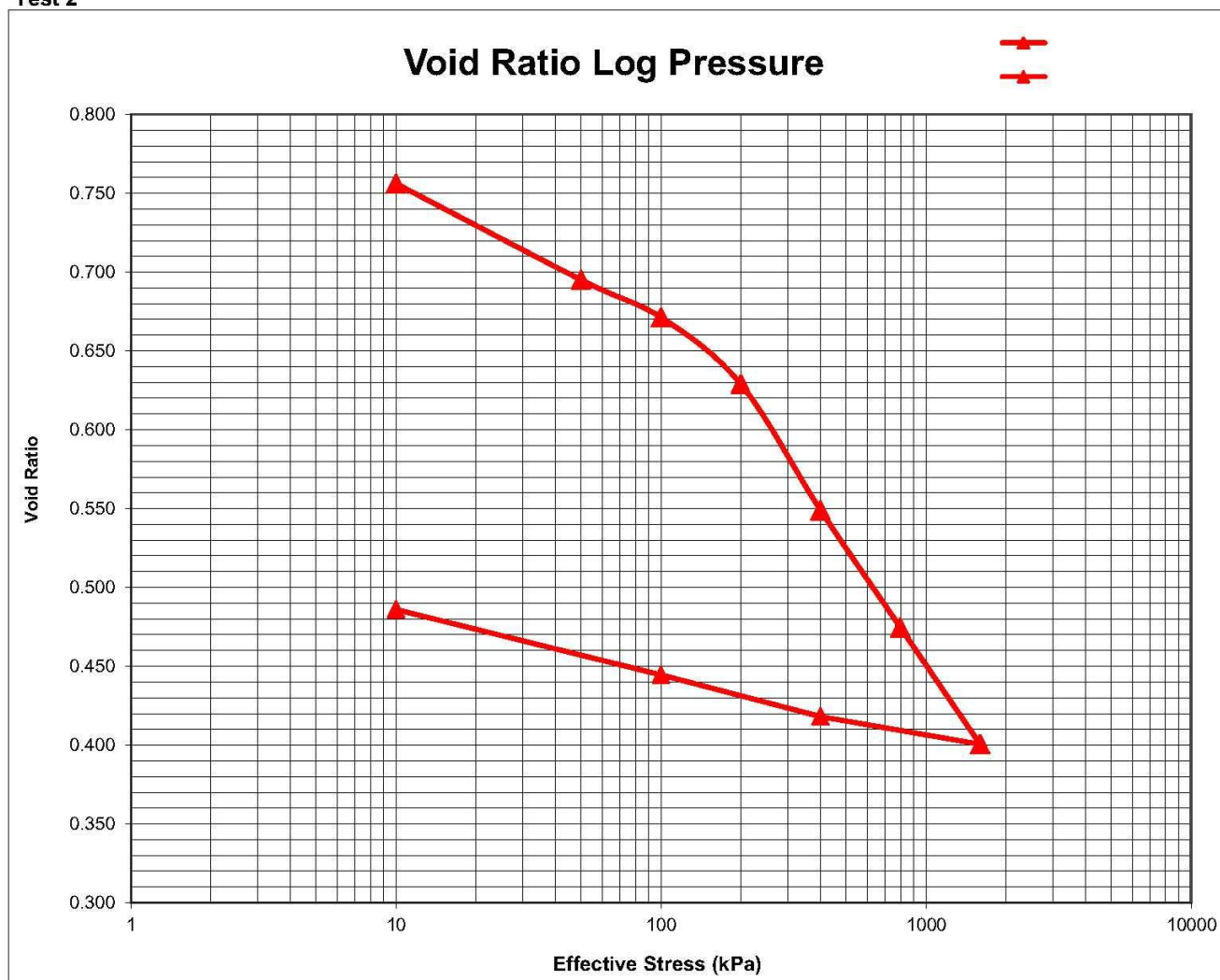
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2004					Sample No.:	2004-22			
Borehole No:	Mix C12+C18+C22+C28+C30					Depth:	-			
Date Received:	23/08/2013					Date Tested:	21/10/2013			

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.90	2.61	3.97	6.41	11.01	15.28	19.54	18.52	17.00	14.62	
Mv (1/MPa)		0.8784	0.2724	0.2432	0.2300	0.1068	0.0532	0.0085	0.0506	0.2643	
Void Ratio	0.75613	0.69498	0.67128	0.62894	0.54888	0.47456	0.40043	0.41811	0.44455	0.48594	

Test 2



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Consolidation Tests

Project:		MZIMVUBU WATER PROJECT				Test 1			
Project No.:		2013-B-2004		Sample No.:		2004-29			
Borehole No:		MIX F5+F8+F10		Depth:		-			
Date Received:		23/08/2013		Date Tested:		11/12/2013			
Remarks:		A remoulded sample tested soaked.							
Machine No.		12	Ring No.		19	Height (mm)	18.5	Diameter (mm)	76.1

Masses for Water Content Determination (g)

Wet Sample and Ring		Dry Sample and Ring	Ring Only	Water Content	
Before Test	After Test			Before Test	After Test
271.7	277.3	254.8	90.64	10.3%	13.7%

Pre-Determined Particle Specific Gravity 2.566

Initial Parameters

Void Ratio	0.3153	Degree of Saturation (%)	83.8	Dry Density (Kg/m ³)	1951
------------	--------	--------------------------	------	----------------------------------	------

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	0	
Dial Correction (u)	0	41	67	107	141	188	257	177	112	39	0	
HH:MM:SS	√Minutes	Dial Readings in Microns								Initial Dial Reading		13839
00:00:00	0.00	13839										
02:00:00	10.95							12238	12500			
03:00:00	13.42									13106		
24:00:00	37.95			13658		13124	12669	12055				
72:00:00	65.73	13877			13416							
96:00:00	75.89		13821									
End of Primary Cons		13877	13821	13658	13416	13124	12669	12055	12238	12500	13106	
Number of Readings:		2	1	1	1	1	1	1	1	1	0	

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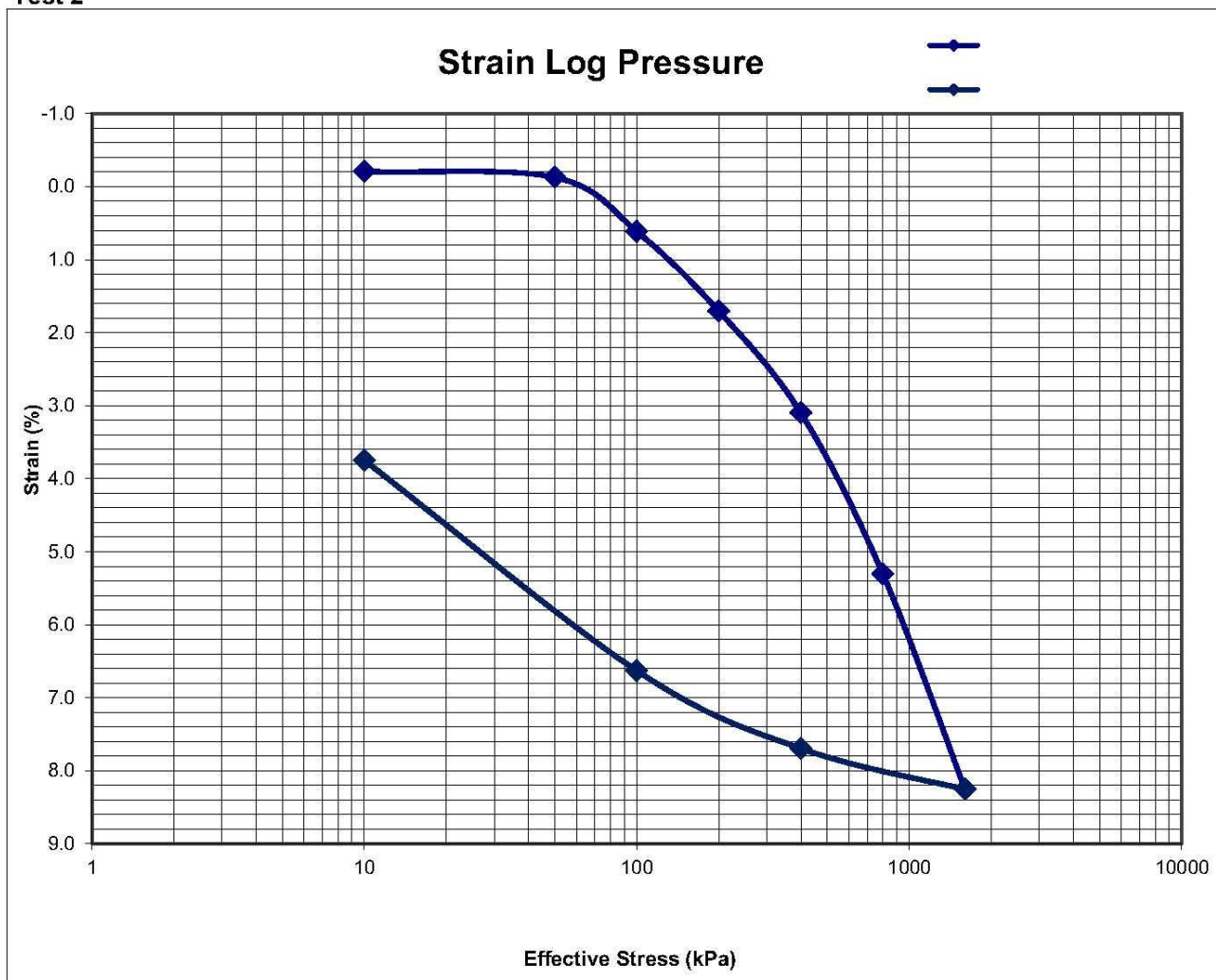
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2004					Sample No.:	2004-29			
Borehole No:	MIX F5+F8+F10					Depth:	-			
Date Received:	23/08/2013					Date Tested:	11/12/2013			

Test 1

Effect.Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.21	-0.12	0.62	1.71	3.10	5.31	8.25	7.70	6.63	3.75	
Mv (1/MPa)		0.0203	0.1481	0.1092	0.0697	0.0551	0.0368	0.0046	0.0355	0.3201	
Void Ratio	0.318	0.3169	0.3072	0.2928	0.2745	0.2455	0.2067	0.214	0.2281	0.2659	

Test 2



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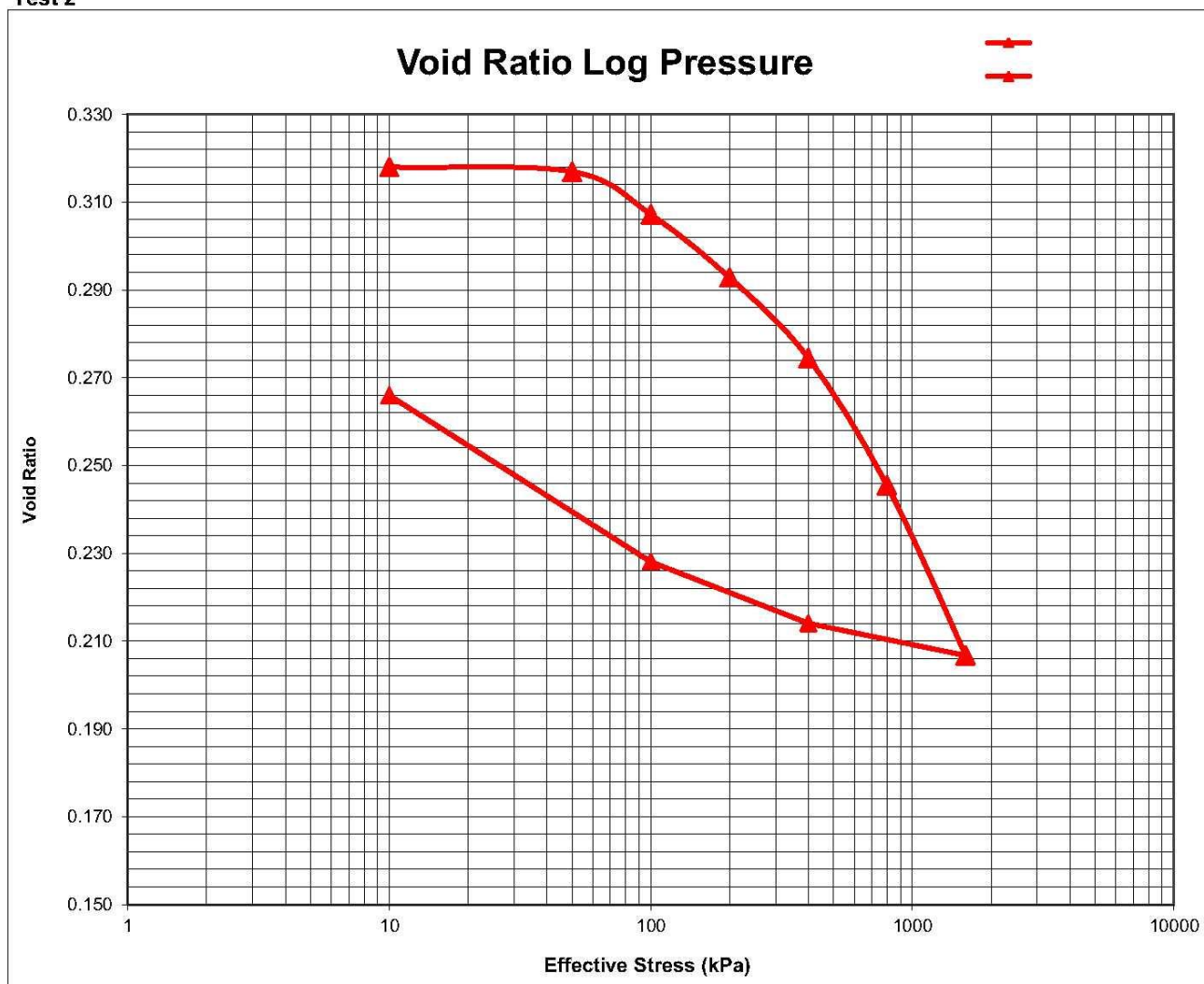
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT		
Project No.:	2013-B-2004	Sample No.:	2004-29
Borehole No:	MIX F5+F8+F10	Depth:	-
Date Received:	23/08/2013	Date Tested:	11/12/2013

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.21	-0.12	0.62	1.71	3.10	5.31	8.25	7.70	6.63	3.75	
Mv (1/MPa)		0.0203	0.1481	0.1092	0.0697	0.0551	0.0368	0.0046	0.0355	0.3201	
Void Ratio	0.318	0.3169	0.3072	0.2928	0.2745	0.2455	0.2067	0.214	0.2281	0.2659	

Test 2



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Consolidation Tests

Project:		MZIMVUBU WATER PROJECT						Test 1
Project No.:		2013-B-2004			Sample No.:		2004-39	
Borehole No:		Mix F25+F29+F34+F37+F39			Depth:		-	
Date Received:		23/08/2013			Date Tested:		21/10/2013	
Remarks:		A remoulded sample tested soaked.						
Machine No.	3	Ring No.	16	Height (mm)	19.95	Diameter (mm)	75.95	

Masses for Water Content Determination (g)

Wet Sample and Ring		Dry Sample and Ring	Ring Only	Water Content	
Before Test	After Test			Before Test	After Test
304.0	305.3	284.5	106.78	11.0%	11.7%

Pre-Determined Particle Specific Gravity 2.717

Initial Parameters

Void Ratio	0.3818	Degree of Saturation (%)	78.1	Dry Density (Kg/m ³)	1966
------------	--------	--------------------------	------	----------------------------------	------

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	0
Dial Correction (u)	0	60	79	113	140	210	327	203	137	46	0
HH:MM:SS	√Minutes	Dial Readings in Microns							Initial Dial Reading		12957
00:00:00	0.00	12957									
02:00:00	10.95							11034	11281		
03:00:00	13.42									11741	
18:00:00	32.86	13040									
24:00:00	37.95		12802		12370	11990	11468	10835			
72:00:00	65.73			12616							
End of Primary Cons		13040	12802	12616	12370	11990	11468	10835	11034	11281	11741
Number of Readings:		2	1	1	1	1	1	1	1	1	0

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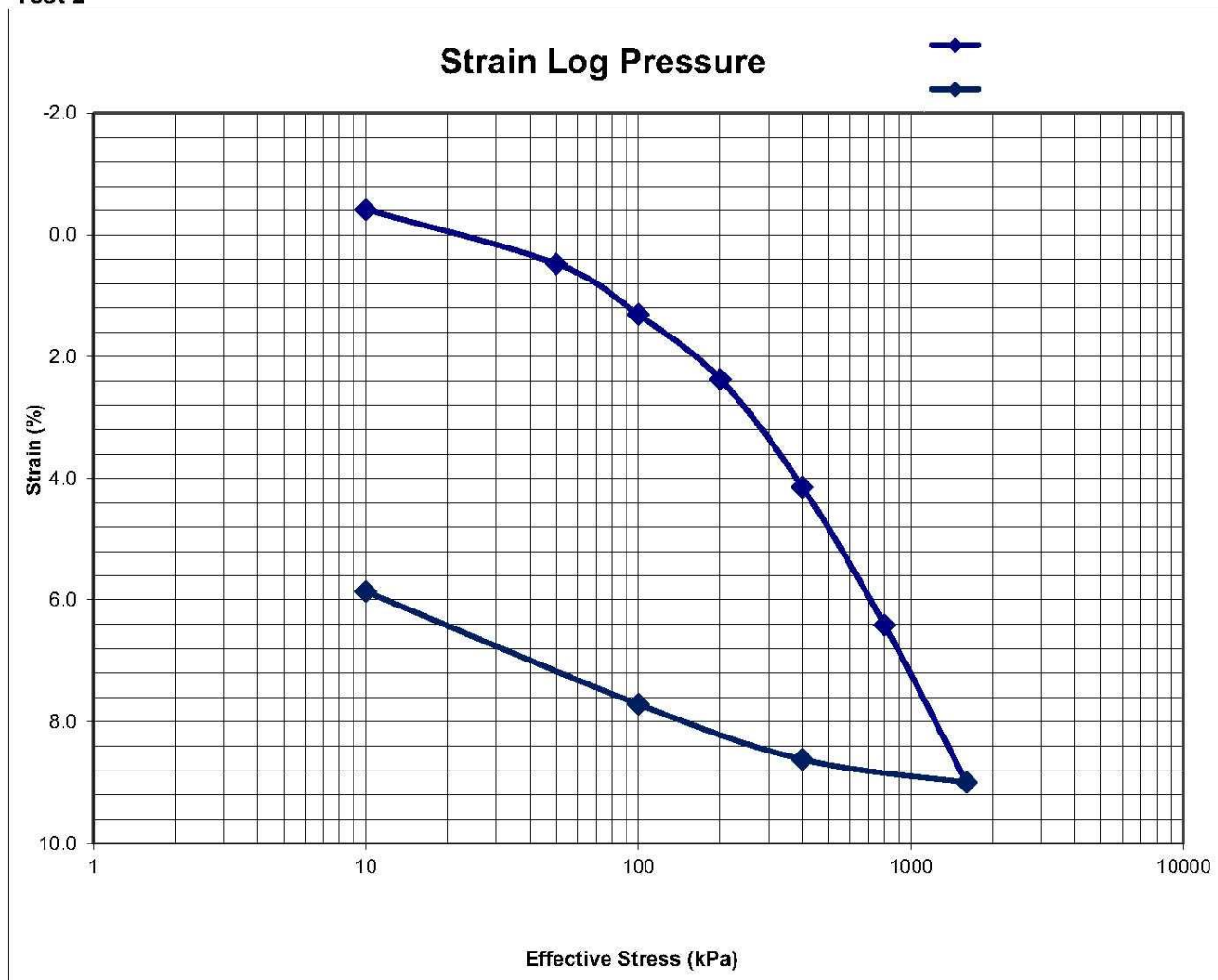
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2004	Sample No.:		2004-39						
Borehole No:	Mix F25+F29+F34+F37+F39	Depth:		-						
Date Received:	23/08/2013	Date Tested:		21/10/2013						

Test 1

Effect.Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.42	0.48	1.31	2.38	4.15	6.41	9.00	8.62	7.71	5.86	
Mv (1/MPa)		0.2231	0.1674	0.1063	0.0885	0.0566	0.0323	0.0031	0.0302	0.2055	
Void Ratio	0.3875	0.3752	0.3636	0.349	0.3245	0.2932	0.2575	0.2627	0.2752	0.3008	

Test 2



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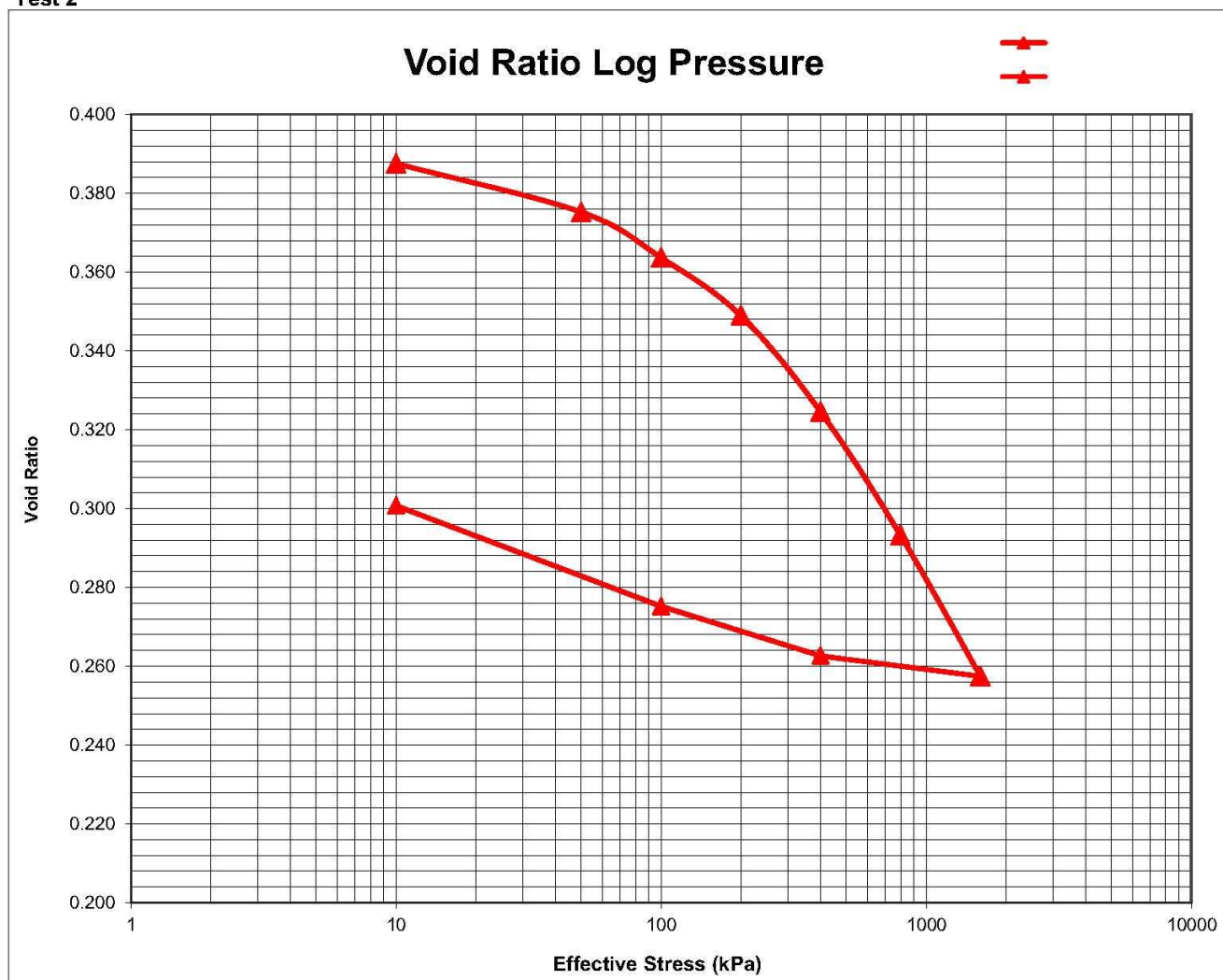
Consolidation Tests

Project:	MZIMVUBU WATER PROJECT									
Project No.:	2013-B-2004					Sample No.:	2004-39			
Borehole No:	Mix F25+F29+F34+F37+F39					Depth:	-			
Date Received:	23/08/2013					Date Tested:	21/10/2013			

Test 1

Effect. Stress (kPa)	10	50	100	200	400	800	1600	400	100	10	
Strain (%)	-0.42	0.48	1.31	2.38	4.15	6.41	9.00	8.62	7.71	5.86	
Mv (1/MPa)		0.2231	0.1674	0.1063	0.0885	0.0566	0.0323	0.0031	0.0302	0.2055	
Void Ratio	0.38754	0.37521	0.36364	0.34896	0.32451	0.2932	0.25746	0.26266	0.27519	0.30075	

Test 2



H 7

PERMIABILITY

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Falling Head Permeability Test Results

Project:	MZIMVUBU WATER PROJECT	
Project No:	2013-B-2246	Date: 28/11/2013

Lab. Sample Reference	Field Sample Reference	Depth (m)	Moisture Contents		Dry density Kg/m ³		Coefficient of Permeability (m/s)		
			Before Test (%)	After Test (%)	Initial	As tested	Range		Average
							Minimum	Maximum	
2246-2	RF 1	1.0 - 1.3	19.3	22.4	1548	1594	1.9E-08	2.7E-08	2.3E-08
2246-3	LF 1 TOP	1.0 - 1.2	36.3	53.4	1016	1056	1.0E-08	2.0E-08	1.4E-08

Remarks: Undisturbed samples.
Saturated and tested under a load of 100kPa.
Densities reported are under a load of 100kPa.

Civilab (Pty) Limited Registration No: 1998/019071/07
BRANCHES: CENTURION • JOHANNESBURG • RUSTENBURG

FallingHead-2013-B-2246

GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES

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Project:	MZINVUBU WATER PROJECT		
Project No:	2013-B-2004	Date:	17/10/2013

[illegible]

Remarks:	Samples remoulded to 98% Proctor. * = Samples remoulded to 95% Proctor. Saturated and tested under a load of 100kPa. Densities reported are under a load of 100kPa.
----------	--

Interim results

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FallingHead-2013-B-2004

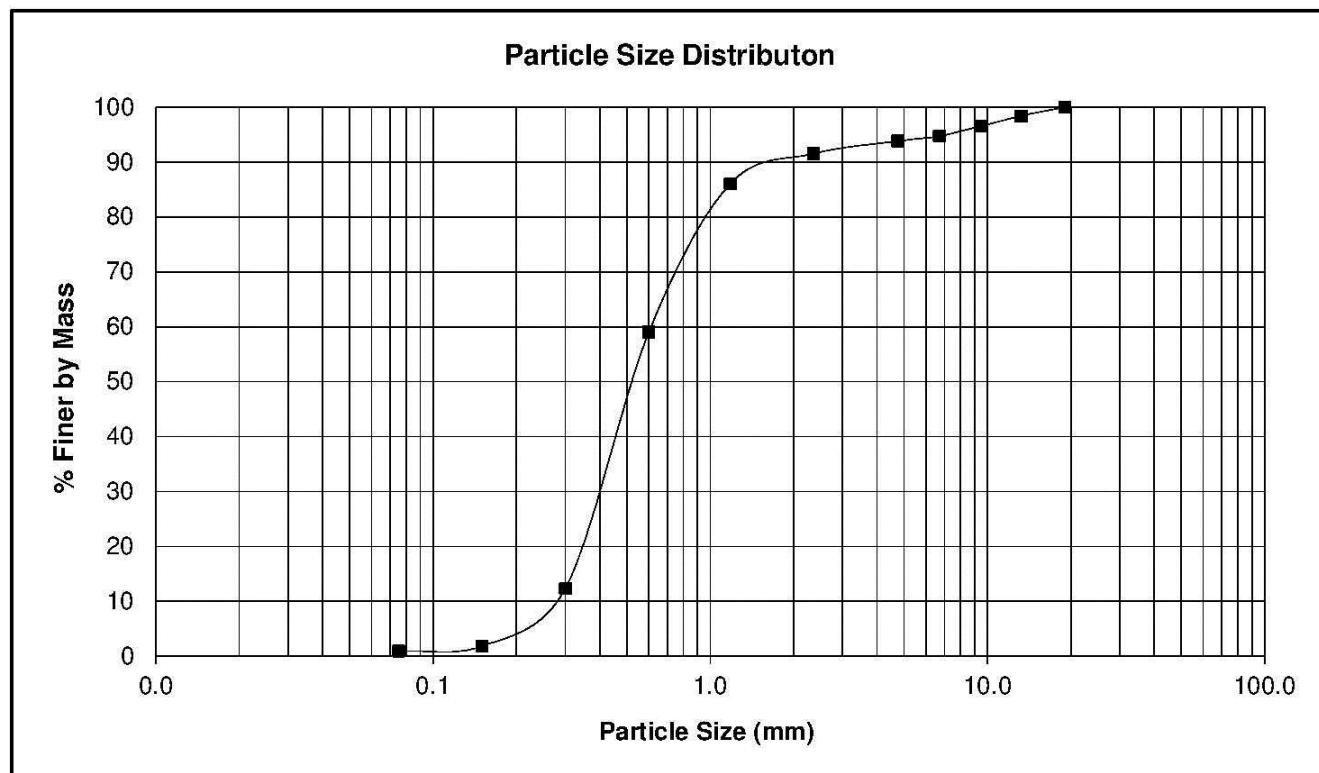
H 8

SAND

Fine Aggregate Test Results

Project	: MZIMVUBU WATER PROJECT	Date	: 1 OCTOBER 2013
Project No	: 2013-B-2004	Lab Sample Reference	: 2004-40
Field Reference	: S1	Remarks	: -
Organic Impurities	: N/T		

Particle Size Distribution				Physical Properties		
Reference		Test Sample	Specification	Parameters	Test Sample	Specification
Finer by Mass (%)	Particle Size (mm)	19 . 0	100	Fineness Modulus	%	2.55
		13 . 2	98	Dust Content		0.9
		9 . 5	97	Sand Equivalent	%	N/T
		6 . 7	95	Moisture Content	%	N/T
		4 . 75	94	Water Absorption	%	N/T
		2 . 36	92	Apparent Relative Density		N/T
		1 . 18	86	Bulk Relative Density		N/T
		0 . 60	59	N/T denotes Not Tested		
		0 . 30	12	N/A denotes Not Applicable		
		0 . 15	2			
		0 . 075	1			



The samples were subjected to analysis according to SABS method 1083:1994.

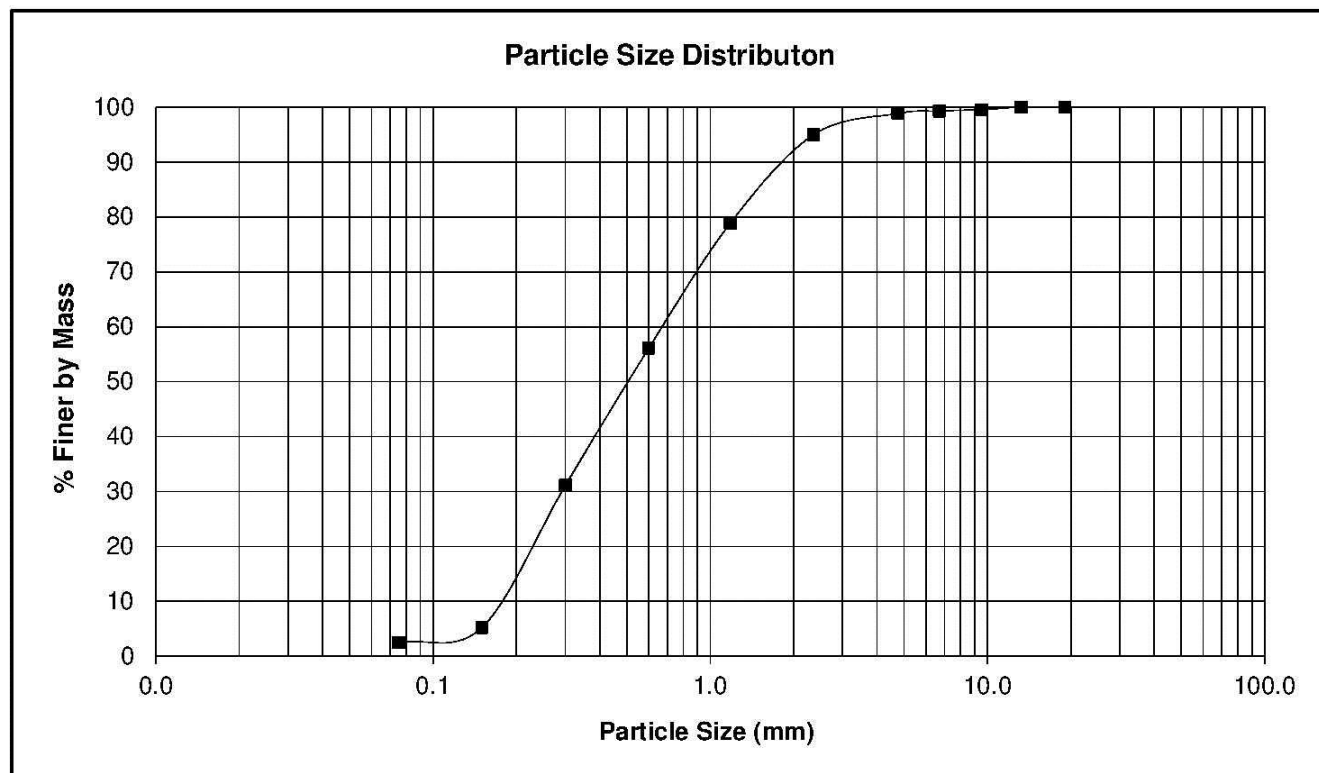
The results reported relate only to the samples tested.

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Fine Aggregate Test Results

Project	: MZIMVUBU WATER PROJECT	Date	: 1 OCTOBER 2013
Project No	: 2013-B-2004	Lab Sample Reference	: 2004-41
Field Reference	: S2	Remarks	: -
Organic Impurities	: Lighter than Reference		

Particle Size Distribution				Physical Properties		
Reference		Test Sample	Specification	Parameters	Test Sample	Specification
Finer by Mass (%)	Particle Size (mm)	19 . 0	100	Fineness Modulus	%	2.35
		13 . 2	100	Dust Content		2.5
		9 . 5	100	Sand Equivalent	%	N/T
		6 . 7	99	Moisture Content	%	N/T
		4 . 75	99	Water Absorption	%	N/T
		2 . 36	95	Apparent Relative Density		N/T
		1 . 18	79	Bulk Relative Density		N/T
		0 . 60	56	N/T denotes Not Tested		
		0 . 30	31	N/A denotes Not Applicable		
		0 . 15	5			
		0 . 075	3			



The samples were subjected to analysis according to SABS method 1083:1994.

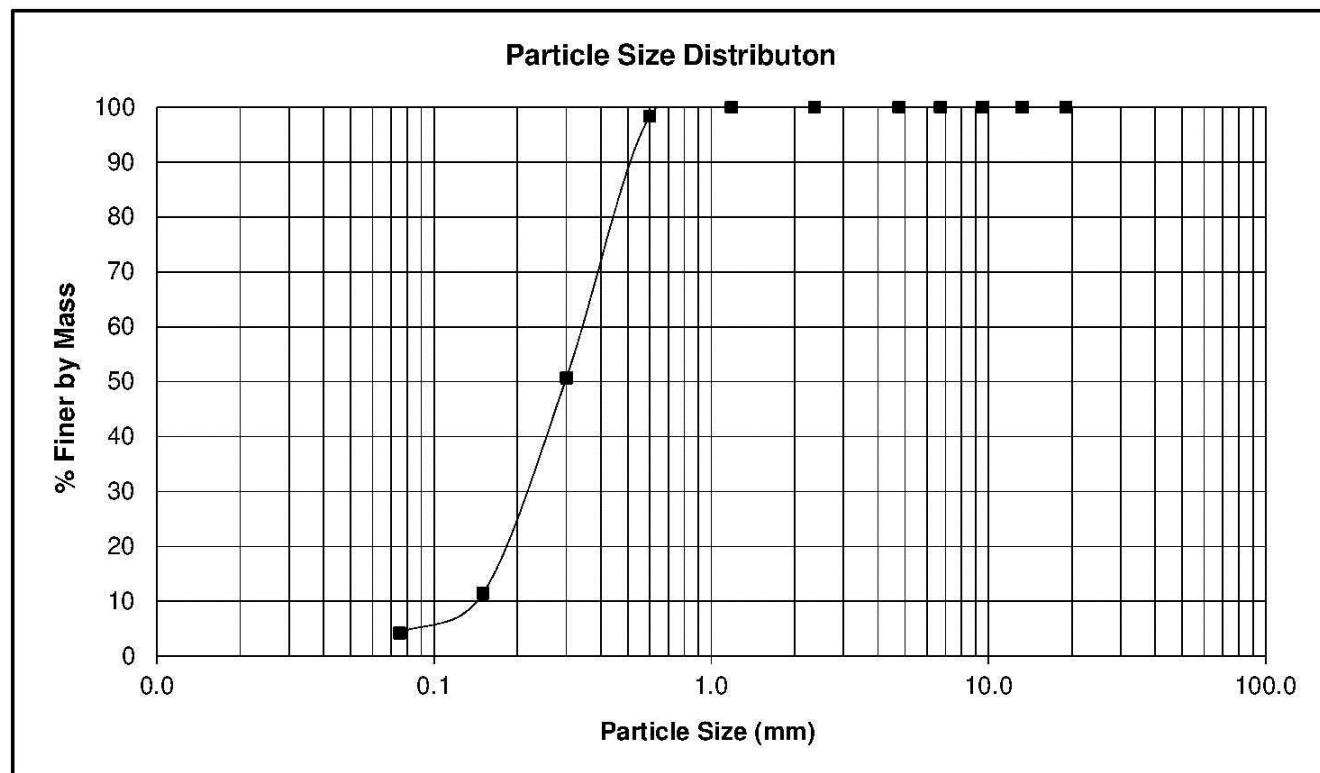
The results reported relate only to the samples tested.

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Fine Aggregate Test Results

Project	: MZIMVUBU WATER PROJECT	Date	: 1 OCTOBER 2013
Project No	: 2013-B-2004	Lab Sample Reference	: 2004-42
Field Reference	: S3	Remarks	: -
Organic Impurities	: N/T		

Particle Size Distribution				Physical Properties		
Reference		Test Sample	Specification	Parameters	Test Sample	Specification
Finer by Mass (%)	Particle Size (mm)	19 . 0	100	Fineness Modulus	%	1.39
		13 . 2	100	Dust Content		4.2
		9 . 5	100	Sand Equivalent	%	N/T
		6 . 7	100	Moisture Content	%	N/T
		4 . 75	100	Water Absorption	%	N/T
		2 . 36	100	Apparent Relative Density		N/T
		1 . 18	100	Bulk Relative Density		N/T
		0 . 60	98	N/T denotes Not Tested		
		0 . 30	51	N/A denotes Not Applicable		
		0 . 15	11			
		0 . 075	4			



The samples were subjected to analysis according to SABS method 1083:1994.

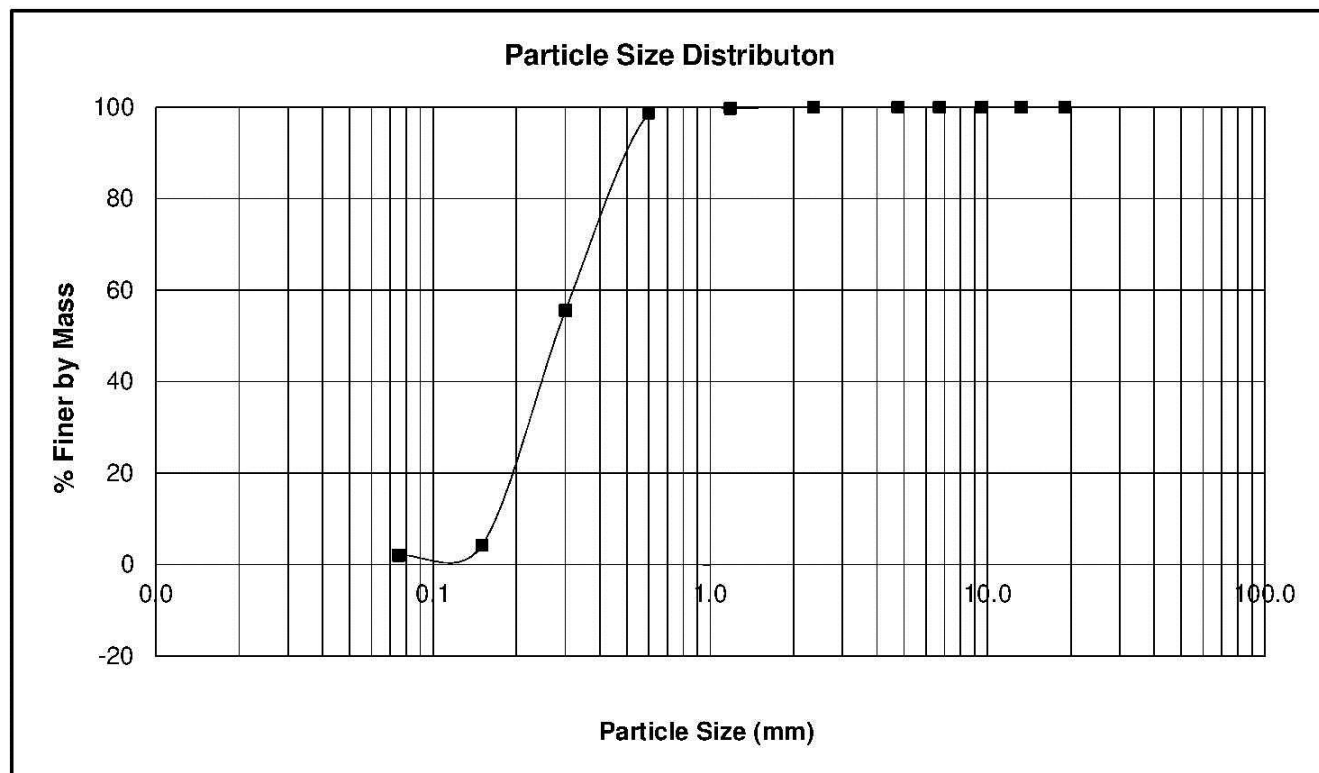
The results reported relate only to the samples tested.

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Fine Aggregate Test Results

Project	: MZIMVUBU WATER PROJECT	Date	: 1 OCTOBER 2013
Project No	: 2013-B-2004	Lab Sample Reference	: 2004-43
Field Reference	: S4	Remarks	: -
Organic Impurities	: Same as Reference		

Particle Size Distribution				Physical Properties		
Reference		Test Sample	Specification	Parameters	Test Sample	Specification
Finer by Mass (%)	Particle Size (mm)	19 . 0	100	Fineness Modulus	%	1.42
		13 . 2	100	Dust Content		2.0
		9 . 5	100	Sand Equivalent	%	N/T
		6 . 7	100	Moisture Content	%	N/T
		4 . 75	100	Water Absorption	%	N/T
		2 . 36	100	Apparent Relative Density		N/T
		1 . 18	100	Bulk Relative Density		N/T
		0 . 60	99	N/T denotes Not Tested		
		0 . 30	56	N/A denotes Not Applicable		
		0 . 15	4			
		0 . 075	2			



The samples were subjected to analysis according to SABS method 1083:1994.

The results reported relate only to the samples tested.

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Prediction of 28-day compressive strength of concrete on the third day using artificial neural networks

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Abstract

In recent decades, artificial neural networks are known as intelligent methods for modeling of behavior of physical phenomena. In this paper, implementation of an artificial neural network has been developed for prediction of compressive strength of concrete. A MISO (Multi Input Single Output) adaptive system has been introduced which can model the proposed phenomenon. The data has been collected by experimenting on concrete samples and then the neural network has been trained using these data. From among 432 specimens, 300 data sample has been used for train, 66 data sample for validation and 66 data sample for the final test of the network. The 3-day strength parameter of concrete in the introduced structure also has been used as an important index for predicting the 28-day strength of the concrete. The simulations in this paper are based on real data obtained from concrete samples which indicate the validity of the proposed tool.

Keywords: Concrete, Strength, Prediction, Artificial, Neural Networks.

1. INTRODUCTION

Different sciences are developing fast in today's world. In recent decades, man has seen increased relationship of sciences in different fields and the more relationship has led to the appearance of the more new knowledge and technology. Nowadays, one of the most important problems of man are technical and engineering problems. The complexity of the most of the problems in this field has made the experts of this field use the new mathematical and modeling methods for solving this type of problems. Intelligent systems can be used as suitable tools for identifying complex systems, due to their ability of learning and adaptation.

One of the complex problems in our world is the problem of the concrete. The main criterion for evaluating the compressive strength of concrete is the strength of the concrete on 28th day. The concrete sample is tested after 28 days and the result of this test is considered as a criterion for quality and rigidity of that concrete.

Concrete is the most widely used structural material in constructions in the world. Massive concreting in huge civil projects like dams, power plants, bridges and etc... usually is not practicable and it is necessary to be performed in several layers and the compressive strength of each layer should not be less than the specified compressive strength. Therefore one should wait 28 days to achieve 28-day strength of each layer of concrete. Thereupon if we have n layers of concrete we need $28 \times n$ days to complete the total project. [1]

2. CONCRETE

Concrete is the only major building material that can be delivered to the job site in a plastic state. This unique quality makes concrete desirable as a building material because it can be molded to virtually any form or shape. Concrete provides a wide latitude in surface textures and colors and can be used to construct a wide variety of structures, such as highways and streets, bridges, dams, large buildings, airport runways, irrigation structures, breakwaters, piers and docks, sidewalks, silos and farm buildings, homes, and even barges and ships.

The two major components of concrete are a cement paste and inert materials. The cement paste consists of Portland cement, water, and some air either in the form of naturally entrapped air voids or minute, intentionally entrained air bubbles. The inert materials are usually composed of fine aggregate, which is a material such as sand, and coarse aggregate, which is a material such as gravel, crushed stone, or slag.

When Portland cement is mixed with water, the compounds of the cement react to form a cementing medium. In properly mixed concrete, each particle of sand and coarse aggregate is completely surrounded and coated by this paste, and all spaces between the particles are filled with it. As the cement paste sets and hardens, it binds the aggregates into a solid mass.

Under normal conditions, concrete grows stronger as it grows older. The chemical reactions between cement and water that cause the paste to harden and bind the aggregates together require time. The reactions take place very rapidly at first and then more slowly over a long period of time. [2]

3. CEMENT

Cement is a material that has adhesive and cohesive properties enabling it to bond mineral fragments into a solid mass. Cement consists of silicates and aluminates of lime made from limestone and clay (or shale) which is ground, blended, fused in a kiln and crushed to a powder. Cement chemically combines with water (hydration) to form a hardened mass. The usual hydraulic cement is known as Portland cement because of its resemblance when hardened to Portland stone found near Dorset, England. The name was originated in a patent obtained by Joseph Aspdin of Leeds, England in 1824.

Typical Portland cements are mixtures of tricalcium silicate ($3\text{CaO} \cdot \text{SiO}_2$), tricalcium aluminate ($3\text{CaO} \cdot \text{Al}_2\text{O}_3$), and dicalcium silicate ($2\text{CaO} \cdot \text{SiO}_2$), in varying proportions, together with small amounts of magnesium and iron compounds. Gypsum is often added to slow the hardening process. [2,3]

4. WATER

The water has two roles in concrete mixture: First is the chemical composition with cement and perform cement hydration and second is to make the concrete composition fluent and workable. The water which is used to make the concrete is drink water. The impurity of water can have undesirable effect on concrete strength. [4]

5. AGGREGATES

Since aggregate usually occupies about 75% of the total volume of concrete, its properties have a definite influence on behavior of hardened concrete. Not only does the strength of the aggregate affect the strength of the concrete, its properties also greatly affect durability (resistance to deterioration under freeze-thaw cycles). Since aggregate is less expensive than cement it is

logical to try to use the largest percentage feasible. Hence aggregates are usually graded by size and a proper mix has specified percentages of both fine and coarse aggregates. Fine aggregate (sand) is any material passing through a No. 4 sieve. Coarse aggregate (gravel) is any material of larger size.

Fine aggregate provides the fineness and cohesion of concrete. It is important that fine aggregate should not contain clay or any chemical pollution. Also, fine aggregate has the role of space filling between coarse aggregates. Coarse aggregate includes: fine gravel, gravel and coarse gravel. In fact coarse aggregate comprises the strongest part of the concrete. It also has reverse effect on the concrete fineness. The more coarse aggregate, the higher is the density and the lower is the fineness. [3,5]

6. COMPRESSIVE STRENGTH OF CONCRETE

The strength of concrete is controlled by the proportioning of cement, coarse and fine aggregates, water, and various admixtures. The ratio of the water to cement is the chief factor for determining concrete strength as shown in figure1. The lower the water-cement ratio, the higher is the compressive strength. A certain minimum amount of water is necessary for the proper chemical action in the hardening of concrete; extra water increases the workability (how easily the concrete will flow) but reduces strength. A measure of the workability is obtained by a slump test.

Actual strength of concrete in place in the structure is also greatly affected by quality control procedures for placement and inspection. The strength of concrete is denoted in the United States by f'_c which is the compressive strength of test cylinder 6 in. in diameter by 12 in. high measured on the 28th day after they are made. [3]

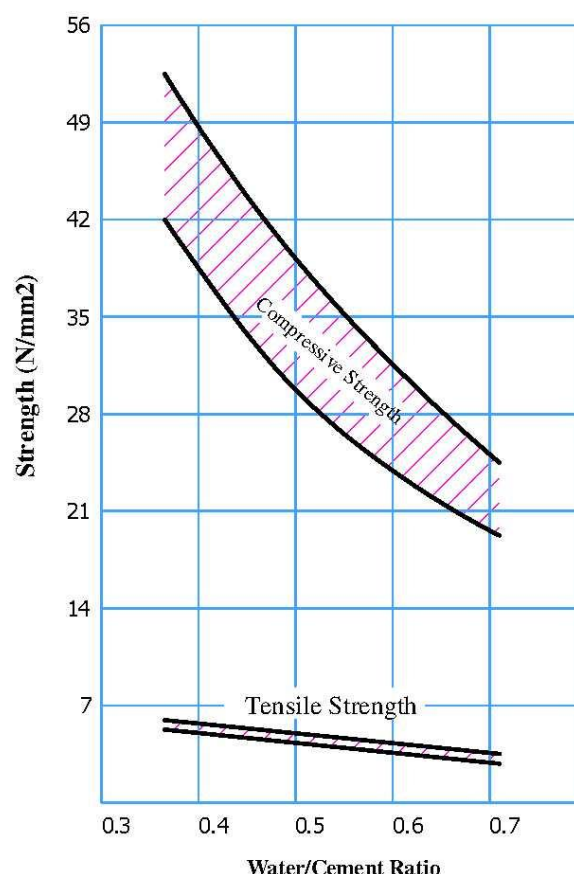


FIGURE 1: illustration of the effect of water/cement ratio in concrete strength [1]

7. CONCRETE SAMPLING

Acceptance of the concrete in the site is performed based on the results of the compressive tests of concrete samples. The concrete samples must be taken from the final consumption place. The purpose of the concrete sampling is to prepare two specimens of concrete which their compressive tests will be performed after 28 days or in any predetermined day. To predict the 28-day compressive strength of concrete we can also have another sample to be tested earlier than 28 days. [1]

8. CONCRETE MIX DESIGN

The concrete mix design is a process of selecting the suitable ingredients of concrete and determining their most optimum proportion which would produce, as economically as possible, concrete that satisfies a certain compressive strength and desired workability. [6]

The concrete mix design is based on the principles of

- Workability
- Desired strength and durability of hardened concrete
- Conditions in site, which helps in deciding workability, strength and durability requirements

9. ADAPTIVE SYSTEMS

Adaptability, in essence, is the ability to react in sympathy with disturbances to the environment. A system that exhibits adaptability is said to be adaptive. Biological systems are adaptive systems; animals, for example, can adapt to changes in their environment through a learning process [7]. A generic adaptive system employed in engineering is shown in Figure 2. It consists of

- set of adjustable parameters (weights) within some filter structure;
- An error calculation block (the difference between the desired response and the output of the filter structure);
- A control (learning) algorithm for the adaptation of the weights.

The type of learning represented in Figure 2 is so-called supervised learning, since the learning is directed by the desired response of the system. Here, the goal is to adjust iteratively the free parameters (weights) of the adaptive system so as to minimize a prescribed cost function in some predetermined sense. [8]

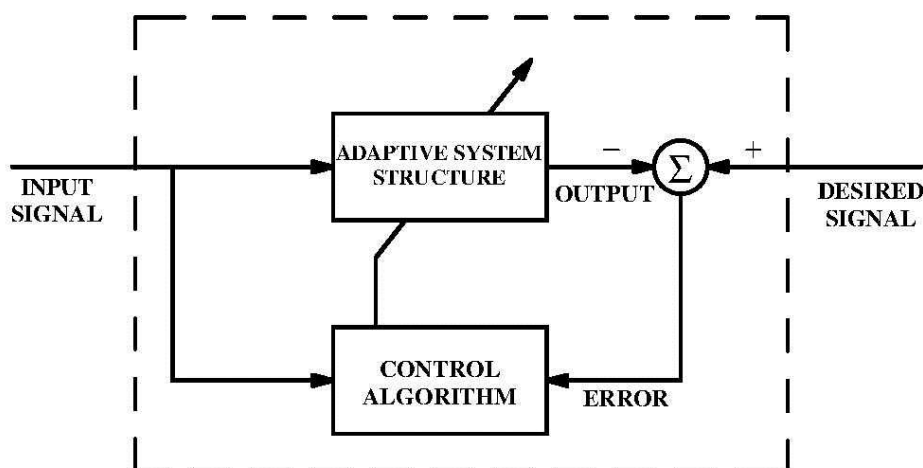


FIGURE 2: Block diagram of an adaptive system

10. ARTIFICIAL NEURAL NETWORKS

Artificial Neural Network (ANN) models have been extensively studied with the aim of achieving human-like performance, especially in the field of pattern recognition and system identification. These networks are composed of a number of nonlinear computational elements which operate in parallel and are arranged in a manner reminiscent of biological neural inter-connections.

The property that is of primary significance for a neural network is the ability of the network to learn from its environment, and to improve its performance through learning. The improvement in performance takes place over time in accordance with some prescribed measure. A neural network learns about its environment through an interactive process of adjustments applied its synaptic weights and bias levels. Ideally, the network becomes more knowledgeable about its environment after each iteration of the learning process. [7]

11. CONCRETE STRENGTH PREDICTION

To predict 28-day strength of concrete, It should identify the effective parameters of the concrete strength. The more accurately identified the parameters, the better is the result.

The studies in this paper were performed in two phases:

1. Phase one, includes the studies about the concrete and effective factors of the concrete compressive strength and also performing the experiments in the real environment and collecting data.
2. Phase two, include studies about how to use artificial neural networks to identify the presented system and to achieve accurate prediction of concrete 28-day compressive strength. [1]

12. PERFORMING EXPERIMENTS

In this study the ACI method is used to perform experiments. Experiments were performed in Aghchay dam in west Azerbaijan in IRAN. The cement used in the experiments was provided from Sofiyan cement plant and the aggregates were provided from the natural materials of the Aghchay dam site. [1]

13. COLLECTING DATA

There are lots of Parameters affect on compressive strength of concrete. But the most important parameters were collected in table 1. It is important that the range of each parameter is limited due to regarding ACI standard.

TABLE 1: Effective parameters of the compressive strength of the concrete

Row	Parameter	Unit	Range
1	Mix Design	-	A-L
2	Water/Cement Ratio	%	35.0 - 75.0
3	Density	ton/m3	2.30 - 2.60
4	Slump	mm	70 - 150
5	Air	%	1.0 - 7.0
6	Silica fumes	gr	0 - 400
7	Super-Plasticizer	kg	0.0 - 3.5
8	Age	day	3, 7, 14, 28, 42
9	Compressive Strength	kg/cm2	70.00 - 420.00

The concrete mix design is affected by these factors:
 Cement, Fine aggregate, Fine gravel, gravel, coarse gravel, air

The 1st to 7th parameters are determined in the first day. There is a salient point about 8th parameter (age). As previously mentioned, the concrete age has a direct arithmetic relation with the concrete strength. The more aged the concrete the higher is the compressive strength. [1] Here is an interesting point so that the 3-day compressive strength of concrete has a mathematical relation with the compressive strength of the same concrete in 7th, 14th, 28th and 42th day. Therefore it can be used as an important parameter for prediction of this system. In other words, the 3-day compressive strength of concrete is a very good criterion to achieve the 28-day compressive strength.

It is conceived from figure.3 that the higher the 3-day compressive strength the higher is the 28-day compressive strength of the concrete. Figure.4 shows the relationship between 3-day compressive strength and 28-day compressive strength for 4 types of concrete with variable w/c ratios, this relation is linear relatively.

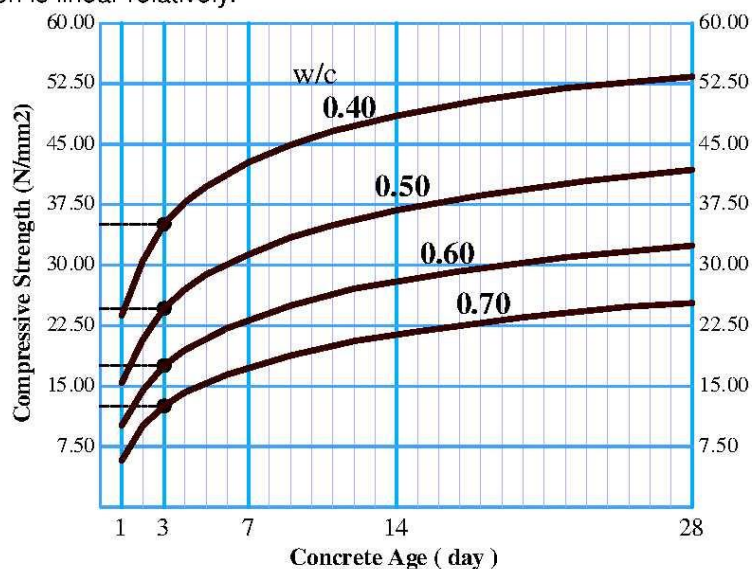


FIGURE 3: illustration of relationship between age and compressive strength of concrete [1]

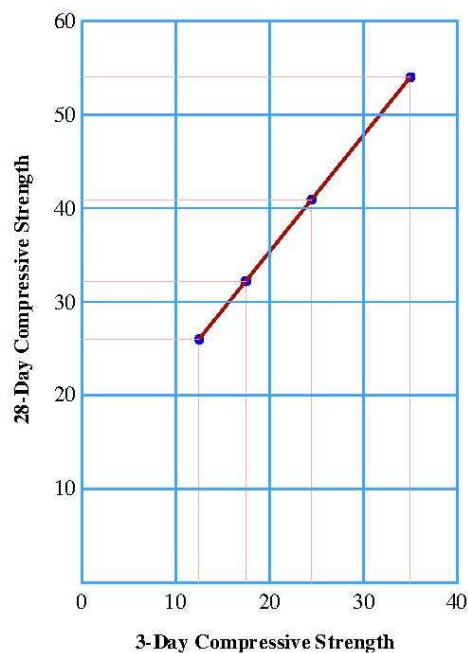


FIGURE 4: illustration of relationship between 3-day and 28-day strength of concrete [1]

14. METHODOLOGY OF CONCRETE STRENGTH NEURAL IDENTIFICATION

A methodology for concrete strength neural identification was developed. It is shown schematically in Figure 5. Three blocks can be distinguished in the scheme. Experimental results, forming a set of data on concrete, used for training and testing the neural network are an integral part of block1.

The experimental results as a set of patterns were saved in a computer file which was then used as the input data for the network in block 2. The data were divided into data for training and testing the neural network. The training patterns were randomly input into the network as following:

1. 70% of total data for training of the neural network
2. 15% of total data for validation of the neural network
3. 15% of total data for testing of the neural network,

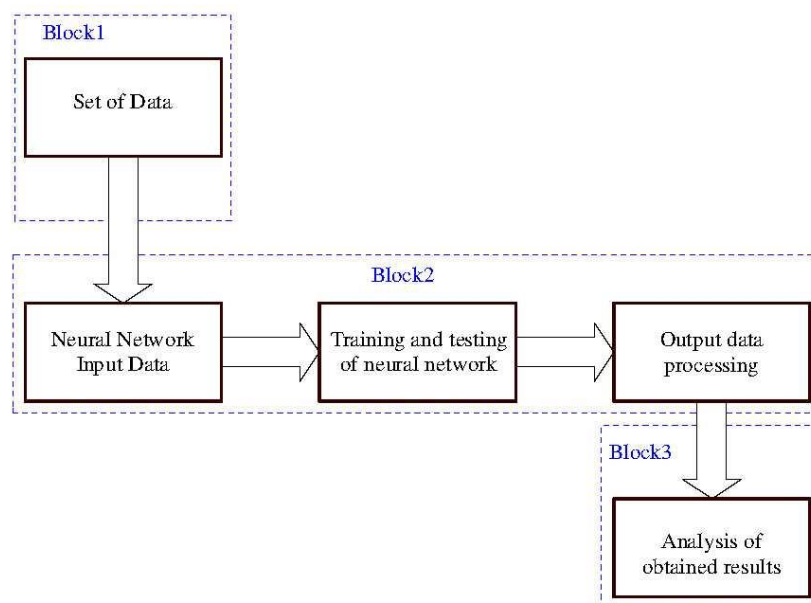


FIGURE 5: Block diagram of concrete compressive strength identification by means of neural networks [9]

If the neural network correctly mapped the training data and correctly identified the testing data, it was considered trained. The obtained results were analyzed in block 3 whose output was identified concrete compressive strength f_c [9]

15. FEED-FORWARD NEURAL NETWORK

The Feed-forward neural network structure for prediction of concrete compressive strength is shown in Figure 6. Feed-forward networks often have one or more hidden layers of sigmoid neurons followed by an output layer of linear neurons. Multiple layers of neurons with nonlinear transfer function allow the network to learn nonlinear and linear relationships between inputs and outputs. [10]

The process of learning with teacher in this network is executed through a back-propagation algorithm so that the network output converges to the desired output. The key distinguishing characteristic of this feed-forward neural network with the back-propagation learning algorithm is that it forms a nonlinear mapping from a set of input stimuli to a set of output using features extracted from the input patterns. The network can be designed and trained to accomplish a wide variety of nonlinear mappings, some of which are very complex. This is because the neural units in the neural network learn to respond to features found in the input. [11]

The number of input and output units is determined by dimensions of the data set whereas the number of hidden layer (M) is a free parameter which is adjusted to achieve the maximum performance. Note that, M determines the degree of freedom of the system. Therefore we expect that there was an optimum value for M. The criterion to achieve the optimum M is defined as: "The smallest M which causes minimum mse while the maximum error is small"

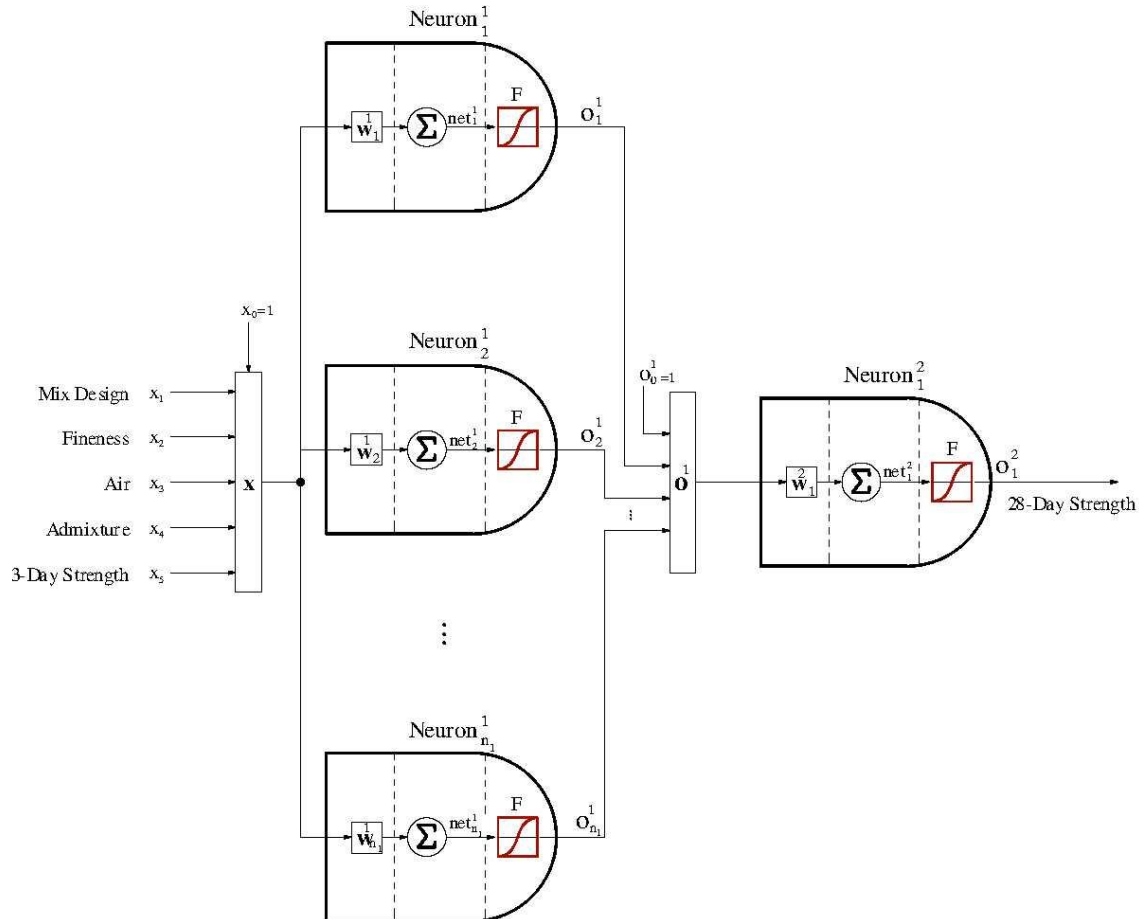


FIGURE 6: Diagram of the feed-forward neural network used for concrete compressive strength prediction

Figure.7 shows the mean squared error of the network output for validation and test data with 10 iterations for each number of hidden neurons. Figure.8 shows the maximum error between desired outputs and the network outputs with 10 iterations for each number of hidden neurons.

The optimum value in this structure is to choose $M=11$ for the number of hidden neurons.

In order to backpropagate the error and update the network weights, Gradient-Descent, Quasi-Newton, Conjugate-Gradient and Levenberg-Marquardt Algorithms were used.

- Gradient Descent $W(k+1) = W(k) - \alpha_k g_k$
- Quasi Newton $W(k+1) = W(k) - H_K^{-1} g_K$
- Conjugate Gradient $W(k+1) = W(k) - g_{k+1} + \alpha_k \Delta W_k$

Where W is the weight matrix, α is the learning rate, g is the gradient of error and H is the hessian matrix of the cost function. [12]

The levenberg-marquardt algorithm is like quasi-newton but it doesn't need to calculate hessian matrix where it can be estimated as follows:

$$H = J^T J, \quad \nabla E = J^T e$$

$$W(k+1) = W(k) - [H + \mu I]^{-1} \nabla E$$

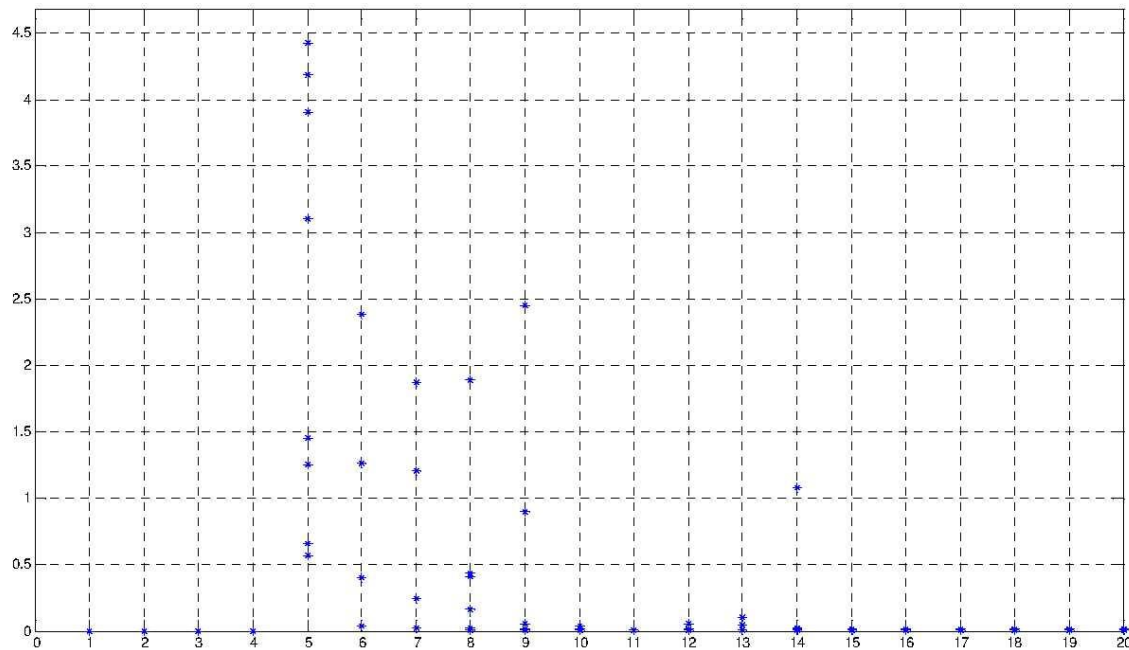


FIGURE 7: Diagram of mean squared error of the network output with 10 iterations for certain number of neurons

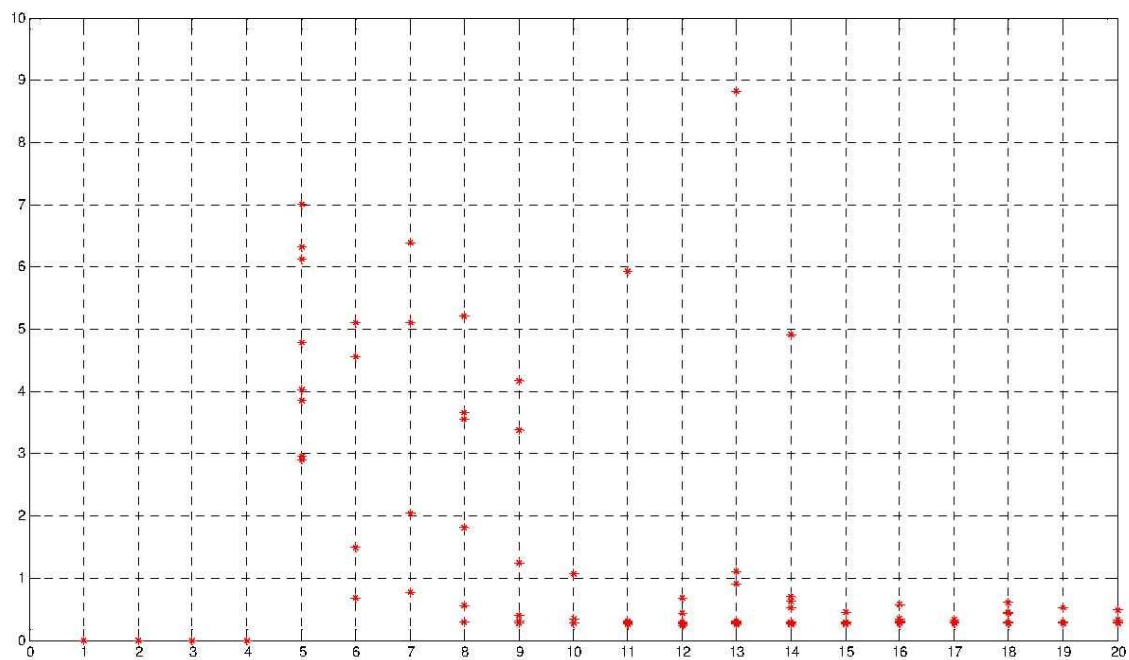


FIGURE 8: Diagram of maximum error of the network output with 10 iterations for certain number of neurons

The results of above algorithms have been collected in Table 2. Each row of the table is the result of average 40 iterations of each method. Evaluation criterion of adaptive systems was defined as following formula:

$$\text{AveragePercentageError} : APE = \frac{1}{N} \sum_{i=1}^N \left| \frac{e_i}{T_i} \right| * 100\%$$

Where T_i is the desired output and e_i is the output error. [13]

TABLE 2: Comparison of different algorithms used for predicting the concrete compressive strength

Row	Algorithm	Accuracy on data (%)				Ave. Time (second)
		Train	Validation	Test	Total	
1	Levenberg-Marquardt	99.436	99.389	99.397	99.407	7.7
2	Polak-Ribiere Conjugate Gradient	98.861	98.836	98.866	98.854	17.3
3	Fletcher-Powell Conjugate Gradient	98.713	98.675	98.695	98.694	12.4
4	Gradient Descent	98.584	98.567	98.606	98.586	24.3
5	Quasi-Newton	98.388	98.341	98.423	98.384	89.2
		Maximum Error (kg/cm2)				epochs
1	Levenberg-Marquardt	5.830	5.056	4.437	5.108	58
2	Polak-Ribiere Conjugate Gradient	9.686	8.536	7.652	8.635	571
3	Fletcher-Powell Conjugate Gradient	10.758	9.457	8.597	9.604	368
4	Gradient Descent	11.897	10.376	9.018	10.430	1833
5	Quasi-Newton	13.825	11.539	10.691	12.018	1999

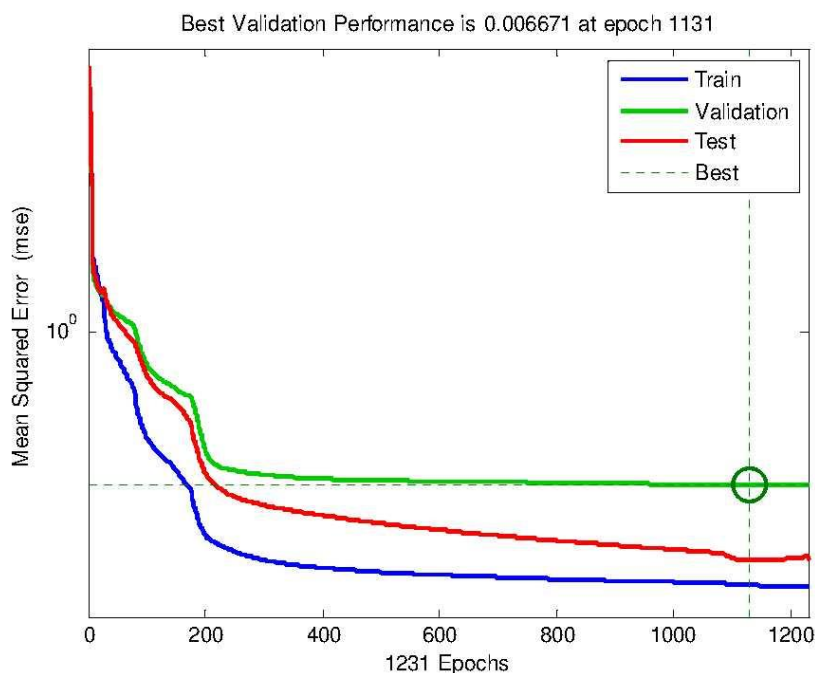


FIGURE 9: Diagram of mean squared error in the feed-forward neural network

It is conceived from table 2, that the best structure for prediction of concrete strength is the first method with levenberg-marquardt algorithm.

Figure 9 shows the mse diagram of the cost function reduction for training, validation and test data. The following results are being conceived from this figure.

1. The final mse is small and admissible
2. The test dataset error and validation dataset error are almost equal.
3. Over fitting was not happened

The diagram of figure.10 also shows the linear regression between network output and desired output for training, validation, test and total data.

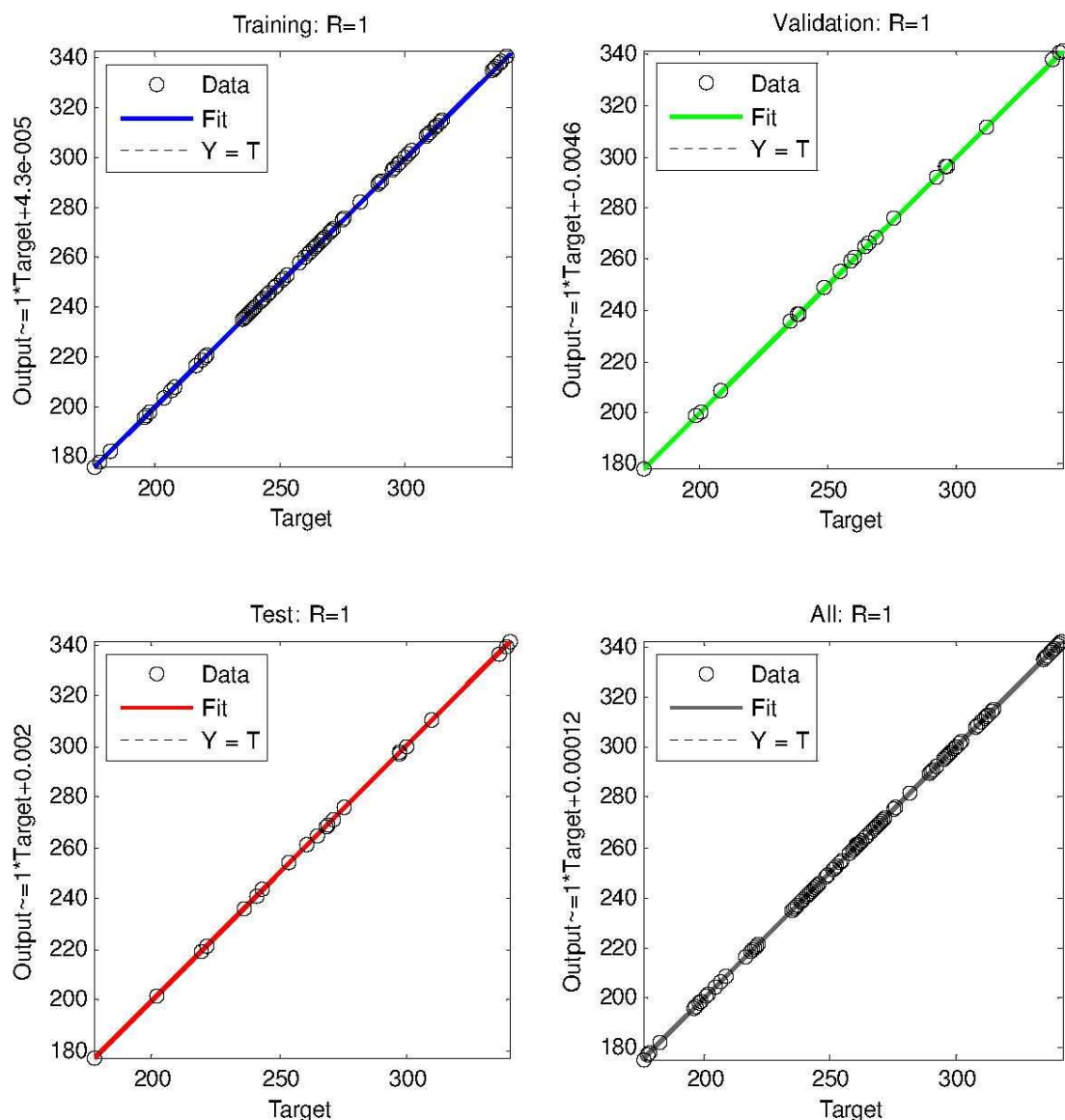


FIGURE 10: Diagram of the network output and desired output for train, validation, test and all data

16. CONCLUSION

In this paper, a practical approach has been presented for prediction of 28-day compressive strength of concrete. Basically, in all of the methods have been resented previously, the 3-day compressive strength of concrete was not considered as an important parameter.

From this point of view we can consider the proposed method as a new method in which the 3-day compressive strength parameter has been introduced as a very important index. [Ref: 13, 14, 15, 16]

The proposed technique can be used as a very useful tool for reducing the duration of the project execution in huge civil projects. For example, imagine if we have a massive concrete structure which requires 10 stages of concreting then we need at least $28 \times 10 = 280$ days to complete the total project regarding to standards. Therefore this project will be finished after about 1 year considering the frigid winter days which concreting is impossible.

Using the proposed tool we can have a precise prediction of the 28-day compressive strength of the concrete on the third day. Thereupon we need $3 \times 10 = 30$ days to complete this project and this is an important progress in order to reducing the duration of the civil projects execution.

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Civilab

Civil Engineering Testing Laboratories

Job No : 2013-B-2004	Date : 24/01//2014
Project : MZIMVUBU	

SOLUBLE DELETERIOUS IMPURITIES

Sample No	10 day cube strength of unwashed sand (a)	18 day cube strength of washed sand	*Interpolated 10 day cube strength of washed sand (b)	a/b %
2004-41	10.1	13.5	11.9	85
2004-43	8.4	11.6	10.2	82

NOTES:

Tested according to SABS test methods 834:1994

* Data interpolated with the aid of page 570 of the International Journal of Engineering, Volume 3: Issue 6. (Submitted with test results)

so/DelF2013-B-2004

Investment Facility Company 842 (Pty) Limited trading as **Civilab** Registration No: 98/19071/07
BRANCHES: CENTURION • JOHANNESBURG • RUSTENBURG

FEASIBILITY STUDY FOR THE MZIMVUBU WATER PROJECT
 GEOTECHNICAL INVESTIGATIONS: NTABELANGA, SOMABADI AND THABENG DAM SITES: APPENDICES
SOIL ANALYSIS REPORT



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 CODE: 2135
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NAME: Mzimvubu 2013-B-2004

DATE: 2 10 2013

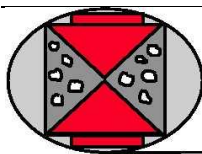
EMAIL: wihan@civilab.co.za
 FAX: 011 835 2503
 Job NO: 11857

Lab No	Ref No	Position	Depth(m)	pH (H ₂ O)	Conductivity	Na	Mg	CEC	ESP	EMgP	Na	Ca	Mg	SAR	Cl
					mS/m	me/100gsoil (cmol+)/kg	me/100gsoil (cmol+)/kg	cmol(+)/kg			me/l	me/l	me/l		mg/kg
60442	S 2			6.88	5.72	0.04	0.57	1.71	2.49	33.10	0.24	0.89	0.50	0.29	2.66
60443	S 4			6.53	4.59	0.04	0.57	1.66	2.51	34.52	0.15	0.04	0.23	0.41	1.26


 N. REEDERS

H 9

WATER



CONTEST

Concrete Technology Services

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Ref: CJ13/08/739

16 August 2013

Client: Jeffares & Green

Subject: Water Testing

LABORATORY REPORT

CLIENT

Jeffares & Green, P O Box 794, HILTON, 3245

SYNOPSIS:

Physical and chemical tests on a sample of water have been provided.

BRIEF FROM CLIENT:

Contest were requested to analyse the samples for;

- Total dissolved solids
- Chloride content
- Calcium hardness as CaCO_3
- pH
- Sulphates (as SO_3)
- Comparative Cubes

SAMPLES:

4 5litres samples of water, referenced, Tsitsa River, by the client, were received on 07.08.2013.

TESTING:

The following test methods were used;

- Total dissolved solids - SABS Standard Method 213.
- Chloride content - Volhard method typically as described in Quantitative Analytical Chemistry by Fritz & Schenk.
- Calcium Hardness of water - SABS Standard Method 216. This does not give the total carbonates and bicarbonates, but simply the calcium hardness or equivalent calcium carbonate in mg/ℓ .
- pH - as described in the operating manual of our pH meter - a WTW inoLab pH720 meter and using Hanna buffer solutions for calibration.
- Sulphate - SABS Standard Method 212.

Adam Investments cc. Reg. No 1988/019362/23 t/a CONTEST Concrete Technology Services
Managing Member: RJL Raw B Tech (Civil Eng)
Members: MT Clark, JS Dunnett, MC Mzobe, VA Horton
Consultant: A J M Horton Pr Tech (Eng), Dip ACT, HND (Chem), HNC (Civ. Eng), FICT, MSA Corr I

Testing, Training and Consulting in Concrete

Ref: CJ13/08/739

16 August 2013

Client: Jeffares & Green

Subject: Water Testing

- Comparative Cubes

All tests were carried out in duplicate i.e. an A and B sample and the average values determined and reported.

RESULTS:

Chemical Testing:

	Client Sample
TDS (mg/l)	105.5
Chloride (Cl ⁻) (mg/l)	5.3
Calcium Hardness as CaCO ₃ (mg/l)	101.6
pH	7.75
Sulphate (SO ₃) (mg/l)	None detected

Physical Testing:

Comparative cubes:

	Control	Sample	Sample as % of Control
	MPa	MPa	%
24hr	4.6	4.5	98
5d	14.9	15.1	101
7d	16.8	17.6	105
28d	tba	tba	tba

COMMENT:

The results indicate that the water sample is suitable for concrete manufacture.

We have used the following limits based on various sources for a number of years.

	(mg/l)
Total dissolved solids	2000
Chloride (as Cl ⁻)	500
Calcium Hardness(as CaCO ₃)	400
pH	6 to 8

Ref: CJ13/08/739
Client: Jeffares & Green
Subject: Water Testing

16 August 2013

Sulphate as SO ₃	1000
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These values seem to be conservative based on some of the latest publications; in particular the upper range of pH seems to have been increased substantially, probably with the experience of using wash water in RMC plants.

The ninth edition of Fulton's Concrete Technology states that the mean compressive strength at **seven** days of the test specimen, prepared with the test water, shall be 90% of the mean compressive strength of the corresponding specimens prepared with distilled or deionised water.

However, the eight edition of Fulton's Concrete Technology states that the compressive strength of 'test' cubes at 28 days should be no less than 90% of the control cubes.

BS 3148 has suggested that if the strength is between 80 and 90%, then the water can still be used if the concrete mix proportions are adjusted.

Compressive strength of cubes at 24 hours and 5 days was carried out to determine any early age effect on the concrete strength.



R J L Raw
B Tech (Civil Eng)

APPENDIX I

LONGITUDINAL SECTION SHOWING RECOMMENDED CUT-OFF EXCAVATION

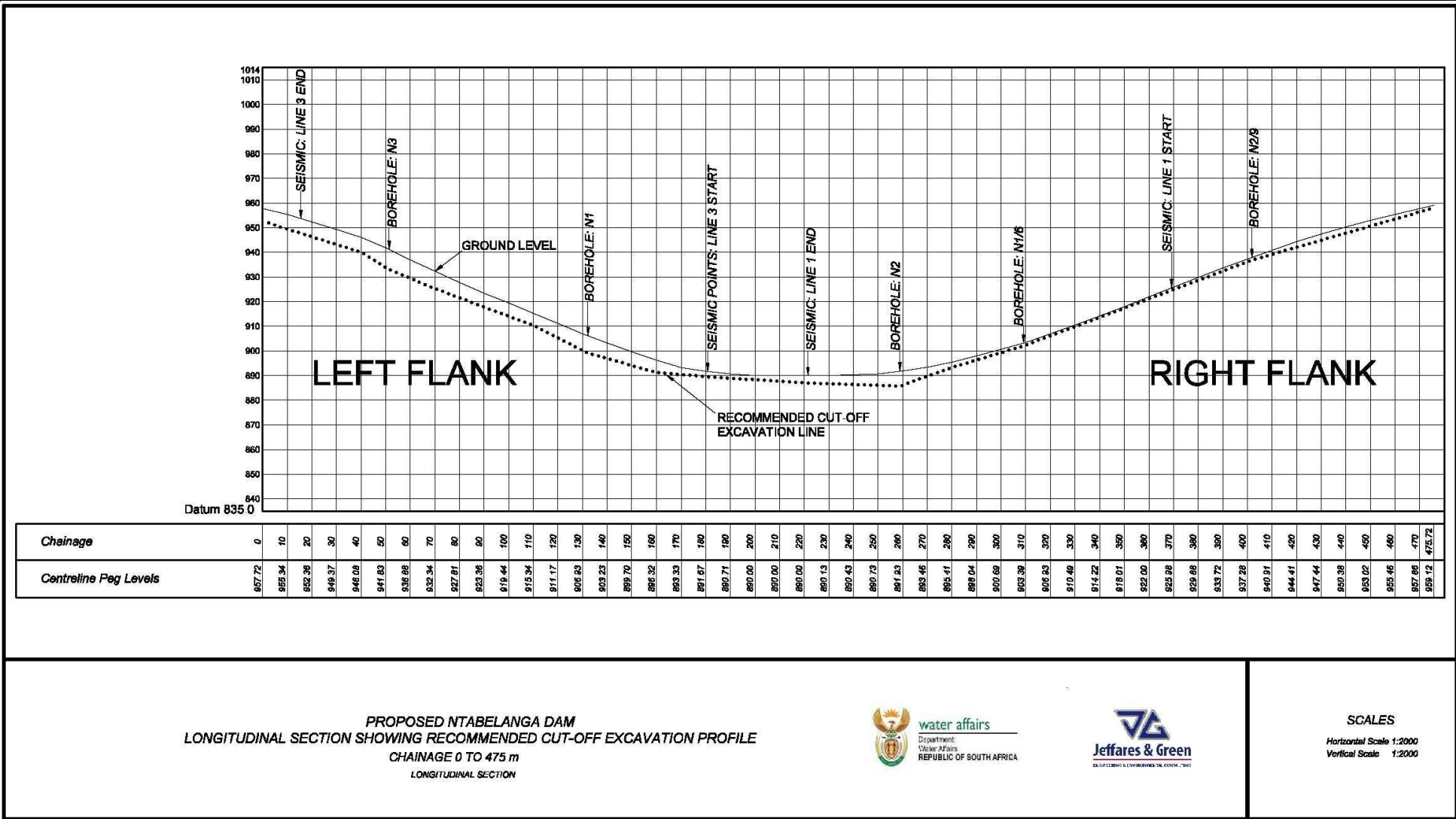


Fig I-1: LS - Recommended Cut-Off Excavation Profile

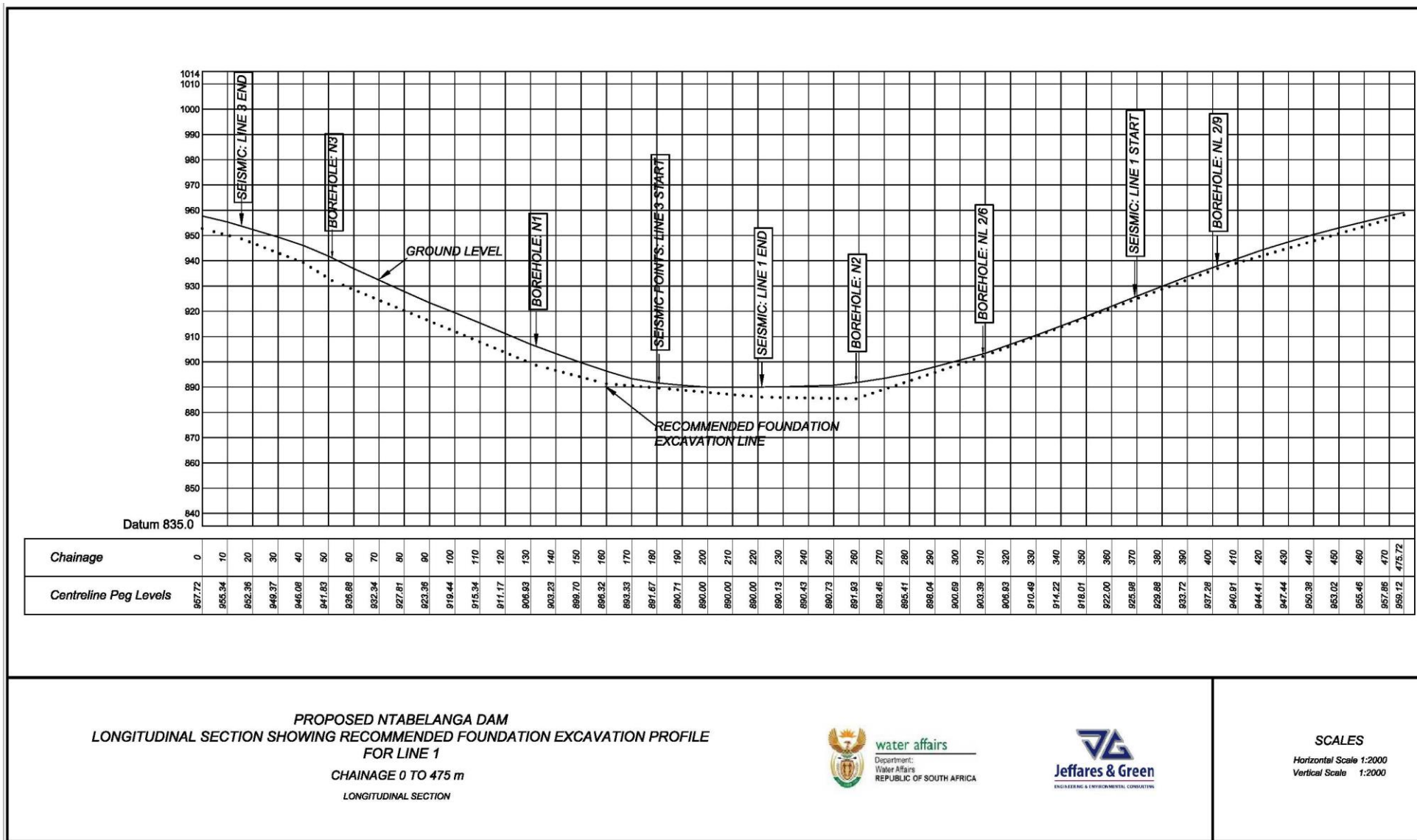


Fig I-2: LS - Recommended Foundation Excavation Profile for Line 1

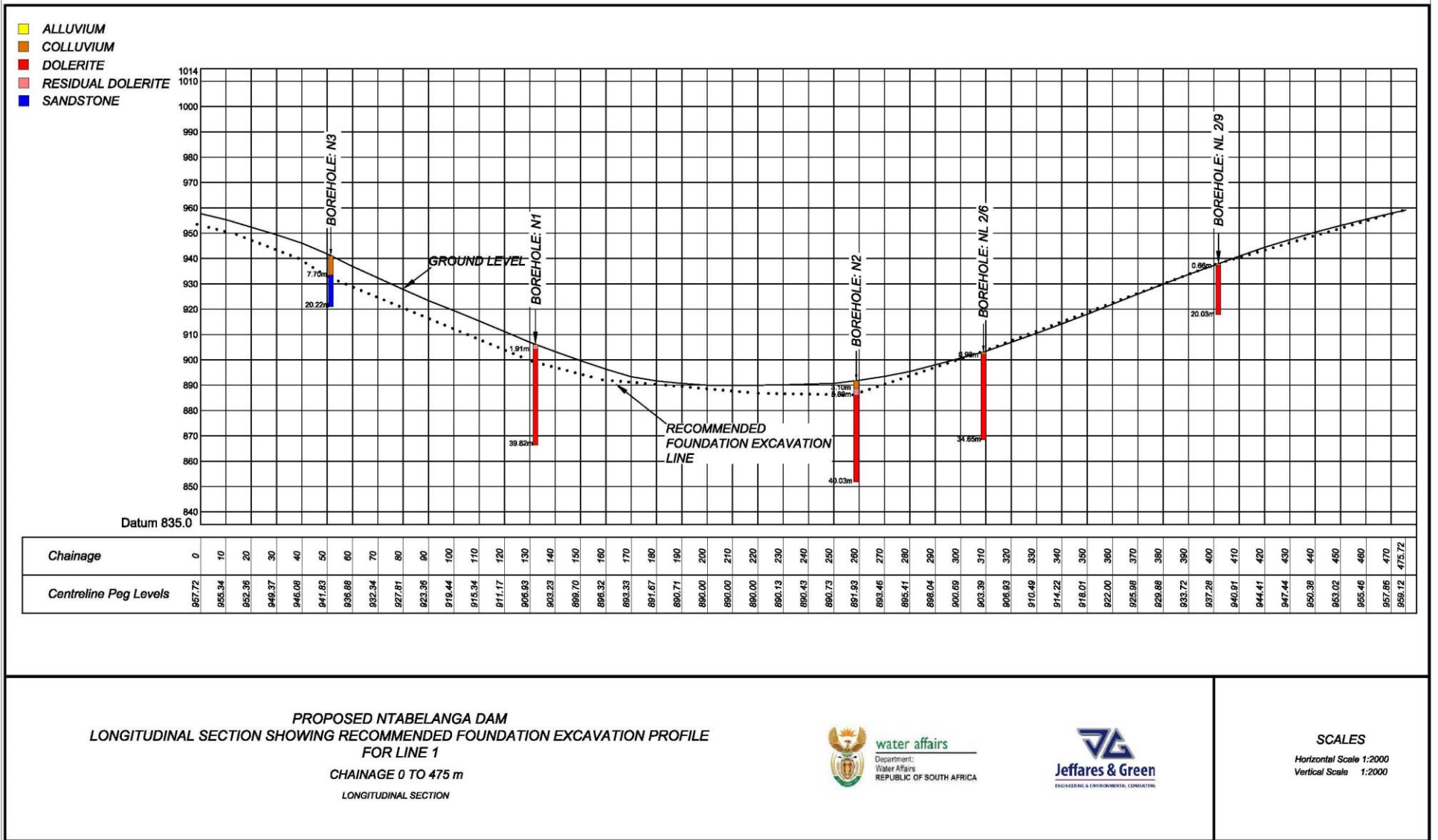


Fig I-3: LS - Recommended Foundation Excavation Profile for Line 1

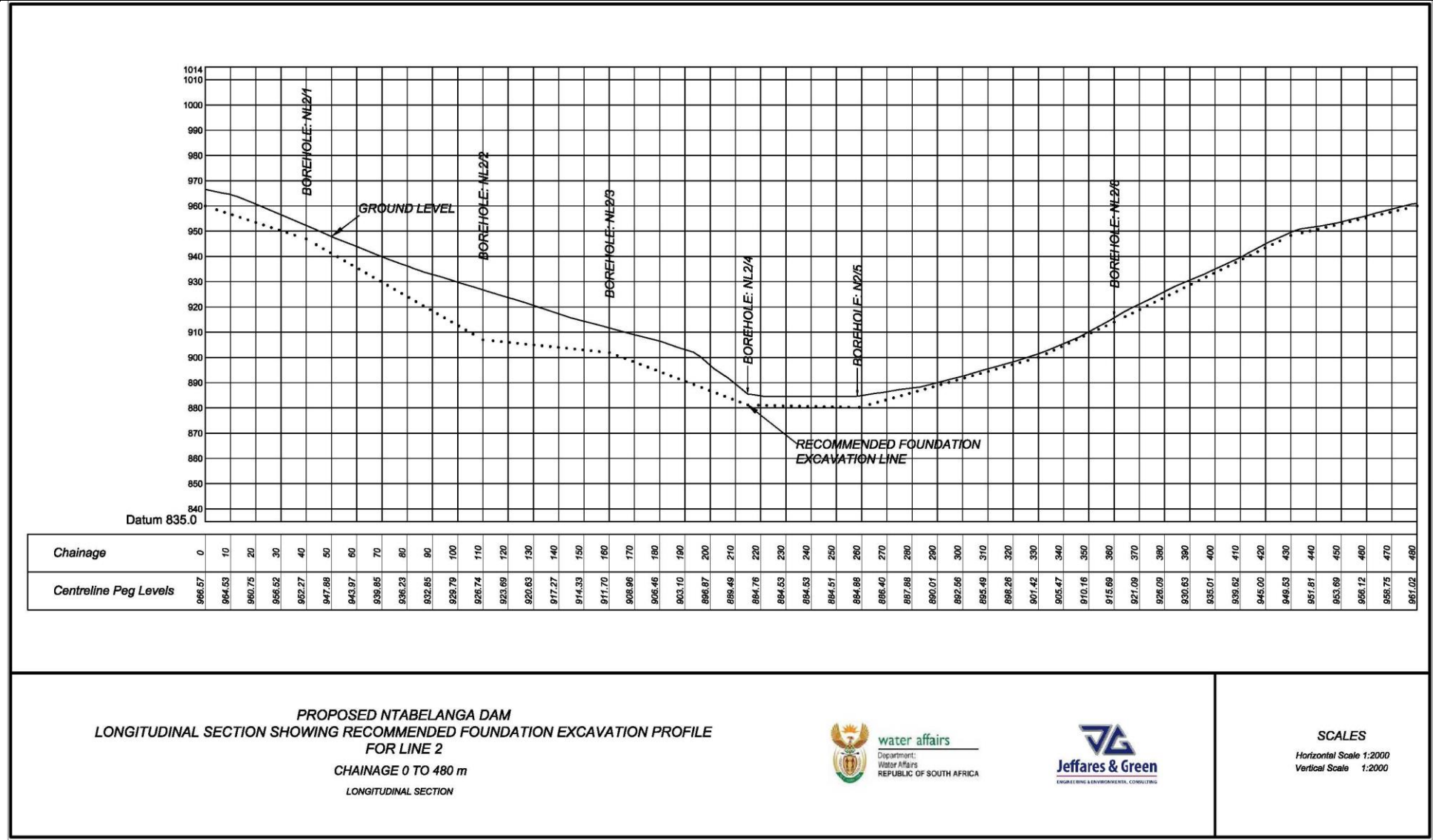


Fig I-4: LS - Recommended Foundation Excavation Profile for Line 2

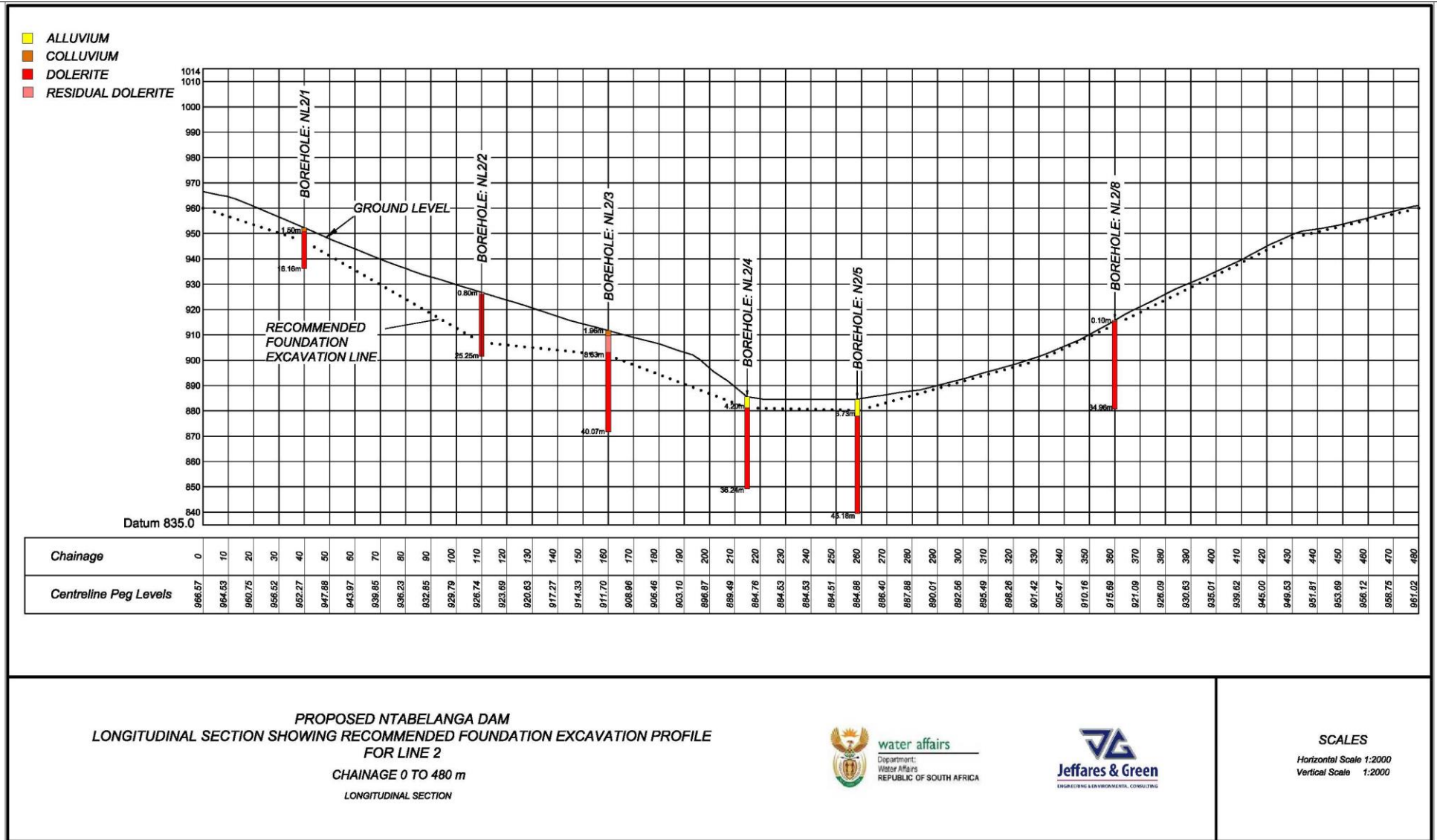


Fig I-5: LS - Recommended Foundation Excavation Profile for Line 2